

A COMPARISON OF THE INVERSE NYQUIST ARRAY AND POLE ASSIGNMENT TECHNIQUES

by **Rainer Horst Erich Venzke**

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ABSTRACT

This dissertation compares the Inverse Nyquist Array (INA) and the Pole Assignment techniques in multivariable control system design.

The representation of multivariable systems in both the frequency domain and state space is discussed. A laboratory flotation system, for which a model by step response analysis is derived, is used as a practical example for both methods.

A detailed description of the theory of both techniques is given. Particular emphasis is given to how the theory can be applied with the use of a personal computer. Computer-aided control system design programs for the INA and Pole Assignment techniques are included.

A complete feedback control scheme for the flotation rig is designed with the INA technique. Pole Assignment by state feedback is used to improve the speed of response of the rig.

The implementation of a Kalman filter, which is required for the Pole Assignment technique, is also described.

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NOMENCLATURE

u	Plant input vector
y	Plant output vector
D	Differential operator
G, g	Transfer function
G	Multivariable transfer function matrix
g	Transfer function element of G
K	Pre-compensator matrix in frequency domain
L	Post-compensator matrix in frequency domain
F	Feedback matrix in frequency domain
K_{pi}	PI controller matrix
Q	Open-loop transfer function
H	Closed-loop transfer function
I	Identity matrix
τ	Time delay
a	Real coefficients
b	" "
x	State vector
A, B, C, D	State space model matrices
P	Controller matrix in frequency domain

1. INTRODUCTION

1.1 INTRODUCTION

The application of multivariable control theory in system design has in the past been extremely tedious, due to the computational complexity. Although most industrial applications are of multivariable nature, only singlevariable techniques were applied as it was difficult and time consuming to use computers such as mainframes, if available, in the design process. With the advent of the personal computer (PC) this has however drastically changed.

The design engineer can now readily apply the multivariable techniques by making use of computer-aided design (CAD) software. The computer will enable him to design, experiment with and simulate the control scheme before implementation. Such computer programs are now becoming increasingly available, easing the process of control system design and allowing the designer to apply techniques which may have been too complicated in the past.

In the course of this research a complete interactive design program for PC's applying the Inverse Nyquist Array (INA) design technique was developed. Routines for the Pole Assignment technique were also written. A paper outlining the approach was presented by the author.(1)

In this research two multivariable design techniques, namely the INA and Pole Assignment methods were investigated. The methods were applied to a laboratory flotation rig and the

necessary software to aid in the design process as well as implementing the control scheme were developed for a PC.

1.2 DISSERTATION ORGANISATION

The aim of this dissertation is to discuss the relative merits and disadvantages of the INA and the Pole Assignment design techniques.

In this chapter, the subject of the research and the aim of the dissertation are formulated. A basic introduction to multivariable systems is given. In chapter two a transfer function model for the flotation rig is developed. The theory of the INA technique is discussed in chapter three and then implemented in chapter four. Chapters five and six repeat the process for the pole assignment method.

The two techniques are compared in chapter seven, where suggestions for future research is also given.

The main software that was developed in the process of this research and the INA design package in particular are combined in Appendix D entitled *Software Reference*.

1.3 PLANT DESCRIPTION

A plant can be described as being some process which is driven by inputs and has a number of outputs. The outputs of the process are functions of its inputs. No restrictions are made to the types of inputs or outputs. They may be mechanical movement, electrical quantities or chemical substances and depend solely on the process being investigated. It is however necessary for these quantities to be measurable in some way.

Singlevariable processes contain plants with one input and one output only. Multivariable processes, which are investigated in this discussion, have a number of inputs and a number of output quantities. In addition, the inputs of such systems are usually interacting, a single input affects more than one output. Fig. 1.1 shows a block diagram of plant with 2 inputs and 2 outputs.

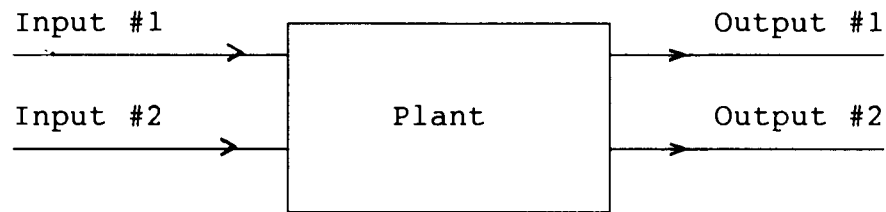


FIG. 1.1 Multivariable process

1.4 CONTROL SYSTEM MODELS

In process control the design engineer is concerned with measuring the outputs of a plant and manipulating its inputs to achieve a desired response of the outputs. To analyse and design a control system, the engineer needs a quantitative model of the plant, which relates the inputs to the outputs.

1.4.1 LINEAR AND TIME-INVARIANT MODELS

It is very intricate to describe in complete detail the behaviour of plants. To avoid complicated models, the analysis of control systems is simplified by modelling the plants with linear and time-invariant differential equations.

1.4.2 NON-LINEAR PLANT BEHAVIOUR

In most plants the requirements of linearity and time-invariance do not hold and to demonstrate the differences, a water level control system (Fig. 1.2) is analysed. In this case the first valve is controlled to keep the level of water in the tank at a fixed setpoint. The second valve acts as a disturbance into the system, which will change the level of the water. The disturbances that affect the plant are termed noise inputs. These are usually numerous and are not contained in the model.

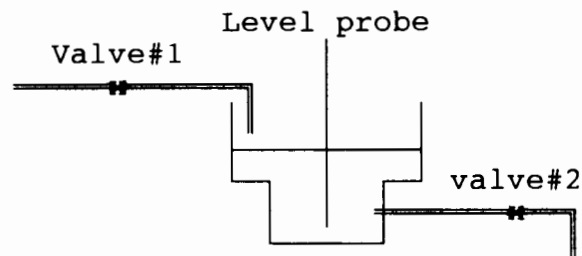


FIG. 1.2 Water level control system

A valve that is opened by pneumatic pressure to regulate the flow into a container has inherent non-linearities. The function relating the pressure to the resulting flow will not be perfectly linear and once the valve is fully open further increases in pressure will not result in bigger flow. The output variables are usually also nonlinear and can also be driven into saturation. The tank collecting the water may have a shape as depicted in Fig. 1.2. For a constant flow into the tank the level will increase more rapidly in the narrower region. Once the tank overflows the measured level will remain at its maximum.

CHAPTER 1 INTRODUCTION

In control theory, methods do exist to analyse non-linear systems, but it is a common practice to rely on the fact that if the input and output variables stay close enough to a given operating point they do behave in a linear fashion.

The simplification of time-invariance also does not hold for most real systems. In the depicted tank system the sensitivity of level probe may depend on the conductivity of the water contained in the tank and this may change over time.

1.4.3 FEEDBACK SYSTEMS

To a certain extent, the inaccuracies in the model can be eliminated by feedback. In feedback systems the output variables are continuously compared to a desired group of setpoints and changes are made to the inputs according to the difference between them.

Using approximate models of plant behaviour greatly simplifies the design process and will lead to acceptable controllers(2) for feedback control systems.

1.5 TRANSFER FUNCTION MODELS

A multivariable plant can be modelled in the time domain by a set of linear differential equations:

$$\mathbf{a}_n D^n \mathbf{y} + \mathbf{a}_{n-1} D^{n-1} \mathbf{y} + \dots + \mathbf{a}_1 \mathbf{y} = \mathbf{u}(t) \quad (1.1)$$

where D represents the differential operator, vector $\mathbf{y}(t)$

the responses to the driving function vector $u(t)$ and the corresponding block diagram is shown below.

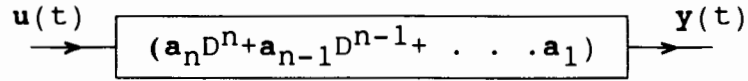


FIG. 1.3 Time domain description

By taking the Laplace transform of the above equation, the frequency domain description with zero initial conditions is then

$$y(s) = G(s)u(s) \tag{1.2}$$

Fig. 1.4 depicts this in block diagram form.

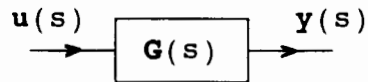


FIG. 1.4 Frequency domain description

A multivariable system given by Eqn. (1.2) having k inputs and m outputs can be written as follows:

$$\begin{bmatrix} y_1(s) \\ y_2(s) \\ \vdots \\ y_m(s) \end{bmatrix} = \begin{bmatrix} g_{11}(s) & g_{12}(s) & \dots & g_{1k}(s) \\ g_{21}(s) & g_{22}(s) & \dots & \cdot \\ \vdots & \vdots & \ddots & \vdots \\ g_{m1}(s) & g_{k2}(s) & \dots & g_{mk}(s) \end{bmatrix} \begin{bmatrix} u_1(s) \\ u_2(s) \\ \vdots \\ u_k(s) \end{bmatrix}$$

where

$$g_{ij}(s) = \frac{a_{c-1}s^{c-1} + a_{c-2}s^{c-2} \dots + a_0}{s^{d-1} + b_{d-2}s^{d-2} \dots + b_0} e^{-\tau s} \quad (1.3)$$

with a_c and b_d being real coefficients and τ is a pure time delay.

1.5.1 RESTRICTION ON $g_{ij}(s)$

In Eqn. (1.3) $c \leq d$ for all physical processes. A transfer function with numerator order higher than that of the denominator is not realisable.

For most control applications it is required that the high frequency gain of $G(s)$ is zero, i.e $G(s)$ is strictly proper(3):

$$\lim_{s \rightarrow \infty} g_{ij}(s) = 0 \quad (1.4)$$

In most cases $G(s)$ is chosen to be a square matrix with $n=k=m$. This is important when multivariable feedback system are designed, because then n individual feedback loops can be constructed such that output y_i is related to input u_i . This setup is detailed in Fig. 1.5.

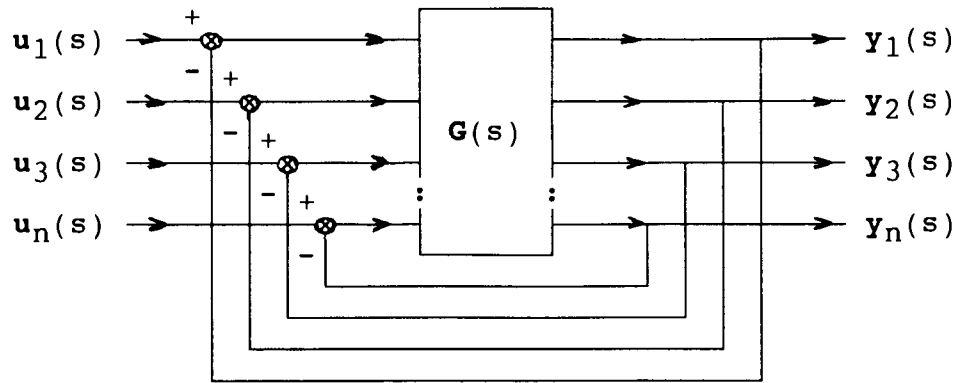


FIG. 1.5 Multivariable unity feedback control system

1.6 STATE SPACE DESCRIPTION

An alternative approach is to model the process by a set of linear first order differential equations:

$$\frac{dx(t)}{dt} = \mathbf{A} x(t) + \mathbf{B} u(t) \quad (1.5)$$

$$y(t) = \mathbf{C} x(t) + \mathbf{D} u(t) \quad (1.6)$$

The above equations relate the system variables or states $x_i(t)$ and their derivatives to the system outputs $y_i(t)$ and inputs $u_i(t)$.

CHAPTER 1 INTRODUCTION

If the plant has k inputs and m outputs and the process has n states then

$$\begin{bmatrix} \dot{x}'_1(t) \\ \dot{x}'_2(t) \\ \vdots \\ \dot{x}'_n(t) \end{bmatrix} = \begin{bmatrix} a_{11} & a_{12} & \dots & a_{1n} \\ a_{21} & a_{22} & \dots & \cdot \\ \vdots & \vdots & \ddots & \vdots \\ a_{n1} & \cdot & \dots & a_{nn} \end{bmatrix} \begin{bmatrix} x_1(t) \\ x_2(t) \\ \vdots \\ x_n(t) \end{bmatrix} + \begin{bmatrix} b_{11} & b_{12} & \dots & b_{1k} \\ b_{21} & b_{22} & \dots & \cdot \\ \vdots & \vdots & \ddots & \vdots \\ b_{n1} & \cdot & \dots & b_{nk} \end{bmatrix} \begin{bmatrix} u_1(t) \\ u_2(t) \\ \vdots \\ u_k(t) \end{bmatrix}$$

$$\begin{bmatrix} y_1(t) \\ y_2(t) \\ \vdots \\ y_m(t) \end{bmatrix} = \begin{bmatrix} c_{11} & c_{12} & \dots & c_{1n} \\ c_{21} & c_{22} & \dots & \cdot \\ \vdots & \vdots & \ddots & \vdots \\ c_{m1} & \cdot & \dots & c_{mn} \end{bmatrix} \begin{bmatrix} x_1(t) \\ x_2(t) \\ \vdots \\ x_n(t) \end{bmatrix} + \begin{bmatrix} d_{11} & d_{12} & \dots & d_{1k} \\ d_{21} & d_{22} & \dots & \cdot \\ \vdots & \vdots & \ddots & \vdots \\ d_{m1} & \cdot & \dots & d_{mk} \end{bmatrix} \begin{bmatrix} u_1(t) \\ u_2(t) \\ \vdots \\ u_k(t) \end{bmatrix}$$

(1.7)

where $\dot{x}_i = \frac{dx_i}{dt}$

The matrixes **A, B, C, D** have constant coefficients and are of dimensions as depicted above.

The block diagram of the state space model is shown in fig. 1.6. The implementation of state or output feedback is also depicted.

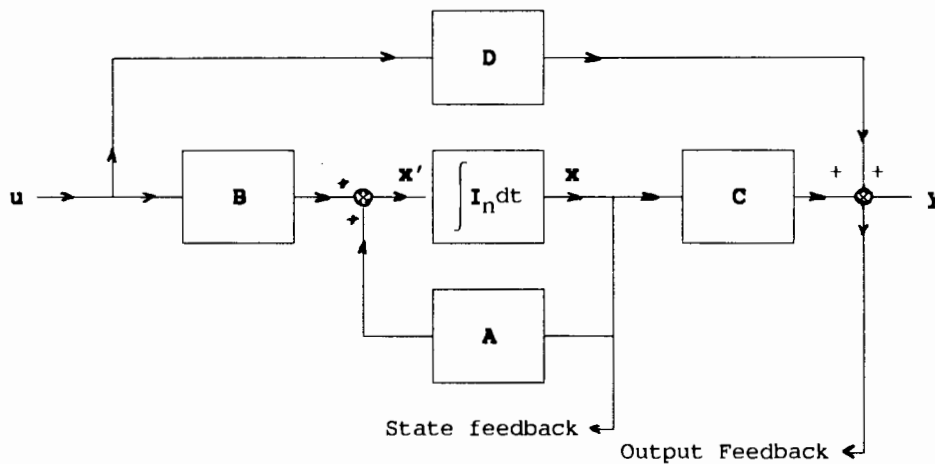


FIG. 1.6 Block diagram of state space model

In most processes $D=0$, which is equivalent to $G(s)$ being strictly proper.

1.7 MOVING BETWEEN MODELS

The equation relating the state space representation to the transfer function model is give by

$$G(s) = C(sI-A)^{-1}B+D \quad (1.8)$$

1.7.1 STATE SPACE TO TRANSFER FUNCTION

The difficulty in moving from state space to the transfer function model lies in evaluating $(sI-A)^{-1}$.

1.7.1.1 Faddeev Method

The Faddeev algorithm(4) computes the adjoint of $(s\mathbf{I}-\mathbf{A})$ and simultaneously calculates the characteristic polynomial $|s\mathbf{I}-\mathbf{A}|$.

$$(s\mathbf{I}-\mathbf{A})^{-1} = \frac{\text{Adj}(s\mathbf{I}-\mathbf{A})}{|s\mathbf{I}-\mathbf{A}|} \quad (1.9)$$

$$= \frac{R_0s^{n-1}+R_1s^{n-2}+\dots+R_{n-2}s+R_{n-1}}{e_0s^n+e_1s^{n-1}+\dots+e_{n-1}s+e_n} \quad (1.10)$$

The matrix coefficients R_i and coefficients e_i are calculated recursively from:

$$\begin{aligned} e_0 &= 1 & R_0 &= \mathbf{I} \\ e_i &= \frac{-1}{i} \text{trace}(\mathbf{A}R_{i-1}) \end{aligned}$$

and

$$\begin{aligned} R_i &= \mathbf{A}R_{i-1} + e_i\mathbf{I}, \quad i=1,n \\ R_n &= 0. \end{aligned} \quad (1.11)$$

Although R_n need not be calculated, it can be used to check the computational accuracy of the method. Because of the recursive nature of the algorithm it is considered to be numerically unsatisfactory.(4) The Faddeev algorithm does however possess the feature of a computational check, which other techniques lack.

1.7.2 TRANSFER FUNCTION TO STATE SPACE

Numerous techniques exist to transform a multivariable model $\mathbf{G}(s)$ to the state space domain.(3)

CHAPTER 1 INTRODUCTION

To move from the transfer function representation to that of state space for singlevariable systems is best illustrated by an example.

Let

$$g(s) = \frac{y(s)}{u(s)} = \frac{a_1s+a_0}{s^2+b_1s+b_0} \quad (1.12)$$

By multiplying numerator and denominator of eqn. (1.12) by $w(s)$ and equating them, then

$$s^2w(s) = -b_1sw(s) - b_0w(s) + u(s)$$

and

$$y(s) = a_1sw(s) + a_0w(s) \quad (1.13)$$

Let

$$\mathbf{x}(s) = \begin{bmatrix} sw(s) \\ w(s) \end{bmatrix} \quad (1.14)$$

then

$$s\mathbf{x}(s) = \begin{bmatrix} -b_1 & -b_0 \\ 1 & 0 \end{bmatrix} \mathbf{x}(s) + \begin{bmatrix} 1 \\ 0 \end{bmatrix} u(s)$$

$$y(s) = \begin{bmatrix} a_1 & a_0 \end{bmatrix} \mathbf{x}(s) \quad (1.15)$$

For the general case assuming that

$$g(s) = \frac{a_{n-1}s^{n-1} + a_{n-2}s^{n-2} \dots + a_0}{s^{d-1} + b_{d-2}s^{d-2} \dots + b_0} \quad (1.16)$$

then

$$\mathbf{A} = \begin{bmatrix} b_{d-2} & b_{d-3} & \dots & b_0 \\ 1 & 0 & \dots & \vdots \\ 0 & 1 & \dots & \vdots \\ \vdots & \vdots & \ddots & \vdots \\ 0 & \vdots & \dots & 1 & 0 \end{bmatrix}, \quad \mathbf{B} = \begin{bmatrix} 1 \\ 0 \\ 0 \\ \vdots \\ 0 \end{bmatrix}$$

$$\mathbf{C} = [a_{d-2} \ a_{d-3} \ \dots \ a_0]$$

$$D = a_{d-1} \tag{1.17}$$

This technique can also be used to transform a multivariable system $\mathbf{G}(s)$ into state space form in the following manner.

If \mathbf{A}_{ij} , \mathbf{B}_{ij} , \mathbf{C}_{ij} , \mathbf{D}_{ij} were found for each $\mathbf{g}_{ij}(s)$ then the state space model can be constructed by setting

$$\mathbf{A} = \begin{bmatrix} \mathbf{A}_{11} & 0 & \dots & 0 \\ 0 & \mathbf{A}_{12} & \dots & \vdots \\ \vdots & \vdots & \ddots & \vdots \\ 0 & 0 & \dots & \mathbf{A}_{nn} \end{bmatrix} \tag{1.18}$$

and forming matrices \mathbf{B} , \mathbf{C} and \mathbf{D} using this structure.

1.8 CONTROLLABILITY AND OBSERVABILITY

In state space models of multivariable systems the criteria of controllability and observability play an important role. They give an indication of whether a plant can be fully controlled, and if not only a subsystem of the plant can be used to design a control scheme. It is thus important, that the model of the plant does not give rise to uncontrollable modes unnecessarily.

1.8.1 CONTROLLABILITY

A system is controllable(5) if all the modes can be excited or controlled by the input.

In terms of the state space representation, the system is controllable if and only if

$$\mathbf{P} = (\mathbf{B} \ \mathbf{AB} \ \mathbf{A}^2\mathbf{B} \ \dots \ \mathbf{A}^{n-1}\mathbf{B}) \quad (1.19)$$

has rank n .

1.8.2 OBSERVABILITY

A system is observable(5) if all the modes affect the output. In terms of the state equations a system is observable if and only if

$$\mathbf{Q} = (\mathbf{C}^T \ (\mathbf{CA})^T \ (\mathbf{CA}^2)^T \ \dots \ (\mathbf{CA}^{n-1})^T) \quad (1.20)$$

has rank n .

1.9 SIMULATION OF SYSTEM RESPONSE

The ability to simulate the system is the most important tool in control system design. It is used to develop a model of the plant by comparing the simulated step responses to those of the plant. It can further be used to analyse the closed-loop system behaviour to step inputs, its integrity and its sensitivity to dynamic changes of the plant.

The fourth-order Runge Kutta technique(6) can be used for this purpose. This method solves the linear first order differential equation in Eqn. (1.5). If a transfer function model is to be simulated, it must be transformed into its state space description first.

The algorithm can be summarised as follows:

Simulation of

$$\mathbf{x}'(t) = \mathbf{Ax}(t) + \mathbf{Bu}(t) \quad (1.21)$$

with initial conditions \mathbf{x}'_0 , \mathbf{x}_0 , \mathbf{u}_0 and choosing a sufficiently small time step size h is achieved by iterating:

$$\mathbf{v}_{1,t} = h(\mathbf{Ax}_t + \mathbf{Bu}_t)$$

$$\mathbf{v}_{2,t} = h(\mathbf{A}(\mathbf{x}_t + \frac{1}{2}\mathbf{v}_{1,t}) + \mathbf{Bu}_t)$$

$$\mathbf{v}_{3,t} = h(\mathbf{A}(\mathbf{x}_t + \frac{1}{2}\mathbf{v}_{2,t}) + \mathbf{Bu}_t)$$

$$\mathbf{v}_{4,t} = h(\mathbf{A}(\mathbf{x}_t + \mathbf{v}_{3,t}) + \mathbf{Bu}_t)$$

$$\mathbf{x}_{t+1} = \mathbf{x}_t + \frac{1}{6} (\mathbf{v}_{1,t} + 2\mathbf{v}_{2,t} + 2\mathbf{v}_{3,t} + \mathbf{v}_{4,t}) \quad (1.22)$$

where \mathbf{x}_{t+1} is an approximation to $\mathbf{x}(t+h)$.

The accuracy of the above method relies heavily on the choice of h . The time step must be small enough for the

CHAPTER 1 INTRODUCTION

iterations to approximate the derivative $x'(t)$ accurately, but if h is too small, then the floating point accuracy of the computer will introduce significant rounding errors. This algorithm is relatively easy to implement on a digital computer and an online adjustment of h by trial and error usually gives acceptable results. More accurate methods exist(7), but they are often unnecessarily complicated.

1.10 CONCLUSION

Although numerous representations exist, the transfer function and state space models for linear, time-invariant multivariable systems were presented in particular. A detailed description of changing from one to the other was given.

The transfer function model is usually used to establish a model from step response analysis, whereas the state space model is derived scientifically. The former will be found for the flotation rig in the next chapter.

CHAPTER 1 INTRODUCTION

2. THE FLOTATION RIG

2.1 INTRODUCTION

In this chapter industrial flotation systems with particular reference to the one at Black Mountain are described. A detailed description of the laboratory flotation rig is given and the desired operating region is specified.

A linear transfer function modelling the rig is found from step tests and a sub-system is selected from it, which will be used to apply the Inverse Nyquist and Pole Assignment techniques in later chapters.

2.2 INDUSTRIAL FLOTATION SYSTEMS

Flotation systems are mainly used in South Africa in the mineral extraction industry. A detailed description of such an application is given by Twidle(8). In that system copper, lead and zinc are recovered from ground complex sulphide ore by sequential flotation. By-products such as silver are also produced. The crushed pulp is sequentially treated with chemical reagents in different tanks of the flotation circuit to produce the desired concentrate.

The levels of slurry in the various tanks and the chemical properties such as pH make up the controlled entities.

2.3 THE LABORATORY FLOTATION RIG

The laboratory flotation rig has been built to model the flow characteristics of industrial flotation systems. The plant structure is depicted in Fig. 2.1. The model consists of one circuit, which is made up of four individual flotation extraction tanks, simulating the Rougher, Scavenger, Cleaner and Recleaner.

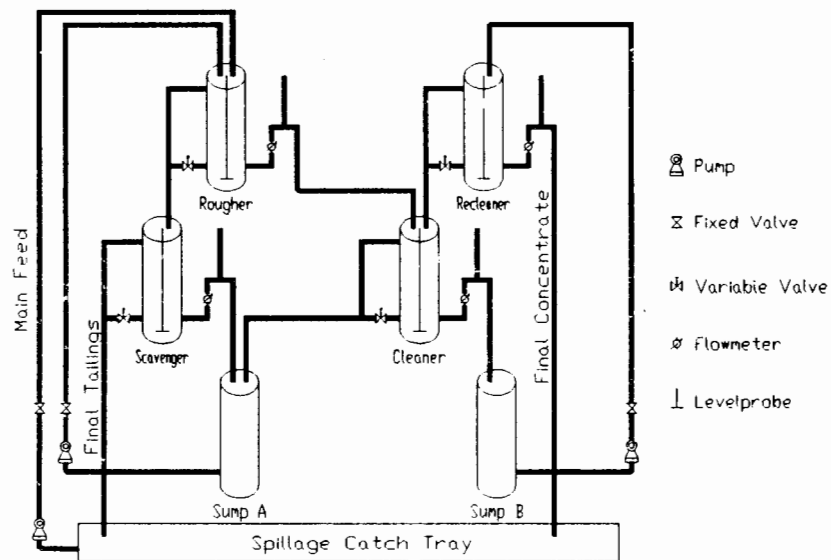


FIG. 2.1 Laboratory flotation rig

CHAPTER 2 THE FLOTATION RIG

In a industrial plant the pulp is mixed with chemical substances such that the desired product or concentrate accumulates in the froth which then passes to the next extraction process, where additional chemicals may be added. Once most of the concentrate is removed the remaining pulp, termed the final tailings, may pass to another circuit where the process is repeated to extract a different product.

In the laboratory setup tap water instead of pulp is used. The water is pumped from a spillage catch tray at a fixed rate into the Rougher tank. The concentrate in the 'froth' passes onto the Cleaner tank. The pipes passing the concentrate are mounted at the bottom to simplify construction, which is acceptable as no froth is actually produced in the tanks. The tailings of the Rougher tank enter the Scavenger tank, from which the concentrate is pumped back into the Rougher to repeat the first extraction process. The tailings of the Scavenger are discarded into the spillage catch tray.

The concentrate collected from the Rougher and Scavenger tanks enter the Cleaner from which the concentrate moves on to the Recleaner and the tailings are fed back to the Rougher via a sump. The concentrate obtained from the Recleaner tank is the end-product of this flotation circuit and would normally contain a high concentration of the extracted mineral. The tailings of the Recleaner are passed back into the Cleaner to re-enter the second filtering process.

Overflow protection pipes are mounted on all the tanks.

In a real plant the individual tanks may consist of a number of tanks with their own filtering processes.

CHAPTER 2 THE FLOTATION RIG

The levels of the pulp in the four tanks and the flows of the concentrate are the measured variables in the model. Other controlled entities such as the addition of chemicals to and measurements such as pH of the pulp are not included in the model.

The signals from the level probes and flowmeters are read by an analog to digital (A/D) converter into the microcomputer. A D/A card is used to control the pneumatic outlet valves of the individual tanks from the computer.

The range of values for the level measurements, flowmeters and the output to the valves are from 0 to 4095, which will be referred to as units. A maximum level and flow reading corresponds to 4095 units and a complete closure of a valve is achieved by writing a value of 4095 units.

2.3.1 OPERATING REGION

An operating region for the valves and water level needs to be defined in which a mathematical model, as discussed in chapter one, describes the behaviour of the flotation rig in a linear fashion.

The operating regions of the level of water in all tanks are defined in Fig. 2.2.

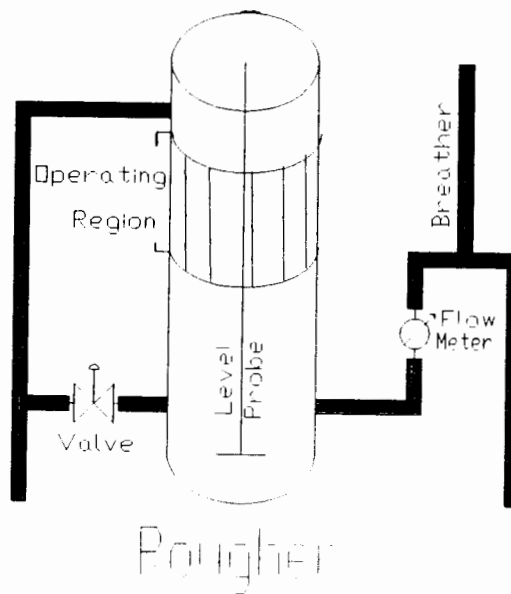


FIG. 2.2 Operating region

It is necessary to operate the plant in these regions as severe changes in the plant characteristics take place when the height of water move beyond these limits. If for example the Rougher level falls below the operating region then no connection exists between it and the Cleaner tank, and whereas before a change in the Rougher valve opening would affect the level of the Cleaner this would not occur anymore. Similarly, the tanks will overflow if the maximum levels are exceeded. Additional changes occur when the valve

inputs are saturated. The valve settings must thus be kept well inside their operating regions.

Less severe non-linearities exist too. The level probes and the valve characteristics are not perfectly linear. The flow from the tanks are functions of the height of water in them and the pumps are not perfect. Nonetheless, for small departures from a selected operating point, the behaviour can be approximated by a linear model.

If the system is kept near to this operating point a simplified linear model can describe the plant with sufficient accuracy. Obviously the plant will not always stay at this point and the success of a control scheme can be measured by its insensitivity to small deviations between the plant and its model.

2.4 THREE-STAGE CONTROL SCHEME

Flotation systems are usually controlled in three stages. During the first stage a start-up controller is applied to move the system into its operating region. A setpoint tracking controller is then inserted to control the levels and chemical balances. The third controller is used to initiate the shut down sequence as otherwise failures such as overflowing may occur.

2.5 BLACK-BOX IDENTIFICATION

The so-called Black-box identification procedure(9) is applied to determine the transfer function of the flotation rig by step test analysis. It is well known that feedback control does not require a very accurate model of the plant and a detailed examination of the maximum allowable

inaccuracies has been given by Donati(10). Further, it is widely accepted that a simple and reduced-order model is usually sufficient to design an appropriate control scheme.(2)

2.6 MODEL DETERMINATION

The flotation rig has four valve inputs. It is thus only possible to control four of the eight output quantities directly and so obtain a n -input, n -output model of the plant. The flow measurements, which are usually difficult to obtain in an industrial plant, are disregarded and the level measurements are taken as the plant outputs.

The transfer function relating the valve inputs $u(s)$ to the level outputs $y(s)$ is given by

$$y(s) = G(s) u(s), \quad (2.1)$$

with

$$\begin{aligned} y_1(s) &= \text{Rougher level,} \\ y_2(s) &= \text{Scavenger level,} \\ y_3(s) &= \text{Cleaner level,} \\ y_4(s) &= \text{Recleaner level} \end{aligned}$$

and

$$\begin{aligned} u_1(s) &= \text{Rougher tailings valve,} \\ u_2(s) &= \text{Scavenger tailings valve,} \\ u_3(s) &= \text{Cleaner tailings valve,} \\ u_4(s) &= \text{Recleaner tailings valve.} \end{aligned}$$

2.6.1 SINGLE-LOOP PI CONTROLLER

Singlevariable PI controllers were used to move the waterlevels y_i of the plant into their operating regions by adjusting the corresponding inputs u_i . These were necessary as it was exceedingly difficult to adjust the valves manually to obtain a stable operating point. This problem arose due to the high interaction between the various tanks making it difficult to predict the affect of changing a valve setting on the levels of the different tanks. As the PI controllers were ignorant of these interactions, their individual gains had to be chosen carefully to allow all levels to reach their operating points.

Although the plant can be considered to be open-loop stable, at least in the operating region, it was found that if the valve settings were not perfect the levels would slowly move out of the operating regions and some tanks would eventually run dry.

A single-loop PI controller $P(s)$ was designed by trial and error.

$$P(s) = \frac{1}{10s} \begin{bmatrix} 2s+2 & 0 & 0 & 0 \\ 0 & 5s+5 & 0 & 0 \\ 0 & 0 & 6s+6 & 0 \\ 0 & 0 & 0 & 3s+3 \end{bmatrix} \quad (2.2)$$

This controller was used to move the levels to their operating levels, at which point the valve settings were fixed and the plant was given time to attain steady state. The step tests could then be performed by changing the valve settings by a specific amount.

CHAPTER 2 THE FLOTATION RIG

Even with the use of the controller, it was found that depending on the moment when the inputs were fixed, the levels would sometimes still drift out of the operating regions. The reason for this was that the valve inputs were not stationary at the time when they were clamped as the PI controller's gain was large enough such that the measurement noise was transmitted to the inputs. Reducing the gain however was not an acceptable decision as it took approximately 10 minutes for the plant to reach the desired levels and decreasing the gain would have made the time even longer. Once the valve settings had been fixed, a further 10 minutes was required to allow the tank to attain steady-state.

The above difficulties could be partially eliminated by using a non-linear PI controller as applied in a previous project(11), where the controller gain is reduced as the levels near their setpoints. This approach was unnecessary in the case of the laboratory rig, where the time involved to obtain step tests was not critical.

The manual valve setting for the main feed was also critical. If the flow into the flotation circuit was too little then the valves would be virtually closed and the levels would drop below their operating region. If alternatively the flow was too high then the valves would be completely open and the tanks would eventually overflow. The tolerance of the valve setting for the main feed was found to be extremely small.

2.6.2 STEP TEST PROCEDURE

During the step tests, which took about 10 minutes, the plant had to remain in its operating region to prevent large

CHAPTER 2 THE FLOTATION RIG

changes in the model, for reasons discussed previously. It was also important that the plant had attained steady-state before a step is applied. Otherwise the step responses would be distorted, if the levels were drifting prior to the time of the step change.

The fixed valves for the pumps of Sump A and Sump B were opened sufficiently such that no water would accumulate in them, otherwise they would act as storage devices and change the model.

A large number of step-tests for each valve had to be performed such that an optimal step size could be found. If the step size was too small, no response could be detected due to the valve characteristics and because the level measurements are contaminated by noise. If however, the step size was too large, then the levels would move out of their operating regions and invalidate the assumption of linearity.

In Table 2.1 selected step tests with their corresponding step size in percent are listed. The percentage closing was calculated from:

$$\text{Percent closing} = \frac{u_t - u_0}{4096} \times 100\% \quad (2.3)$$

where u_0 is the initial valve setting and u_t is the final setting.

Step test No.	Valve stepped	Percentage closing
1.a)	Rougher	-5%
b)	"	10%
c)	"	-20%
d)	"	25%
e)	"	20%
f)	"	-20%
2.a)	Scavenger	-5%
b)	"	10%
c)	"	10%
d)	"	-20%
3.a)	Cleaner	5%
b)	"	-9%
c)	"	15%
d)	"	15%
e)	"	-10%
4.a)	Recleaner	10%
b)	"	-20%
c)	"	30%
d)	"	20%
e)	"	-30%

Table 2.1 Selected list of experiments

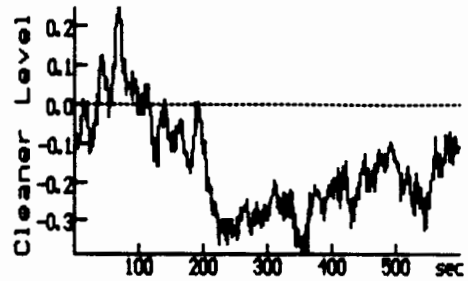
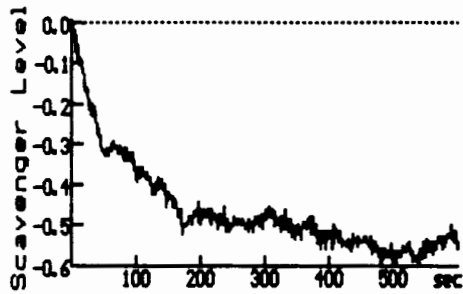
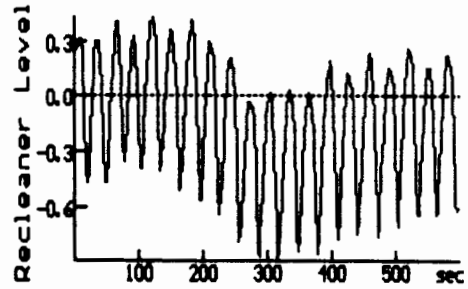
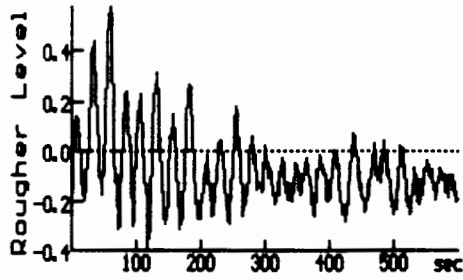
The tests were performed and the results were normalised such that they could be compared with each other and a transfer function could be fitted to them. Normalisation is achieved by subtracting the initial level from the readings and dividing the result by the step size ($u_t - u_0$). The resulting plots then correspond to a system with zero initial conditions and a step size of +1 units (i.e. opening the valve by 1 unit).

2.6.2.1 Step Test Results

The normalised responses are shown in the following pages.
The original data is contained in Appendix A.

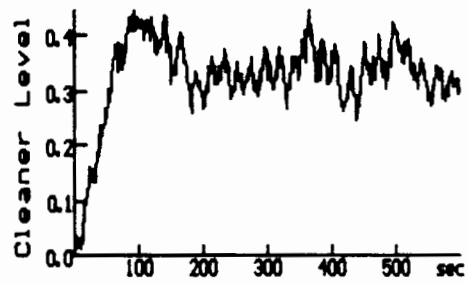
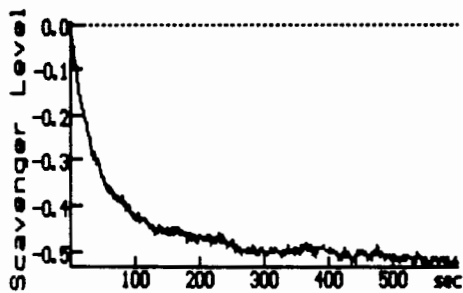
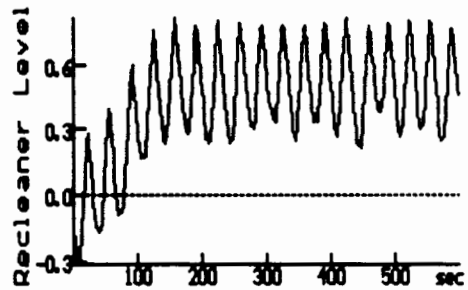
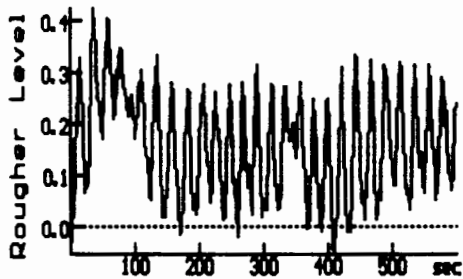
Flotation System Open-Loop Step Response

Test 1a) Rougher Step Size Normalised



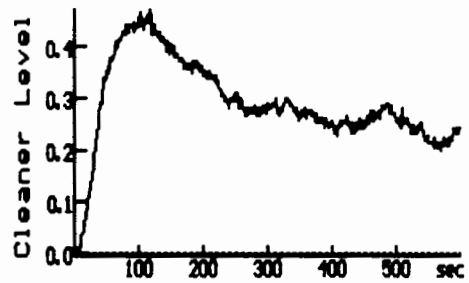
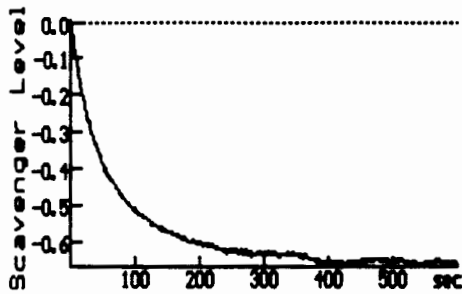
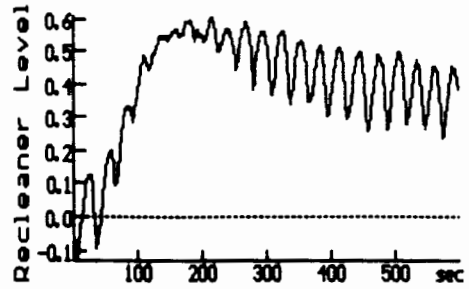
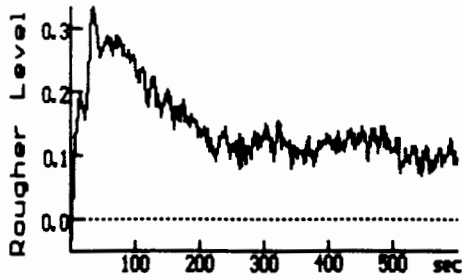
Flotation System Open-Loop Step Response

Test 1b) Rougher Step Size Normalised



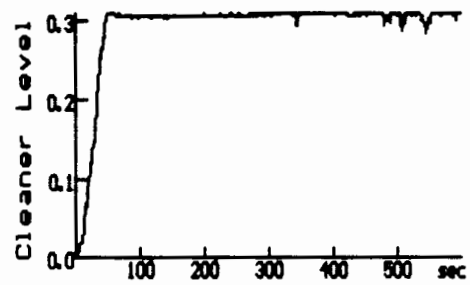
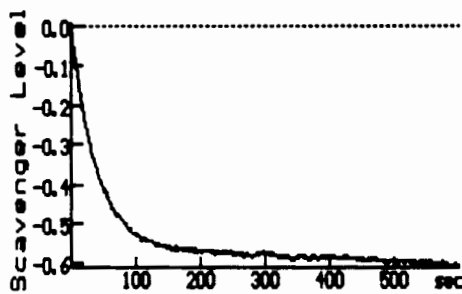
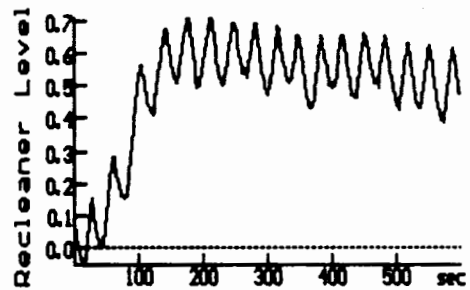
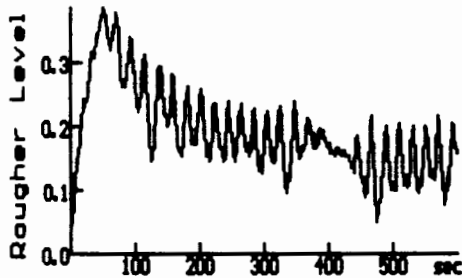
Flotation System Open-Loop Step Response

Test 1c) Rougher Step Size Normalised



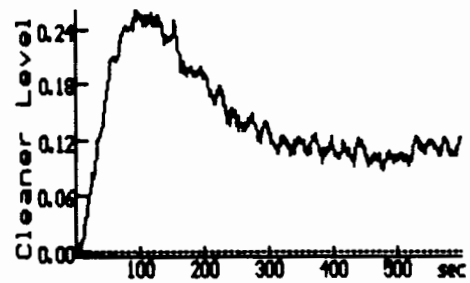
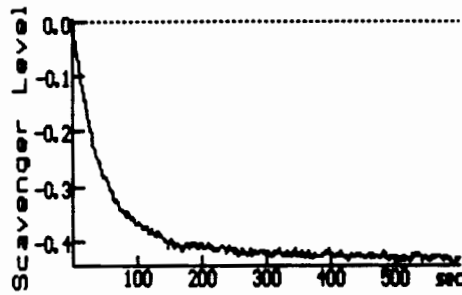
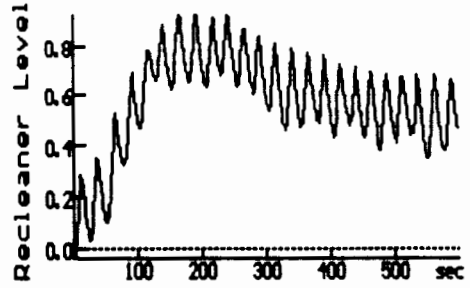
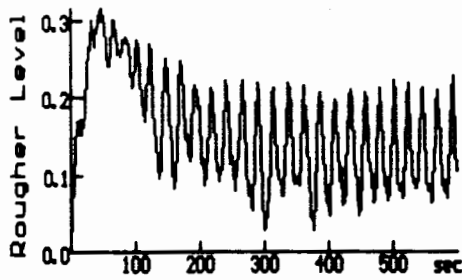
Flotation System Open-Loop Step Response

Test 1d) Rougher Step Size Normalised



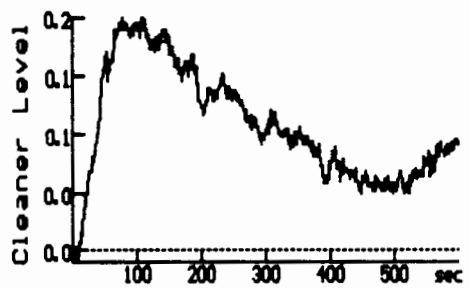
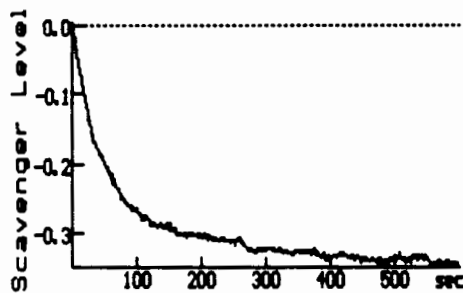
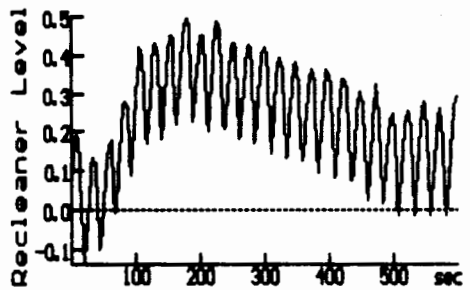
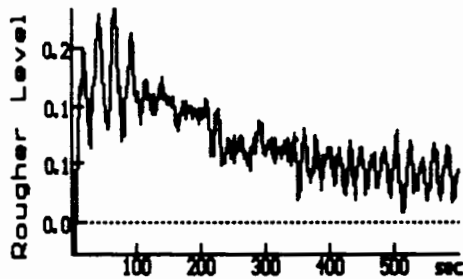
Flotation System Open-Loop Step Response

Test 1e) Rougher Step Size Normalised



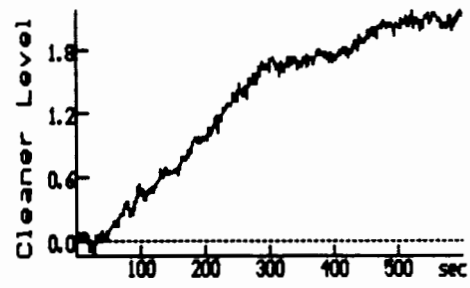
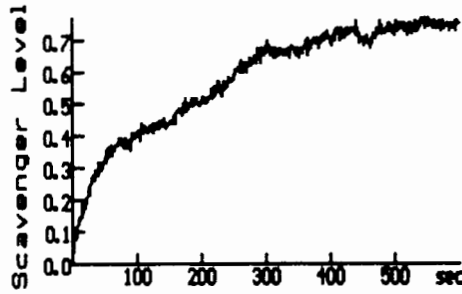
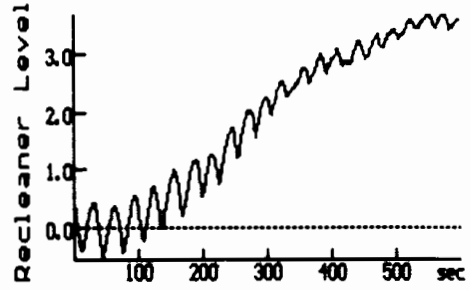
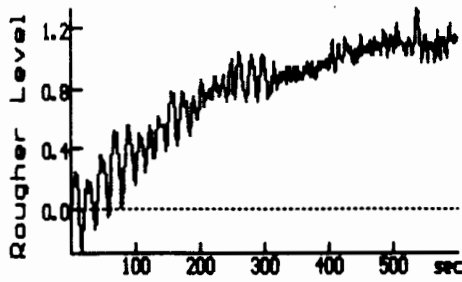
Flotation System Open-Loop Step Response

Test 1f) Rougher Step Size Normalised



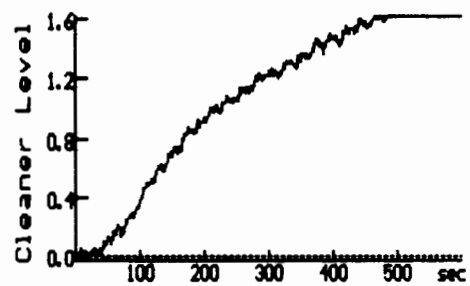
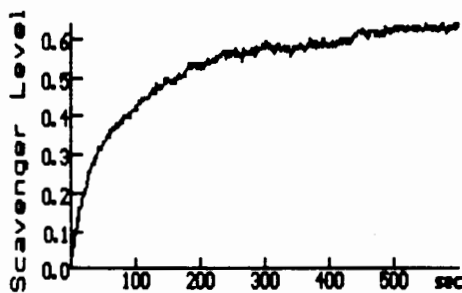
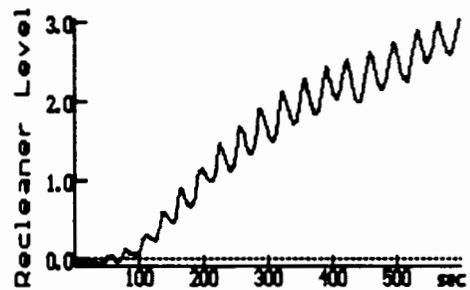
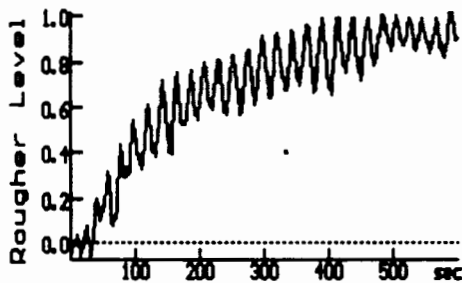
Flotation System Open-Loop Step Response

Test 2a) Scavenger Step Size Normalised



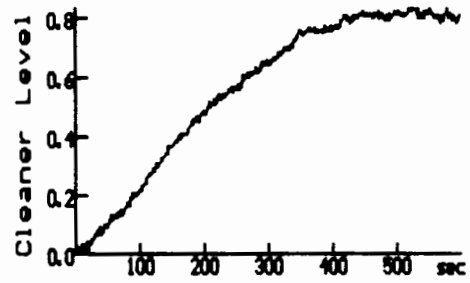
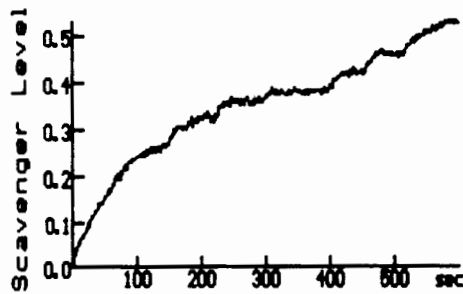
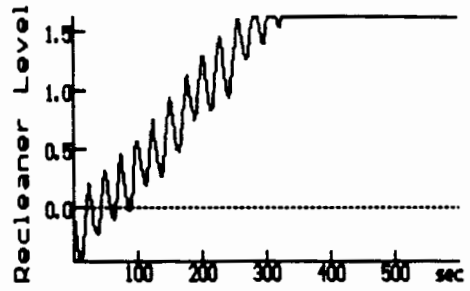
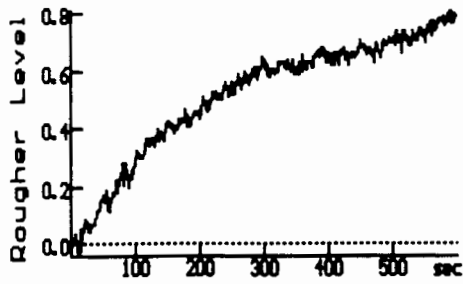
Flotation System Open-Loop Step Response

Test 2b) Scavenger Step Size Normalised



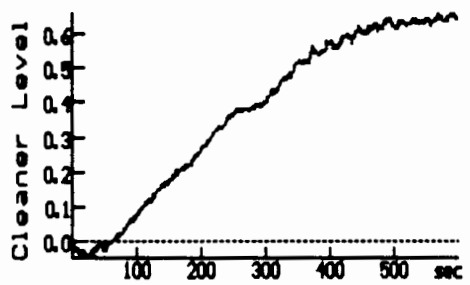
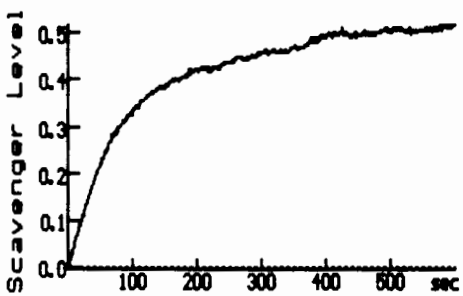
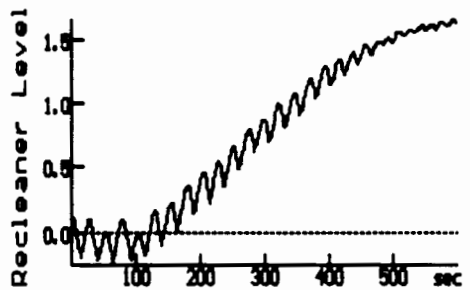
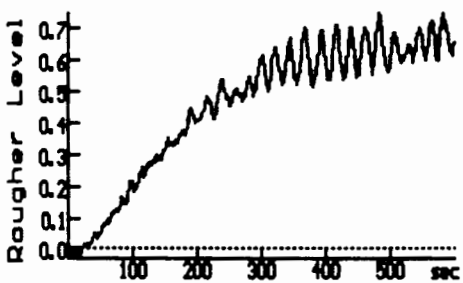
Flotation System Open-Loop Step Response

Test 2c) Scavenger Step Size Normalised



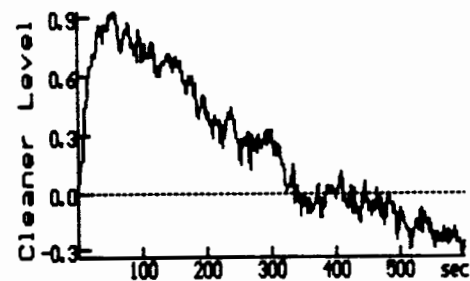
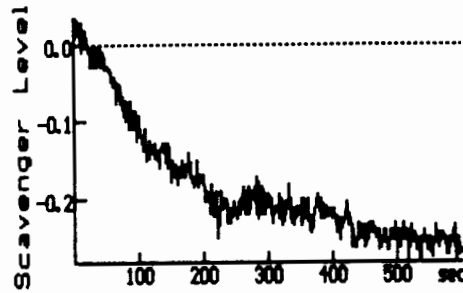
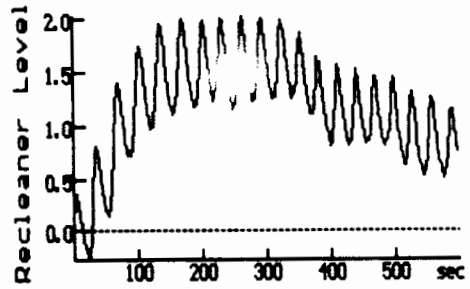
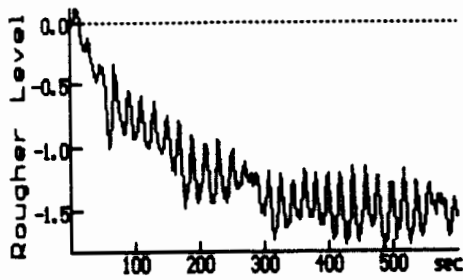
Flotation System Open-Loop Step Response

Test 2d) Scavenger Step Size Normalised



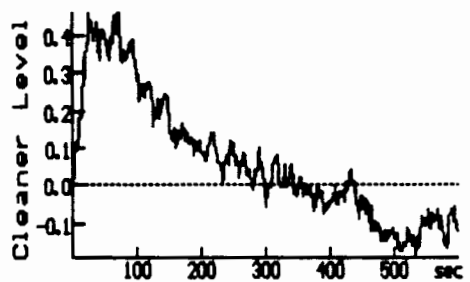
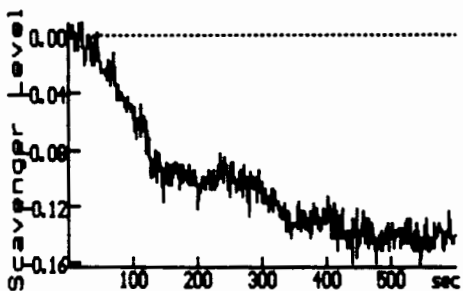
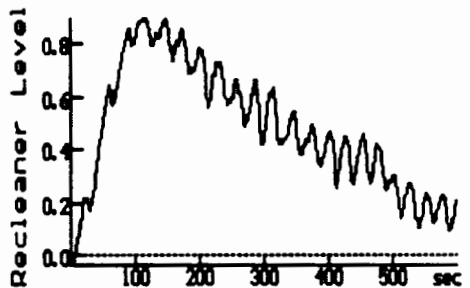
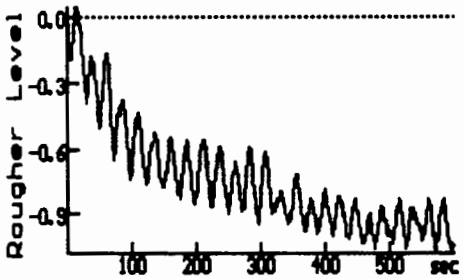
Flotation System Open-Loop Step Response

Test 3a) Cleaner Step Size Normalised



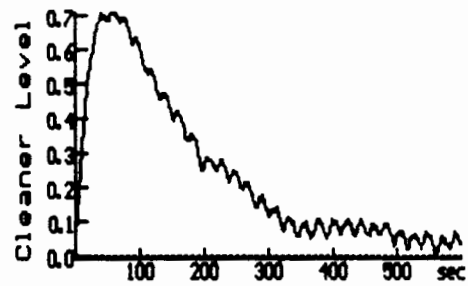
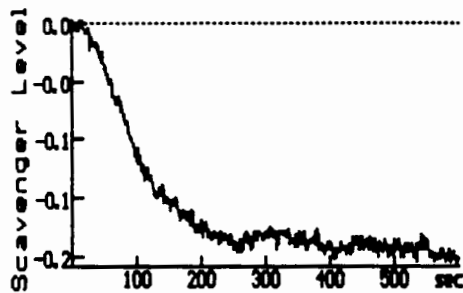
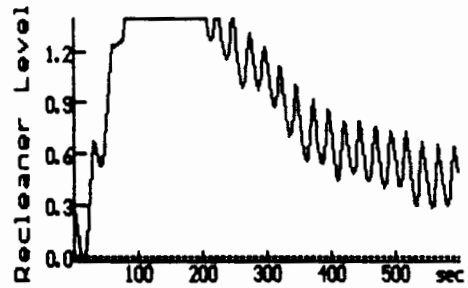
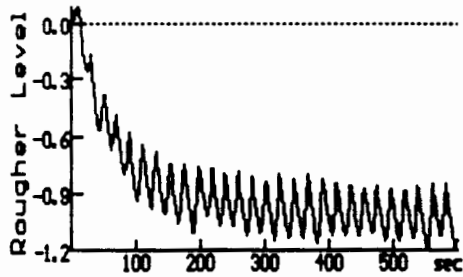
Flotation System Open-Loop Step Response

Test 3b) Cleaner Step Size Normalised



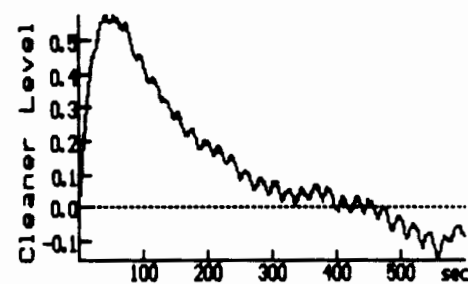
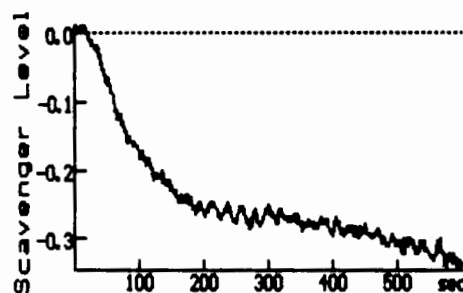
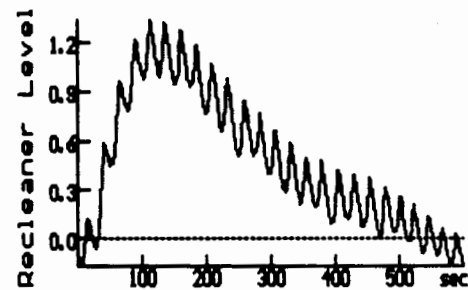
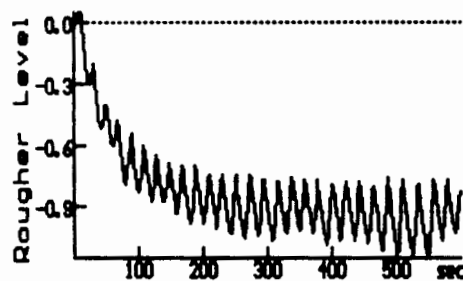
Flotation System Open-Loop Step Response

Test 3c) Cleaner Step Size Normalised



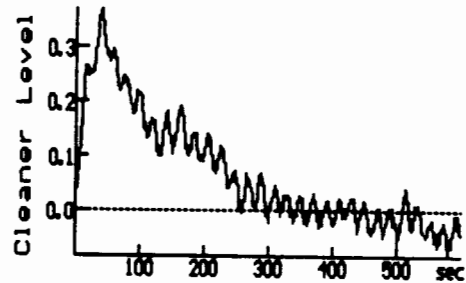
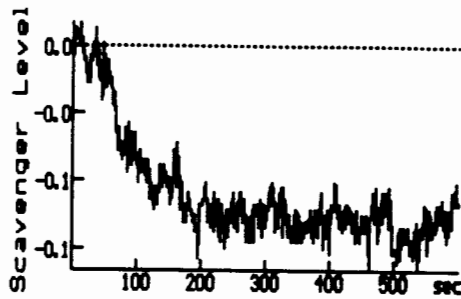
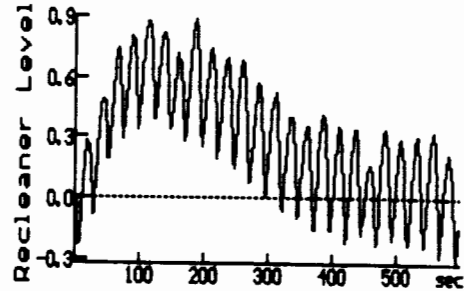
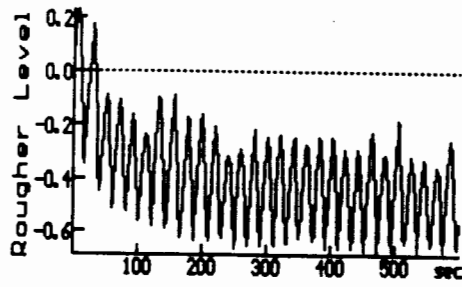
Flotation System Open-Loop Step Response

Test 3d) Cleaner Step Size Normalised



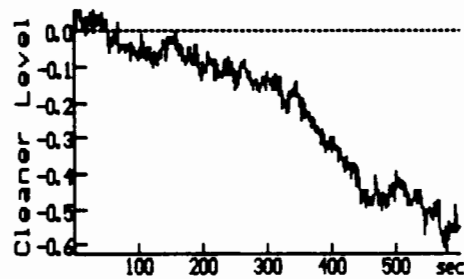
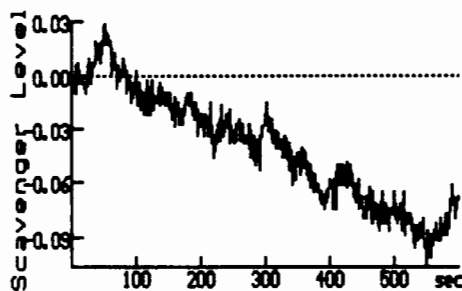
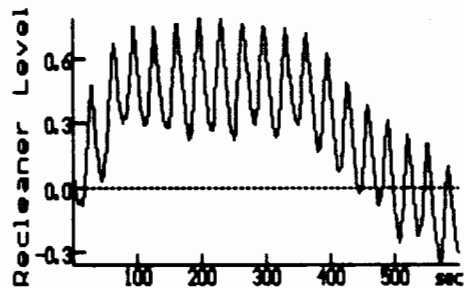
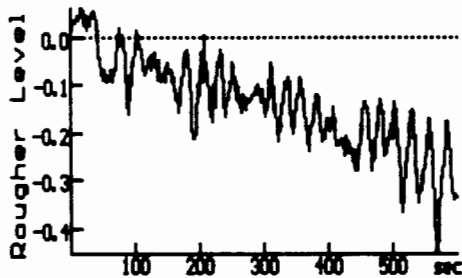
Flotation System Open-Loop Step Response

Test 3e) Cleaner Step Size Normalised



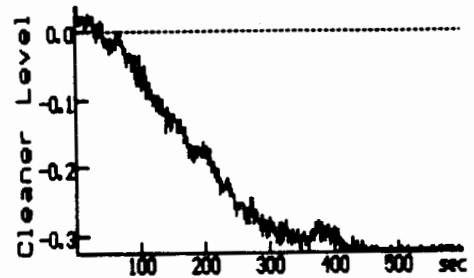
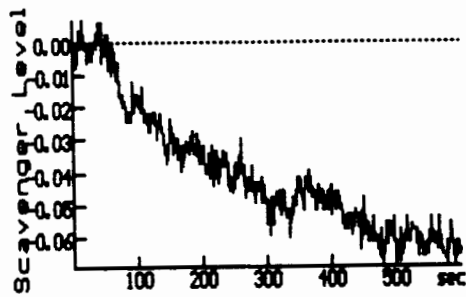
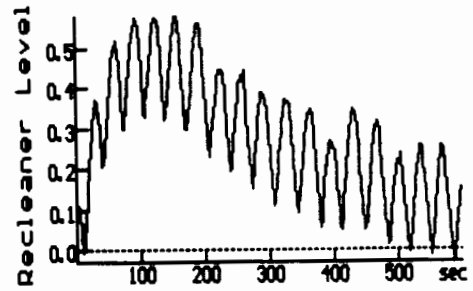
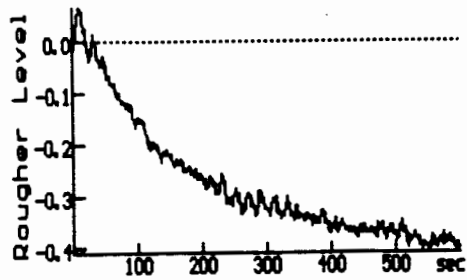
Flotation System Open-Loop Step Response

Test 4a) Recleaner Step Size Normalised



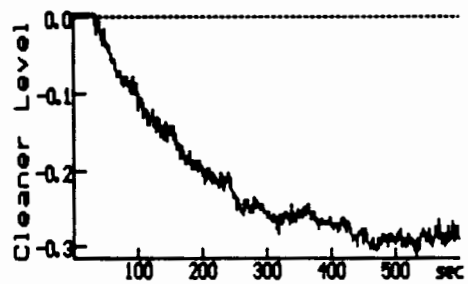
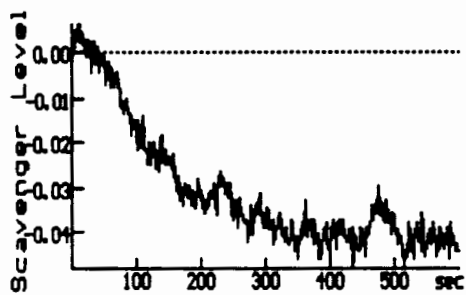
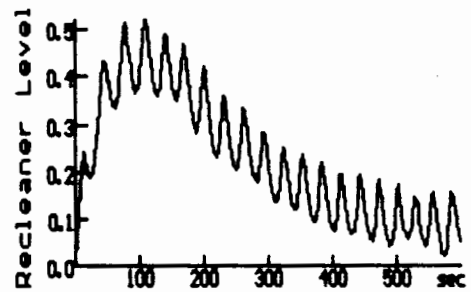
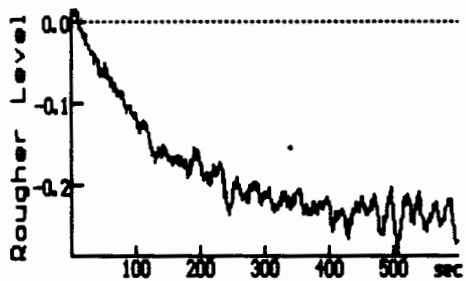
Flotation System Open-Loop Step Response

Test 4b) Recleaner Step Size Normalised



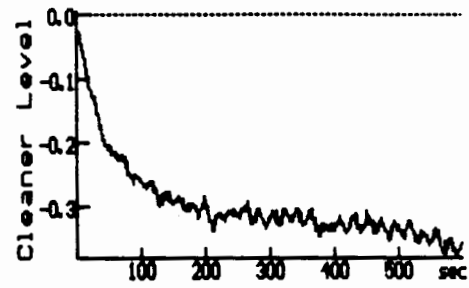
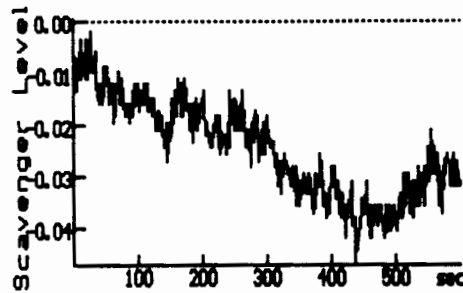
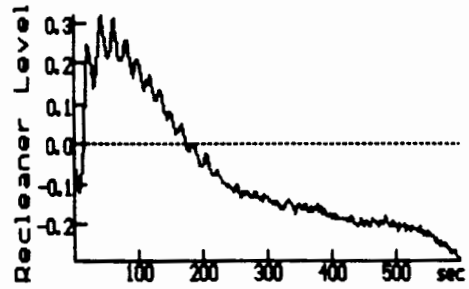
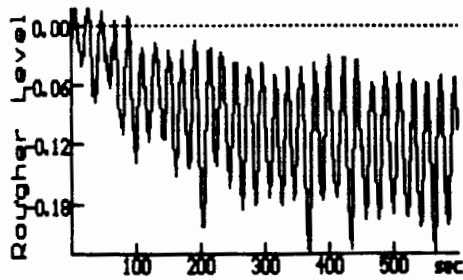
Flotation System Open-Loop Step Response

Test 4c) Recleaner Step Size Normalised



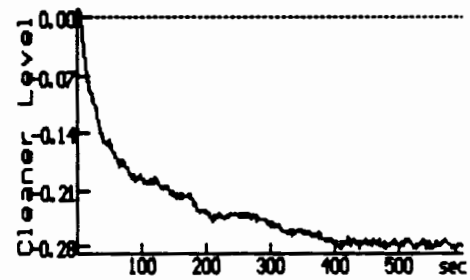
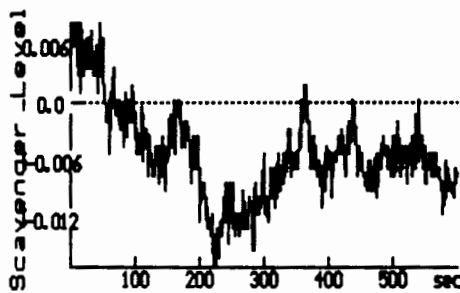
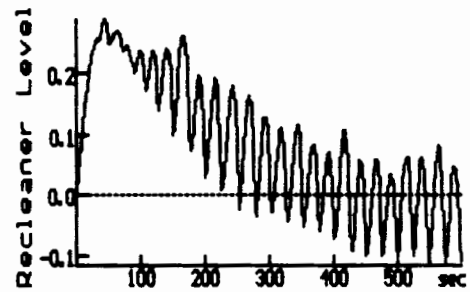
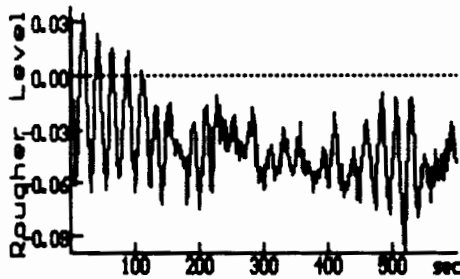
Flotation System Open-Loop Step Response

Test 4d) Recleaner Step Size Normalised



Flotation System Open-Loop Step Response

Test 4e) Recleaner Step Size Normalised



2.6.2.2 Selecting Responses

Table 2.2 lists the step responses, which best characterised the behaviour of the plant to the different step inputs. These responses are then used to fit transfer functions to them.

Valve stepped	Response used
Rougher	Test 1.c)
Scavenger	Test 2.d)
Cleaner	Test 3.d)
Recleaner	Test 4.b)'

'As the Cleaner level response of Test 4.b) was saturated, it was replaced with that of Test 4.d).

Table 2.2 Step tests used to fit transfer functions

2.6.2.3 Fitting Transfer Functions

The sinusoidal variations of Rougher and Recleaner levels were caused by the pumps cavitating as the Sump tanks were emptied. This behaviour is not included in the mathematical model.

The step responses of a single output $y(s)$ is given by

$$y(s) = g(s) u(s) \tag{2.4}$$

with $u(s) = s^{-1}$ corresponding to a step input.

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The transfer functions $g(s)$ could be divided into three basic types, summarised as follows:

$$g(s) = \frac{a}{s+b} e^{-\tau s} \quad (\text{First order}) \quad (2.5)$$

$$g(s) = \frac{a}{s+bs+c} e^{-\tau s} \quad (\text{Second order, no zero}) \quad (2.6)$$

$$g(s) = \frac{as+b}{s+cs+d} e^{-\tau s} \quad (\text{Second order with zero}), \quad (2.7)$$

where τ corresponds to a pure time delay in seconds and s is in rad/sec.

To fit a particular function to a response, the initial coefficients are selected by trial and error. Once a reasonable correspondence is achieved, the coefficients are optimised with a nonlinear parameter adjustment technique [see NELM in the *Software Reference*].

2.6.3 FLOTATION RIG TRANSFER FUNCTION

The above method is applied and the resulting transfer function modelling the flotation rig are found to be:

(units of s are in rad/sec)

$$g_{1,1}(s) = \frac{1.40E-2 s + 6.83E-5}{s^2 + 3.95E-2 s + 5.91E-4} \quad (2.6a)$$

$$g_{1,2}(s) = \frac{1.53E-4}{s^2 + 4.07E-2 s + 2.20E-4} \quad (2.6b)$$

$$g_{1,3}(s) = \frac{-2.00E-2}{s + 2.08E-2} e^{-10s} \quad (2.6c)$$

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$$g_{1,4}(s) = \frac{-3.02E-3}{s + 7.58E-3} e^{-20s} \quad (2.6d)$$

$$g_{2,1}(s) = \frac{-1.22E-2}{s + 1.87E-2} \quad (2.6e)$$

$$g_{2,2}(s) = \frac{5.97E-3}{s + 1.19E-2} \quad (2.6f)$$

$$g_{2,3}(s) = \frac{-4.05E-3}{s + 1.37E-2} e^{-20s} \quad (2.6g)$$

$$g_{2,4}(s) = \frac{-4.95E-4}{s + 8.13E-3} e^{-40s} \quad (2.6h)$$

$$g_{3,1}(s) = \frac{1.66E-2 s + 9.69E-5}{s^2 + 3.40E-2 s + 3.81E-4} e^{-10s} \quad (2.6i)$$

$$g_{3,2}(s) = \frac{1.27E-4}{s^2 + 4.33E-2 s + 1.61E-4} e^{-30s} \quad (2.6j)$$

$$g_{3,3}(s) = \frac{6.45E-2 s - 1.31E-5}{s^2 + 9.66E-2 s + 6.47E-4} \quad (2.6k)$$

$$g_{3,4}(s) = \frac{-7.10E-3}{s + 2.16E-2} \quad (2.6l)$$

$$g_{4,1}(s) = \frac{1.44E-2 s + 7.80E-5}{s^2 + 2.50E-2 s + 1.94E-4} e^{-40s} \quad (2.6m)$$

$$g_{4,2}(s) = \frac{2.95E-4}{s^2 + 3.79E-2 s + 1.57E-4} e^{-100s} \quad (2.6n)$$

$$g_{4,3}(s) = \frac{3.15E-2 s + 2.24E-5}{s^2 + 1.92E-2 s + 1.74E-4} e^{-20s} \quad (2.6o)$$

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$$g_{4,4}(s) = \frac{1.84E-2 s + 1.14E-5}{s^2 + 3.08E-2 s + 1.41E-4} \quad (2.6p)$$

where $g_{ij}(s)$ are in units of [%Level / %Valve Setting].

The similarity of the simulated and the actual step responses can be seen in Figs. 2.3 - 2.6.

Actual / Simulated Open-Loop Step Response
Rougher Step Size Normalised

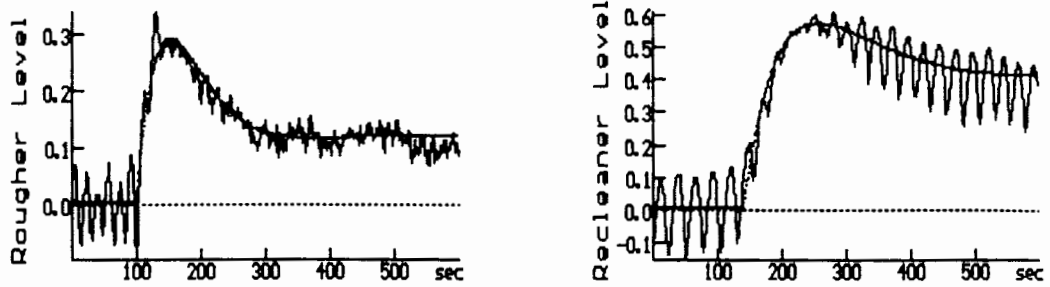
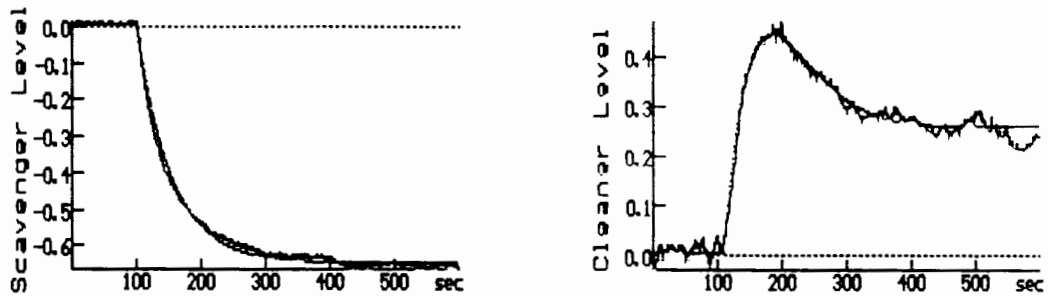


FIG. 2.3



Actual / Simulated Open-Loop Step Response
Scavenger Step Size Normalised

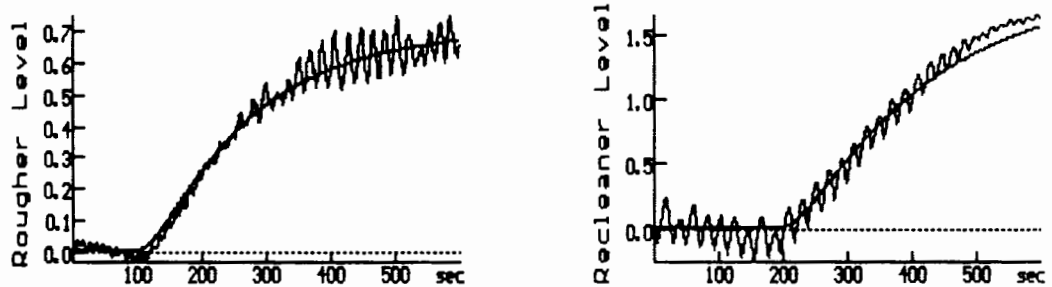
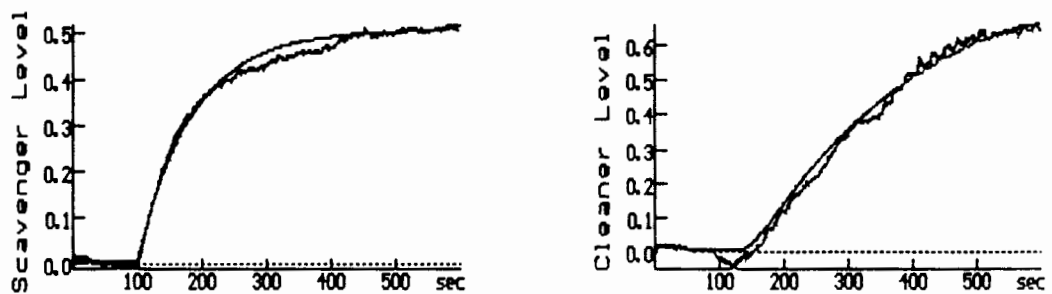


FIG. 2.4



Actual / Simulated Open-Loop Step Response
Cleaner Step Size Normalised

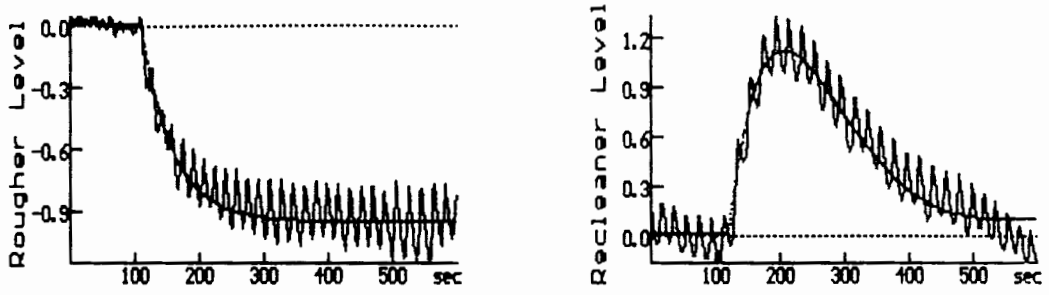
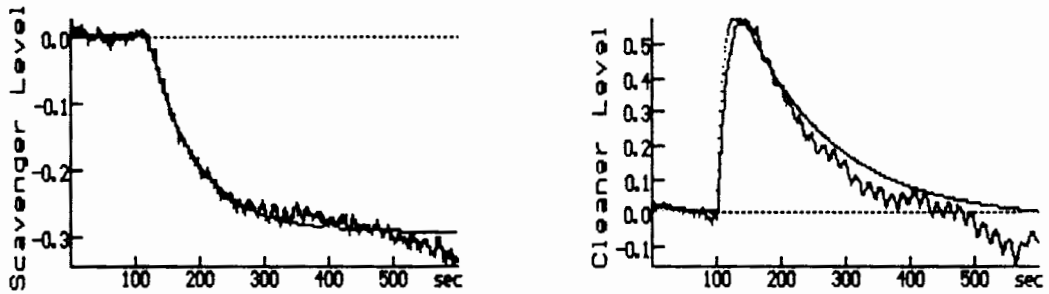


FIG. 2.5



Actual / Simulated Open-Loop Step Response
Recleaner Step Size Normalised

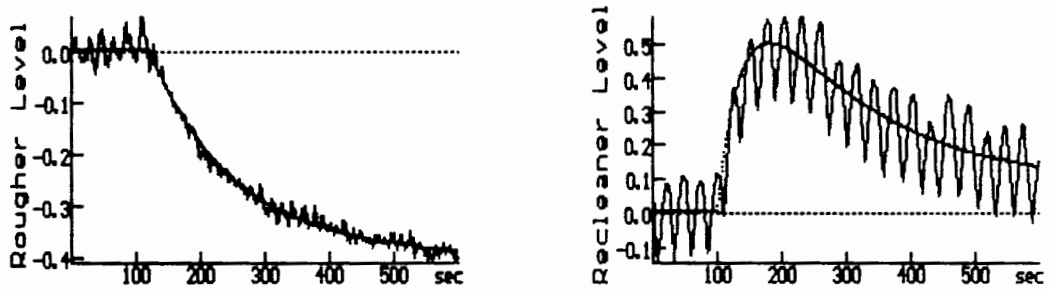
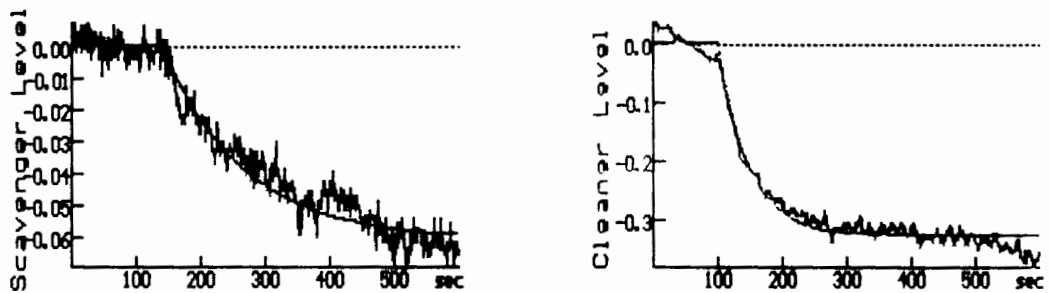


FIG. 2.6



2.6.4 TWO-TANK SYSTEM MODEL

Instead of using the full flotation circuit as a practical example for the succeeding discussions on the Inverse Nyquist and the Pole Assignment techniques, a subsystem was used instead to simplify the analysis. The flotation system is of order 4, which will pose problems in the application of both methods, as the system can be considered to be of high order. Since any design procedure will become very cumbersome as the process order becomes large, it is sufficient to use a subsystem of the flotation rig to apply and compare the two techniques and only briefly mention the difficulties with large order systems.

The transfer function of the two-tank sub-system with two inputs and two outputs contains the Rougher and Scavenger tank model, only and the valves of the other two tanks are fixed, i.e.

$$u_3(s) = u_4(s) = 0. \quad (2.7)$$

The new model will be given by

$$y(s) = G(s) u(s) \quad (2.8)$$

where y and u are 1×2 vectors and $g_{ij}(s)$ (for $i=1,2$ and $j=1,2$) are given by Eqs. (2.6).

2.7 CONCLUSION

This chapter has demonstrated how the transfer function of the flotation rig was established by step response analysis,

CHAPTER 2 THE FLOTATION RIG

with special care taken to limit the inherent nonlinearities.

This type of identification can be performed on most industrial systems and usually results in a satisfactory mathematical model, which can then be used to develop a control scheme.

CHAPTER 2 THE FLOTATION RIG

3. THE INVERSE NYQUIST ARRAY TECHNIQUE

3.1 INTRODUCTION

The Inverse Nyquist Array (INA) design technique is discussed in this chapter. The general model of a multivariable plant is developed in the frequency domain. A short discussion on diagonal systems is given to demonstrate the fundamentals of the INA technique.

The concept of diagonal dominance is derived to apply the Nyquist stability criterion on multivariable systems. Details of achieving dominance are presented. Finally it is shown how singlevariable techniques are applied to design single-loop controllers to complete the control scheme.

3.2 MODELS FOR THE INVERSE NYQUIST ARRAY METHOD

3.2.1 SYSTEM MODEL

In the discussion on the INA technique a system description, similar to that of Rosenbrock(3,12), is used here. The model is described by the transfer function notation, because the INA method is applied in the frequency domain. If the system is given by state space equations, it has to be converted into the corresponding transfer function first [see Section 1.7.2].

In industrial applications, where the plant dynamics cannot easily be described by differential equations, a black-box identification of the plant by step response analysis is necessary. This approach was used on the flotation rig [see Section 2.6] and led to a transfer function model, which could then directly be used for the INA technique.(2)

A block diagram of a linear, time-invariant feedback control system is shown in fig. 3.1, where the plant has n inputs and n outputs and is modelled by a $n \times n$ transfer function matrix $G(s)$. The number of inputs must equal the number of outputs such that n individual feedback loops can be constructed as noted in section 1.5.1. The n individual feedback paths are joined to simplify the block diagram in Fig. 3.1.

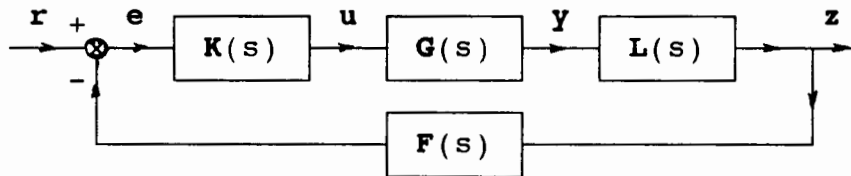


Fig. 3.1 Multivariable control system representation

The inputs and outputs of the plant model $G(s)$ are represented by vectors u and y respectively. The vector r contains the required setpoint values, e the comparator output and vector z is the system output. All the above vectors have n elements.

The matrices $K(s)$ and $L(s)$ are termed the pre- and post-controllers respectively. The feedback matrix is denoted by $F(s)$. All the matrices used have dimension $n \times n$.

3.2.2 MODEL RESTRICTIONS

Various restrictions are imposed on the system matrices thus simplifying analysis of the control scheme.

The plant model $\mathbf{G}(s)$ should be strictly proper, i.e.

$$\lim_{s \rightarrow \infty} \mathbf{g}_{ij}(s) = 0 \quad (3.1)$$

and must be of least order, then

$$|\mathbf{G}(s)| \neq 0 \quad (3.2)$$

The post-controller matrix $\mathbf{L}(s)$ should be diagonal, i.e with off-diagonal elements = 0, because for most applications the system outputs are to be controlled independently from each other. In addition, the matrix $\mathbf{L}(s)$ is in most cases kept independent of s , such that the system output remains the controlled variable.

Similarly, the feedback matrix $\mathbf{F}(s)$ is kept diagonal and independent of s , such that a direct relationship exists between the setpoint values and output variables. In the analysis of the closed-loop system, the open-loop gains of the individual loops are inserted into the diagonal elements \mathbf{f}_i .

The system integrity can also be simulated by setting some or all the $\mathbf{f}_i=0$. It is then relatively easy to predict the system behaviour under fault conditions.

By restricting both matrices $\mathbf{L}(s)$ and $\mathbf{F}(s)$ to be diagonal and constant it can be shown that the constants l_i of $\mathbf{L}(s)$ can be moved into the matrix $\mathbf{K}(s)$ by multiplying the i th column of $\mathbf{K}(s)$ by l_i . This would eliminate the need for a matrix $\mathbf{L}(s)$ with its restrictions in the control system

scheme. But to keep the design of the control system more general it is nevertheless included.

The restrictions governing the matrix $\mathbf{K}(s)$ are the following. Because of the eventual inclusion of $\mathbf{K}(s)$ in the plant by electronic (analog or digital) means the elements $k_{ij}(s)$ must be realizable, i.e. proper and stable. If the elements are not strictly proper, care must be taken that they do not impede the system performance by amplifying high frequency noise.

3.2.3 SYSTEM EQUATIONS

The open-loop transfer function of the above multivariable system, relating the output vector \mathbf{z} to the input setpoint vector \mathbf{r} , is denoted by \mathbf{Q} , then

$$\mathbf{Q} = \mathbf{L}\mathbf{G}\mathbf{K} \quad (3.3)$$

Using \mathbf{H} to denote the corresponding closed loop system then

$$\mathbf{H} = (\mathbf{I}_n + \mathbf{Q}\mathbf{F})^{-1} \mathbf{Q} \quad (3.4)$$

and the inverse relationship follows with

$$\mathbf{H}^{-1} = \mathbf{Q}^{-1} + \mathbf{F} \quad (3.5)$$

if \mathbf{Q}^{-1} exists.

From the above relationship it follows that if the system analysis is directed toward using \mathbf{Q}^{-1} instead of \mathbf{Q} then the transformation to the closed loop system is a simple one, namely an addition of \mathbf{F} .

3.2.4 CONTROLLABILITY

The restriction that \mathbf{Q}^{-1} must exist implies that the plant model transfer function matrix $\mathbf{G}(s)$ must be controllable and the choice of both the matrices $\mathbf{K}(s)$ and $\mathbf{L}(s)$ are not allowed to impede the controllability of $\mathbf{Q}(s)$, i.e.

$$|\mathbf{G}(s)| \neq 0$$

$$|\mathbf{K}(s)| \neq 0$$

and

$$|\mathbf{L}(s)| \neq 0 \tag{3.6}$$

Although this constraint manifests itself from the mathematical derivation, it is important for practical reasons. If for example a specific choice of $\mathbf{K}(s)$ with $|\mathbf{K}(s)| = 0$ is used then the individual loops of the multivariable system are no longer linearly independent and the individual system outputs cannot be controlled independently any more. Therefore the system order must be reduced before a control scheme can be developed. It is therefore obvious to keep both $|\mathbf{K}(s)|$ and $|\mathbf{L}(s)| \neq 0$.

The plant model $\mathbf{G}(s)$ should have least order from outset and controllable [see Eqn.3.2], thus eliminating the problem of $|\mathbf{G}(s)| = 0$.

3.3 DIAGONAL SYSTEMS

The basic aim of the INA method is to design the matrix \mathbf{K} and \mathbf{L} such that the matrix \mathbf{Q} becomes diagonal. This process is referred to as decoupling of the plant \mathbf{G} . Although matrix \mathbf{L} could be used to decouple the plant by column operations on $\mathbf{G}(s)$ in general, this approach will not be applied in

CHAPTER 3 THE INVERSE NYQUIST ARRAY TECHNIQUE

this discussion, because of the restrictions imposed on \mathbf{L} previously.

If the open-loop transfer matrix \mathbf{Q} is diagonal then the multivariable system can be split into n independent singlevariable feedback systems. Controllers can then be developed by singlevariable techniques and inserted into the individual loops to complete the control scheme.

In addition, well established singlevariable methods can be applied to diagonal systems to determine stability of the various loops of \mathbf{H} . If the individual loops are stable, it can be stated without restriction that the multivariable system will be stable.

This discussion has shown that multivariable system design can be greatly simplified if the system is made diagonal, because then only singlevariable techniques need to be applied. This observation is the foundation on which the INA method is based. The multivariable system is transformed into a number of singlevariable systems.

3.4 THE CONCEPT OF DIAGONAL DOMINANCE

From the discussion above it is evident that a matrix \mathbf{K} such that

$$\mathbf{K}(s) = \mathbf{G}^{-1}(s) \quad (3.7)$$

would make the system diagonal. But due to the restrictions imposed on \mathbf{K} in section 3.2.2, the matrix of Eqn.(3.7) will seldom be realizable. To decouple a plant completely is not possible for most applications and a more generalised approach has to be developed.

CHAPTER 3 THE INVERSE NYQUIST ARRAY TECHNIQUE

The concept of diagonal dominance was introduced by Rosenbrock(3) to relax the requirement that the system must be completely decoupled, before singlevariable techniques can be applied.

The mathematical definition of diagonal dominance is as follows:

A matrix $\mathbf{Q}(s)$ is diagonally row dominant if and only if

$$|q_{ii}(s)| - \sum_{\substack{j=1 \\ j \neq i}}^n |q_{ij}(s)| > 0 \text{ for } i=1,2..n \quad (3.8)$$

and column dominant if and only if

$$|q_{jj}(s)| - \sum_{\substack{i=1 \\ i \neq j}}^n |q_{ij}(s)| > 0 \text{ for } j=1,2..n. \quad (3.9)$$

A matrix \mathbf{Q} is diagonally dominant if it is either row or column dominant for all relevant s values.

The concept of dominance can be regarded as a measure of coupling between different inputs and outputs of a system. A diagonally dominant multivariable system has the property, that the interaction from the off-diagonal elements will not impair the stability of the diagonal elements and the stability of the multivariable system can be determined by the application of the extended Nyquist stability criterion on the diagonal elements.

3.4.1 GRAPHICAL INTERPRETATION

Nyquist diagrams are drawn for all $n \times n$ elements $q_{ij}(s)$ of matrix $\mathbf{Q}(s)$ by setting $s=jw$ and $0 \leq w \leq \infty$. The real parts of s can be excluded to determine stability because $\mathbf{Q}(s)$ is

assumed to be strictly proper.(3) In addition, it is sufficient for w to range from zero to w_{\max} , where w_{\max} is about 10 times the fastest pole of a plant. The plot so obtained is referred to as a Nyquist Array diagram.

3.4.2 GERSHGORIN BANDS

The mathematical test for diagonal dominance of a matrix Q (Eqs. (3.8) & (3.9)) can easily be performed by the following graphical construction on the Nyquist Array diagram.

To check for row diagonal dominance, a circle of radius

$$d_i(s) = \sum_{\substack{j=1 \\ j \neq i}}^n |q_{ij}(s)| \quad (3.10)$$

with centre at $q_{ii}(s)$ for each frequency w is drawn for $i=1,2..n$.

If w moves from 0 to w_{\max} in sufficiently small steps, an envelope, tangential to the circles can be drawn for each diagonal element. These regions are then referred to as the Gershgorin bands.

If the bands do not include the origins $(0, j0)$, then $Q(s)$ is row dominant.

A similar construction can be made to determine column dominance. In that case the radii of the circles are calculated from:

$$d'_j(s) = \sum_{\substack{i=1 \\ i \neq j}}^n |q_{ij}(s)| \quad (3.11)$$

At any operating point of $\mathbf{Q}(s)$ the actual Nyquist diagram will lie within that band. If $\mathbf{Q}(s)$ is dominant then stability, gain and phase margins can be determined from these 'fuzzy' Nyquist plots by similar methods as applied to singlevariable systems.

The bands can be constructed for $\mathbf{Q}^{-1}(s)$, by substituting i th, j th element of $\mathbf{Q}^{-1}(s)$, i.e. $\hat{q}_{ij}(s)$ for $q_{ij}(s)$ in Eqs. (3.10) & (3.11).

3.4.3 EXTENDED NYQUIST STABILITY CRITERION

3.4.3.1 Direct Nyquist

If the matrix $\mathbf{Q}(s)$ is diagonally dominant, the closed-loop system with feedback matrix \mathbf{F} is stable if and only if the bands encircle and do not enclose the critical point $(-\mathbf{f}_i^{-1}, j0)$, N_i times with

$$N_i = -p_0 \quad (3.12)$$

where p_0 is the number of unstable open-loop poles.

If the plant is open-loop stable then p_0 is zero. The closed-loop system is then stable if the band passes the critical point on the right.

3.4.3.2 Inverse Nyquist

If the matrix $\mathbf{Q}^{-1}(s)$ is diagonally dominant, then the closed-loop system is stable if and only if the bands encircle and do not enclose the critical points $(-\mathbf{f}_i, j0)$, N_i times and the origin N_j times such that

$$N_i + N_j = -p_o \quad (3.13)$$

where p_o is the number of unstable open-loop poles.

If p_o is zero, then the multivariable system will be stable if the bands encircle the critical point and the origin the same number of times. In most situations it is sufficient if the bands do not intersect the real axis to the left of the origin and to the right of the critical points.

The critical points $(f_i^{-1}, j0)$ or $(f_i, j0)$ must lie to the left of the origin, because the theory is applied to negative feedback system only.

3.4.4 GAIN MARGINS

The margins of stability of the loop gains f_i can be easily determined from either the Nyquist or Inverse Nyquist Array diagram by the application of the above stability criteria.

The regions of f_i in which the closed-loop systems will remain stable is referred to as the gain space, which can be drawn for systems of order 2, i.e. two inputs and two outputs.(3) This area can then be used to check system integrity and it gives an indication of the maximum allowable variation in open-loop gain.

If the loop gains remain in these regions, the closed-loop system is stable. If however, the gains move out of these regions, it does not mean that the system will definitely be unstable. A tighter estimation of the gain margins is possible with the application of Ostrowski bands, which are discussed in the next section.

3.4.5 OSTROWSKI BANDS

The circles for the Ostrowski bands of $\mathbf{Q}^{-1}(s)$ are constructed in a similar fashion as those for the Gershgorin bands, but the radii of the circles for row dominance are now:

$$r_i = \varnothing_i(s)d_i(s)$$

where

$$\varnothing_i(s) = \max_j \frac{d_j(s)}{|\mathbf{f}_j + \hat{\mathbf{q}}_{jj}(s)|} \quad (3.14)$$

and $d(s)$ refer to the radii of the Gershgorin circles for $\mathbf{Q}^{-1}(s)$ given by eqn. (3.10).

In the case of column dominance $d(s)$ is replaced by $d'(s)$ and found from eqn. (3.11).

If $\mathbf{Q}^{-1}(s)$ is dominant then the Ostrowski bands are found to be narrower than the Gershgorin counterparts and allow tighter design of the gains \mathbf{f}_i . It is important to note, that a change in the gain of one loop will affect the radii of the other loops and it is therefore difficult to establish the exact gain space for which the closed-loop system $\mathbf{H}^{-1}(s)$ will be stable. The region so determined will usually be larger than that for Gershgorin bands.

In practice however, the design of a dominant and stable system is done with the aid of Gershgorin bands mainly, although this will result in a conservative choice of feedback gains. Having obtained a suitable feedback matrix \mathbf{F} , the Ostrowski circles can be plotted as a final check for stability and dominance.

3.5 ACHIEVING DIAGONAL DOMINANCE

The previous sections have shown that the Nyquist stability criterion can be applied to diagonally dominant systems. The first step of the INA technique is thus to design \mathbf{K} such that \mathbf{Q}^{-1} is diagonally dominant, before stability is considered.

The next Sections will demonstrate different methods to achieve this.

3.5.1 DIRECT AND PSEUDO-DIAGONALISATION

The following two methods will result in a real constant \mathbf{K} matrix. The one approach directly diagonalises $\mathbf{G}(s)$ at zero frequency by setting $\mathbf{K} = \mathbf{G}^{-1}(0)$ and the other is referred to as pseudo-diagonalisation(3,13). These two methods are not discussed in detail here although they have been applied in the past for simple systems.

Attention is focused instead on dynamic pre-compensators as they can easily be implemented with today's microcomputer technology and they are generally more successful at making $\mathbf{Q}^{-1}(s)$ diagonally dominant over the whole frequency range.

3.5.2 ELEMENTARY OPERATIONS

By operating on the rows or columns of $\mathbf{Q}^{-1}(s)$ by elementary operations, similar to Gauss elimination, it is possible to achieve dominance in most cases, if $\mathbf{K}(s)$ is allowed to be sufficiently complicated. At this point it is important to recall that a few restrictions are made to the form that $\mathbf{K}(s)$ may take [see Section 3.2.2], because the resulting

pre-compensator will have to be implemented in the final control scheme.

Other considerations such as non-minimum phase and controllability are discussed by Porter(14).

As the design involves a number of consecutive steps the pre-compensator can be written as

$$K(s) = K_n(s) \dots K_2(s) K_1(s) \quad (3.15)$$

where $K_i(s)$ correspond to the i th elementary operation.

Each elementary operation $K_i(s)$ can then be implemented in the control scheme individually, which is less complicated than implementing $K(s)$ as a whole.

3.5.2.1 Renumbering the inputs

The first step involves renumbering of the inputs of $G(s)$ with the aid of a permutation matrix $K(s)$. This allows the 'dominant' elements of each column of $Q^{-1}(s)$ to be moved into diagonal positions by swopping its rows.

The i th row can be swopped with j th row of $Q^{-1}(s)$ by setting $K(s) = I$ and swopping the i th column with j th column of K , then

$$K(s) = \begin{matrix} \text{Column} & 1 & 2 & & i & & j & & n & \text{Row} \\ \left[\begin{array}{cccccccc} 1 & 0 & \dots & 0 & \dots & 0 & \dots & 0 \\ 0 & 1 & \dots & 0 & \dots & 0 & \dots & 0 \\ \vdots & \vdots & & \vdots & & \vdots & & \vdots \\ 0 & 0 & \dots & 0 & \dots & 1 & \dots & 0 \\ \vdots & \vdots & & \vdots & & \vdots & & \vdots \\ 0 & 0 & \dots & 1 & \dots & 0 & \dots & 0 \\ \vdots & \vdots & & \vdots & & \vdots & & \vdots \\ 0 & 0 & \dots & 0 & \dots & 0 & \dots & 1 \end{array} \right] & \begin{array}{l} 1 \\ 2 \\ i \\ j \\ n \end{array} \end{matrix} \quad (3.16)$$

3.5.2.2 Row operations

The second type of operation involves adding a multiple of one row to another row of $Q^{-1}(s)$ to reduce the off-diagonal elements, which is related to Gauss elimination.

The operation

$$Row_i = Row_i + \alpha(s)Row_j \tag{3.17}$$

where $\alpha(s)$ is the multiplication function, is performed by setting $K(s)=I$ and then subtracting $\alpha(s)Col_i$ from Col_j , then

$$K(s) = \begin{matrix} \text{Column} & 1 & 2 & & i & & j & & n & \text{Row} \\ \left[\begin{array}{cccccccc} 1 & 0 & \dots & 0 & \dots & 0 & \dots & 0 \\ 0 & 1 & \dots & 0 & \dots & 0 & \dots & 0 \\ \vdots & \vdots & & \vdots & & \vdots & & \vdots \\ 0 & 0 & \dots & 1 & \dots & -\alpha(s) & \dots & 0 \\ \vdots & \vdots & & \vdots & & \vdots & & \vdots \\ 0 & 0 & \dots & 0 & \dots & 1 & \dots & 0 \\ \vdots & \vdots & & \vdots & & \vdots & & \vdots \\ 0 & 0 & \dots & 0 & \dots & 0 & \dots & 1 \end{array} \right] & \begin{array}{l} 1 \\ 2 \\ \\ i \\ \\ j \\ \\ n \end{array} \end{matrix} \tag{3.18}$$

The negative sign arises because the operation are performed on $Q^{-1}(s)$ and not $Q(s)$.

The rational function $\alpha(s)$ must have all its poles in the open left half plane and must be proper. If the multiplier function is not strictly proper then care must be taken that the gain at high frequency will not amplify the noise of the system excessively. In practice it is sufficient that

$$\lim_{s \rightarrow \infty} |\alpha(s)| \leq 10 \tag{3.19}$$

If element $\hat{q}_{ik}(s)$ is to be eliminated by using Row_j then the multiplier becomes

$$\alpha(s) = \frac{\hat{q}_{ik}(s)}{\hat{q}_{kj}(s)} \quad (3.20)$$

After performing the row operation $\hat{q}_{ik}(s) = 0$.

In practice it is very difficult to obtain $\alpha(s)$ because the elements $\hat{q}_{ik}(s)$ and $\hat{q}_{kj}(s)$ are not known in terms of s . A symbolic derivation of $\mathbf{Q}^{-1}(s)$ from $\mathbf{G}(s)$ in terms of s is extremely burdensome and also unnecessary because the resulting $\alpha(s)$ will most probably not conform to the restrictions that are imposed on $\mathbf{K}(s)$.

In most practical applications an approximation to $\alpha(s)$ is used, which will eliminate the reduced element sufficiently.

The row operations are thus a matter of trial and error. The INA design involves choosing an appropriate row for the elimination and finding an adequate approximation of the multiplier function. It is further a matter of skill to determine in which order the off-diagonal elements should be reduced. It is thus necessary to have a computer-aided control system design (CACSD) package to apply the INA technique. (5) The structure of such a programme is discussed in the *Software Reference*.

3.6 SINGLE-LOOP CONTROLLER DESIGN

After having achieved diagonal dominance, a diagonal matrix $\mathbf{K}_p(s)$ can be developed to complete the feedback control scheme. The elements of $\mathbf{K}_p(s)$ control the individual loops of the decoupled system and they can be designed by singlevariable techniques.

The Inverse Nyquist diagram of the diagonal elements can be used to design individual PID controllers, phase-lag or phase-lead circuits to improve the speed, gain and phase margins of the feedback loops as for singlevariable systems(14).

3.7 CONCLUSION

The INA technique is a powerful multivariable method in that it includes stability analysis, which is related to singlevariable systems. The design of a pre-compensator that results in a diagonal dominant system is intricate, but can be simplified sufficiently with the aid of an interactive CACSD package.

The technique can also be applied to the design of feedback controllers for the closed-loop system by making use of the Inverse Nyquist diagrams of the diagonal elements.

CHAPTER 3 THE INVERSE NYQUIST ARRAY TECHNIQUE

4. APPLICATION OF THE INVERSE NYQUIST ARRAY TECHNIQUE

4.1 INTRODUCTION

The Inverse Nyquist Array (INA) design technique was presented in chapter three. The method is now applied to the flotation rig with specific reference to controlling the Rougher and Scavenger tanks.

This chapter demonstrates the individual steps involved in the design of a pre-compensator to achieve dominance, single-loop controllers to control the levels and finally how this control scheme can be implemented on a digital computer.

4.2 FLOTATION RIG MODEL

The transfer function representation of the two-tank model is constructed from chapter two.

$$\begin{bmatrix} \mathbf{y}_1(s) \\ \mathbf{y}_2(s) \end{bmatrix} = \mathbf{G}(s) \begin{bmatrix} \mathbf{u}_1(s) \\ \mathbf{u}_2(s) \end{bmatrix} \quad (4.1)$$

where

$$G(s) = \begin{bmatrix} \frac{1.40E-2 s + 6.83E-5}{s^2 + 3.95E-2 s + 5.91E-4} & \frac{1.53E-4}{s^2 + 4.07E-2 s + 2.20E-4} \\ \frac{-1.22E-2}{s + 1.87E-2} & \frac{5.97E-3}{s + 1.19E-2} \end{bmatrix} \quad (4.2)$$

In eqn.(4.1) y_1 and y_2 refer to the Rougher and Scavenger tank level respectively and u_1 and u_2 correspond to the Rougher and Scavenger valve inputs respectively.

4.3 CLOSED-LOOP MODEL

The closed-loop control scheme, that will be designed to control the levels of the two tanks, is depicted in fig. 4.1.

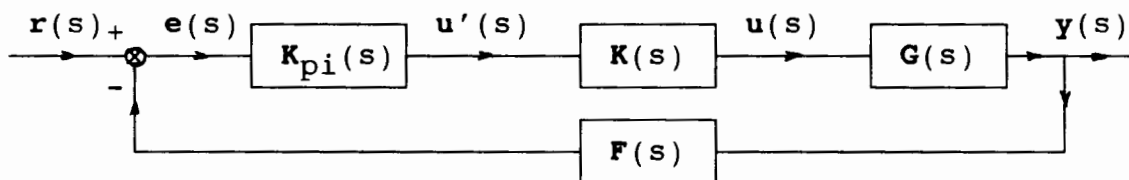


FIG. 4.1 Closed-loop Control Scheme

Vector r represents the setpoint levels for the two tanks, vector e is the comparator output, vector u' contains the inputs to the diagonal dominant system, vector u denotes the valve setting of the plant and vector y symbolises the tank output levels.

The diagonal matrix $K_{pi}(s)$ contains the single-loop proportional plus integral (PI) controllers, matrix $K(s)$ is the pre-compensator, that is designed to make the subsystem $Q(s)=G(s)K(s)$ diagonally dominant, matrix $G(s)$ represents the plant and the identity matrix $F(s)$ signifies unity feedback.

4.4 ACHIEVING DIAGONAL DOMINANCE

The INACAD program [see *Software Reference*] was used throughout the design of the pre-compensator to achieve row-dominance and the PI controllers for setpoint tracking. All the Nyquist diagrams were generated by INACAD. As the software does not cater for a separate single-loop controller, the $L(s)$ matrix was used for that purpose.

4.4.1 UNCOMPENSATED SYSTEM

The INA diagram of $G^{-1}(s)$ with row-dominance Gershgorin circles is depicted in fig. 4.2. (The frequency range was selected from $w=1E-4$ to $w=10$). It can be seen that the interaction of the two tanks is severe, as neither the Rougher nor the Scavenger tanks are dominant.

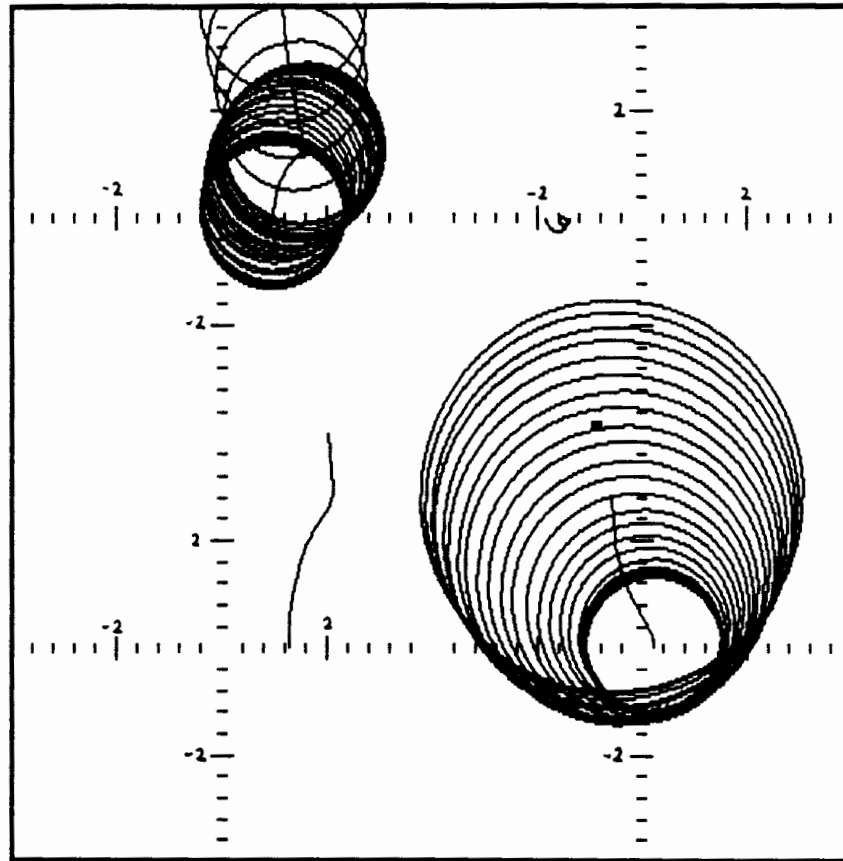


FIG. 4.2 INA Diagram of $G^{-1}(s)$ with Gershgorin circles

4.4.2 ROW OPERATIONS

The element $(2,1)$ of $G^{-1}(s)$ is eliminated by adding a multiple of row 1 to row 2.

$$\text{Row}_2 = \text{Row}_2 + \alpha(s) \text{Row}_1 \quad (4.3)$$

The multiplication function and its approximation is shown in fig. 4.3.

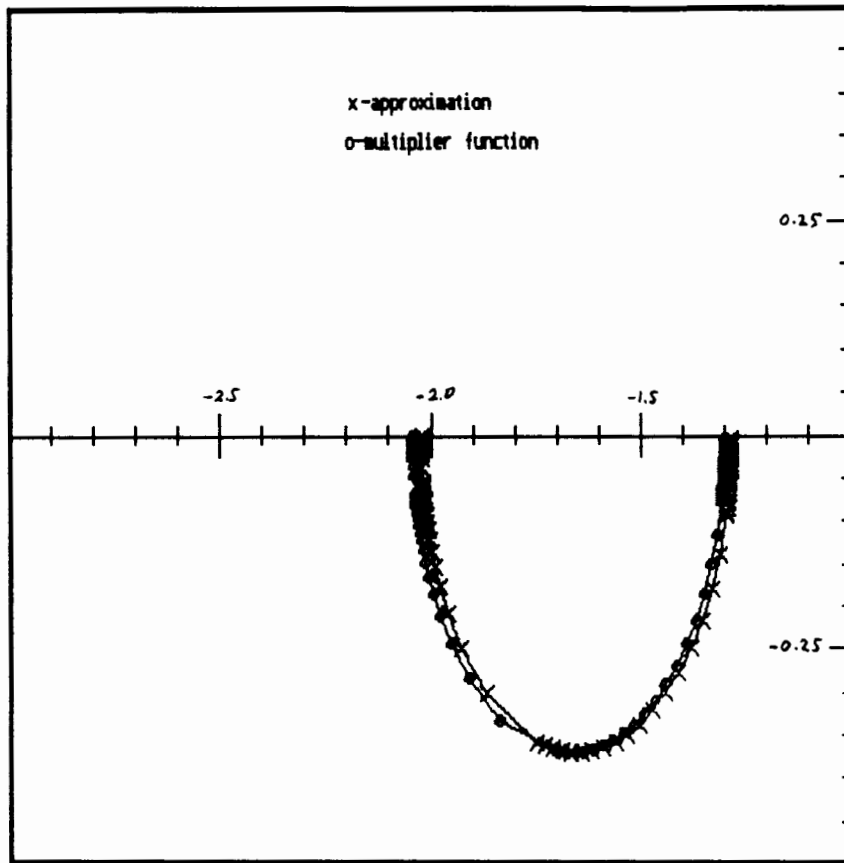


FIG. 4.3 Multiplication function to eliminate element (2,1)

The coefficients of the multiplication function were found by a non-linear parameter adjustment technique [see NELM in Chapter 7] then

$$\alpha(s) = - \frac{178.8 s + 1.748}{88.38 s + 1.363} \quad (4.4)$$

and the corresponding pre-compensator matrix is

$$K_1(s) = \begin{bmatrix} 1 & 0 \\ \frac{178.8 s + 1.748}{88.38 s + 1.363} & 1 \end{bmatrix} \quad (4.5)$$

The result of this row operation is depicted in Fig. 4.4. It can be seen that element (2,2) is now row-dominant.

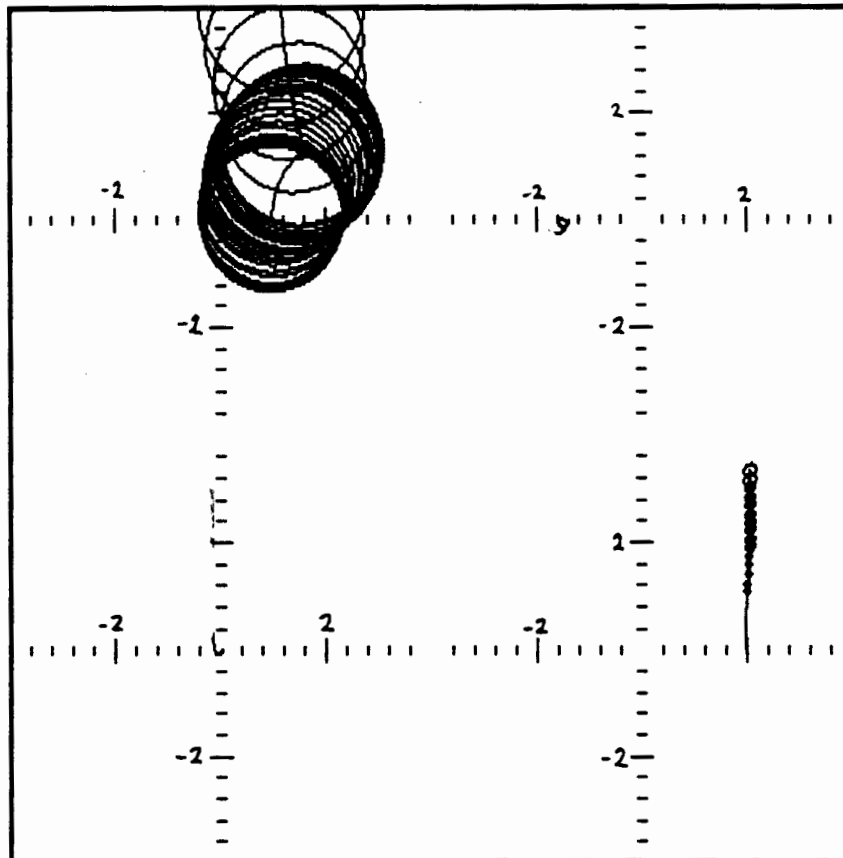


FIG. 4.4 INA Diagram of $G^{-1}(s)K_1$ with Gershgorin circles

In a similar fashion the element (1,2) of $\mathbf{G}^{-1}(s)\mathbf{K}_1$ is now eliminated by adding a multiple of row 2 to row 1.

$$\text{Row}_1 = \text{Row}_1 + \alpha(s) \text{Row}_2 \quad (4.6)$$

The multiplication function and its approximation is shown in fig. 4.5.

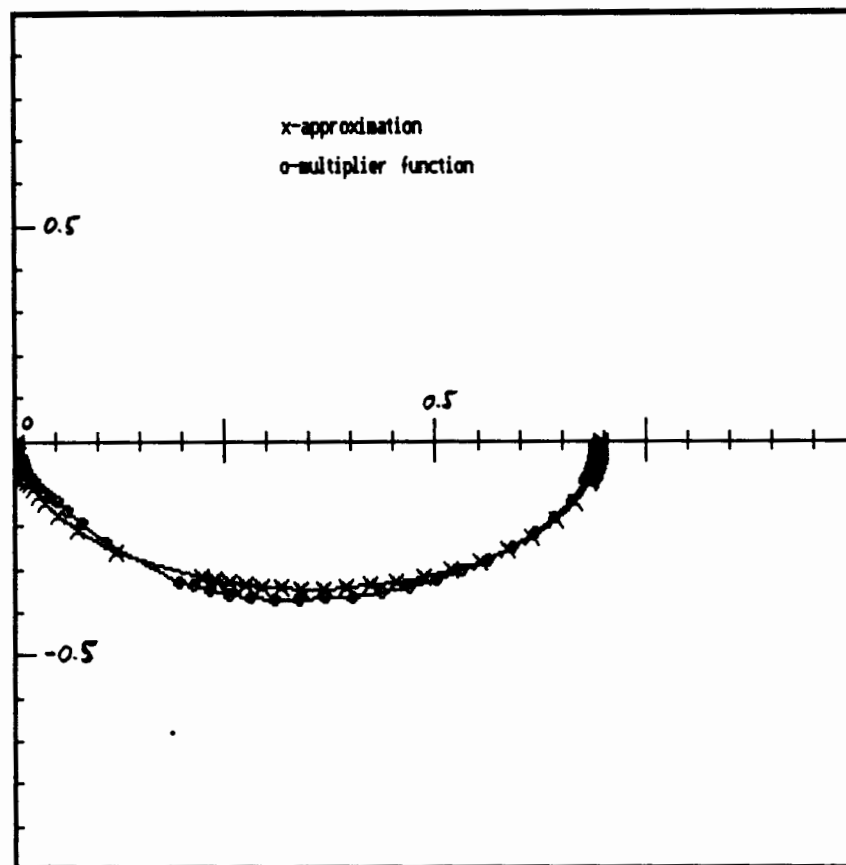


FIG. 4.5 Multiplication function to eliminate element (1,2)

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The coefficients were optimised and then

$$\alpha(s) = \frac{0.2935 s + 0.8089}{85.31 s + 1.159} \quad (4.7)$$

and the corresponding pre-compensator matrix is

$$K_2(s) = \begin{bmatrix} 1 & - \frac{0.2935 s + 0.8089}{85.31 s + 1.159} \\ 0 & 1 \end{bmatrix} \quad (4.8)$$

The INA diagram in fig. 4.6 shows that the plant has successfully been decoupled and is now row dominant.

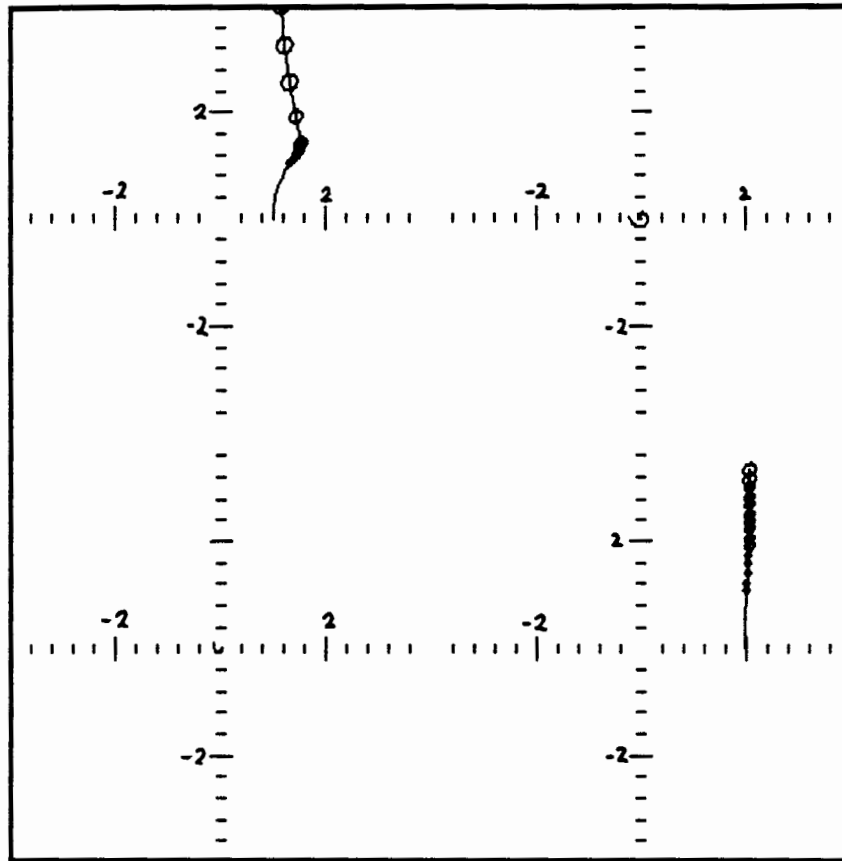


FIG. 4.6 INA Diagram of $G^{-1}(s)K_1K_2$ with Gershgorin circles

4.5 DESIGN OF SINGLE-LOOP PI CONTROLLERS

Since the control system is now diagonally dominant single-loop controllers can be designed by singlevariable techniques.

The PI controllers were designed such that the closed-loop system has step-responses with a maximum gain of 1.3, both

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levels are controlled equally fast and the noise sensitivity is kept at a minimum.

The resulting PI controller was found to be:

$$\mathbf{K}_{pi}(s) = \begin{bmatrix} \frac{10s+1}{s} & 0 \\ 0 & \frac{25s+2.5}{s} \end{bmatrix} \quad (4.9)$$

The resulting Direct Nyquist diagram is depicted in fig. 4.7.

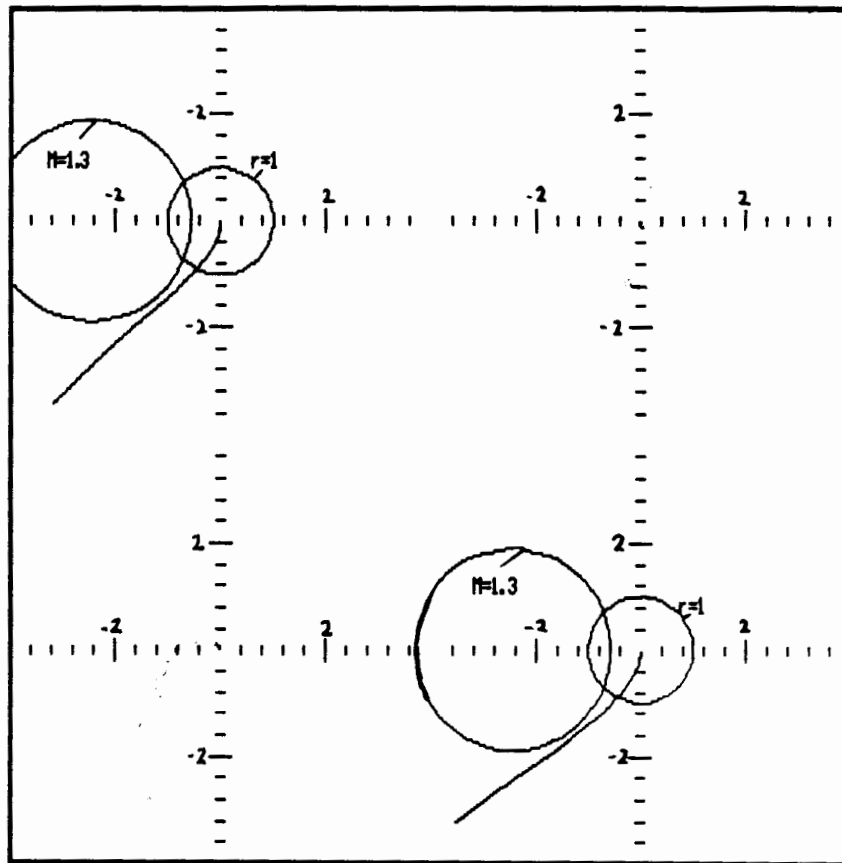


FIG. 4.7 Direct Nyquist Diagram of final control system

4.6 INTERPRETATION OF INITIAL CONDITIONS

The block diagram of Fig. 4.8 depicts the control system where r_t contains the setpoint levels, e_t the comparator output, u'_t the input to the dominant system, u_t the actual plant input and y_t the actual plant output, at time t and the initial valve settings are in u_0 .

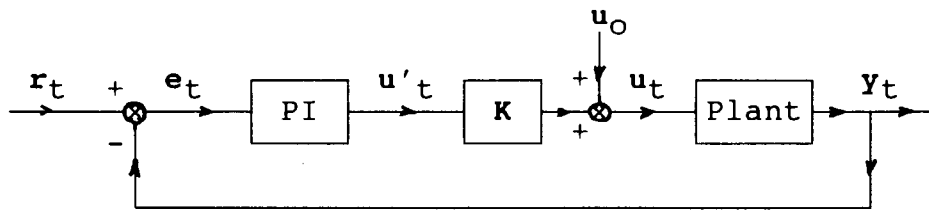


FIG. 4.8 Implementation of initial conditions

At the time $t=0$, when the control scheme is activated the setpoint levels are set to the initial output levels, the integrators of the PI controller and the initial conditions for K are set to zero, then

$$r_t = y_0,$$

$$e_t = 0$$

$$u'_t = 0$$

and

$$u_t = u_0. \quad (4.10)$$

The actual plant input u_t thus remains unchanged until the levels y_t of the tanks differ from the setpoint levels.

4.7 DIGITAL IMPLEMENTATION OF K

This section discusses the implementation of the above pre-compensators $k_{ij}(s)$ and the PI controllers $k_{pi}(s)$ on a digital computer.

4.7.1 THE BASIC DIGITAL CONTROLLER

The equation relating the input $u'(s)$ to the output $y'(s)$ of a singlevariable controller $k(s)$ is given by:

$$y'(s) = k(s)u'(s) \quad (4.12)$$

From eqn. (4.5) & (4.8), it is found that the functions can be formed by:

$$\begin{aligned} k(s) &= \frac{a_1s+a_0}{b_1s+b_0} \\ &= A + \frac{B}{s + b_0/b_1} \end{aligned} \quad (4.13)$$

where

$$\begin{aligned} A &= a_1/b_1 \\ B &= \frac{a_0b_1-a_1b_0}{b_1b_1} \end{aligned}$$

The z-transform of $k(s)$ is

$$k(z) = v(z) + w(z) \quad (4.14a)$$

where

$$v(z) = A \quad (4.14b)$$

and

$$w(z) = \frac{Bz}{z - \sigma z^{-1}} \quad (4.14c)$$

with

$$\sigma = e^{-\tau b_0/b_1} \quad (4.14d)$$

where τ is the sampling period.

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The controller function is then in discrete form:

$$k_n = v_n + w_n \quad (4.15)$$

As v_n is a simple gain function, using eqs.(4.12) & (4.14b), then

$$v_n = A u'_n \quad (4.16)$$

but w_n is a function of z , therefore the direct programming method, as it uses the minimum number of past values, is applied as follows:

Both the numerator and the denominator of the transfer function are multiplied by $z^{-1}q(z)$ to give:

$$\frac{w(z)}{u'(z)} = \frac{Bz}{z-\sigma} \frac{z^{-1} q(z)}{z^{-1} q(z)} \quad (4.17)$$

Equating the denominator of Eqn. (4.17) gives

$$\begin{aligned} u'(z) &= (1-\sigma z^{-1})q(z) \\ &= q(z) - \sigma z^{-1}q(z) \end{aligned} \quad (4.18)$$

then

$$q(z) = u'(z) + \sigma z^{-1}q(z) \quad (4.19)$$

In discrete form the above equation is written as

$$q_n = u'_n + \sigma q_{n-1} \quad (4.20)$$

By equating the numerator of eqn. (4.17), it is found that

$$w(z) = Bq(z) \quad (4.21)$$

and in discrete form this is written as

$$w_n = Bq_n \quad (4.22)$$

From eqs. (4.15b), (4.16) and (4.22) the discrete controller becomes

$$k_n = Au'_n + Bq_n \quad (4.23)$$

where q_n is given by Eqn.(4.20).

4.7.2 THE PRE-COMPENSATOR

Having established how a digital controller is implemented, the next step is to realise the row operation matrices.

The designed pre-compensator $K(s)$ can be written as

$$K(s) = K_2(s)K_1(s) \quad (4.24)$$

From the block diagram in fig. 4.1, the corresponding transfer function is

$$u(s) = K(s) u'(s) \quad (4.25)$$

This can be split into two equations such that

$$u^*(s) = K_1(s) u'(s) \quad (4.26a)$$

$$u(s) = K_2(s) u^*(s) \quad (4.26b)$$

The pre-compensator matrix K_1 from eqn.(4.5) can be written as

$$K_1(s) = \begin{bmatrix} 1 & 0 \\ k^1(s) & 1 \end{bmatrix} \quad (4.27a)$$

where

$$k^1(s) = \frac{178.8 s + 1.748}{88.38 s + 1.363} \quad (4.27b)$$

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The pre-compensator can then be implemented in discrete form, where $u_{i,n}$ corresponds to the i th input at time n , as

$$\begin{aligned} u^*_{1,n} &= u'_{1,n} \\ u^*_{2,n} &= k^1_n + u'_{2,n} \end{aligned} \quad (4.28)$$

where k^1_n is calculated by methods outlined in the previous Section with a sampling period $\tau=1$, then

$$k^1_n = A u'_{1,n} + Bq_{1,n} \quad (4.29a)$$

where

$$q_{1,n} = u'_{1,n} + \sigma q_{1,n-1} \quad (4.29b)$$

with initial condition $q_{1,n=0} = 0$.

In this case

$$A = 2.023$$

$$B = -0.01142$$

and

$$\sigma = 0.9847$$

In a similar fashion as above, the pre-compensator matrix K_2 from Eqn.(4.8) can be written as

$$K_2(s) = \begin{bmatrix} 1 & k^2(s) \\ 0 & 1 \end{bmatrix} \quad (4.27a)$$

where

$$k^2(s) = \frac{-0.2935 s - 0.8089}{85.31 s + 1.159} \quad (4.7)$$

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The pre-compensator can then be implemented in discrete form, where $u_{i,n}$ corresponds to the i th input at time n , as

$$\begin{aligned}u_{1,n} &= u^*_{1,n} + k^2_n \\u_{2,n} &= u^*_{2,n}\end{aligned}\tag{4.28}$$

k^2_n is calculated by methods outlined in the previous Section, again with a sampling period $\tau=1$ and found to be

$$k^2_n = A u'_{2,n} + Bq_{2,n}\tag{4.29a}$$

where

$$q_{2,n} = u'_{2,n} + \sigma q_{2,n-1}\tag{4.29b}$$

with initial condition $q_{2,n=0} = 0$.

In this case

$$A = 3.440E-3$$

$$B = -9.435E-3$$

and

$$\sigma = 0.9865$$

4.7.3 THE PI CONTROLLERS

The PI controllers can be implemented in the following fashion.

From fig. 4.1, the transfer equation for the PI controller is

$$u'(s) = K_{pi}(s)e(s)\tag{4.30}$$

The PI controller matrix of Eqn.(4.9) can be written as

$$\mathbf{K}_{pi}(s) = \begin{bmatrix} k^1_{pi}(s) & 0 \\ 0 & k^2_{pi}(s) \end{bmatrix} \quad (4.31a)$$

where

$$k^1_{pi}(s) = \left[\frac{10s+1}{s} \right] \quad (4.31b)$$

and

$$k^2_{pi}(s) = \left[\frac{25s+2.5}{s} \right] \quad (4.31c)$$

In discrete form the individual PI controllers are realised as follows:

$$u'_{1,n} = k_1(e_{1,n} + i_{1,n}) \quad (4.32a)$$

$$i_{1,n} = i_{1,n-1} + \frac{e_{1,n}}{\tau_1} \quad (4.32b)$$

$$u'_{2,n} = k_2(e_{2,n} + i_{2,n}) \quad (4.33a)$$

$$i_{2,n} = i_{2,n-1} + \frac{e_{2,n}}{\tau_2} \quad (4.33b)$$

where

$$k_1 = 10$$

$$k_2 = 25$$

$$\tau_1 = \tau_2 = 10$$

and the initial conditions are

$$i_{1,n=0} = i_{2,n=0} = 0$$

4.8 CLOSED-LOOP STEP RESPONSE

The level of all four tanks of the flotation rig were moved into their operating regions and allowed to attain steady-state before the designed control scheme was introduced, as discussed in chapter two. As the control system is designed to control only the two specified tanks, the Cleaner and Recleaner valves remained fixed throughout the tests. A step in setpoint level was applied after 100 seconds had elapsed.

The original step responses can be found in Appendix B. To compare the responses to those of a simulation, the responses were normalised by subtracting the initial level and dividing the result by the step size. The initial level is found by averaging the first 100 samples. The normalised responses of both the tanks and simulations are shown in fig. 4.9. The simulated values are shown by solid lines, except during extreme changes when they become dotted.

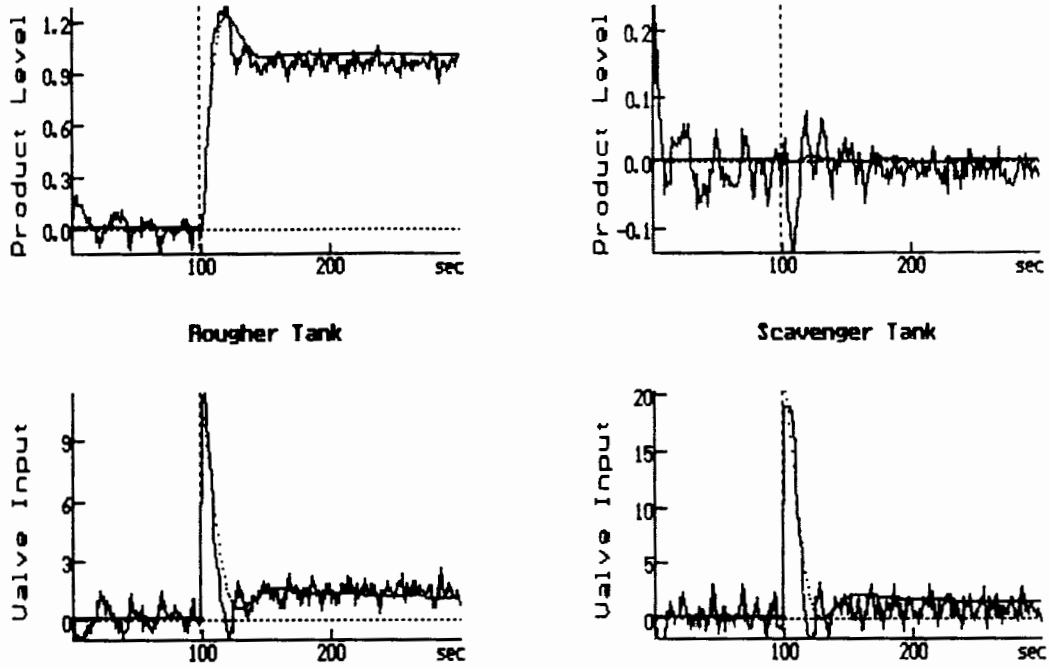
The responses correspond well to the simulated one if the noise of the plant is ignored.

The difference between the actual and the simulated level of the Rougher tank in Fig. 4.9a) can be attributed to the fact, that the initial level used to normalise the response was erroneous because the level had not been at steady-state at $t=0$. It should in fact have been lower.

The reason for the Scavenger valve inputs not reaching their simulated peaks is that the valve was driven into saturation. This also explains why the overshoot of the Scavenger level in Fig. 4.9b) is actually higher than predicted.

Actual / Simulated Closed-Loop Step Response

a) Rougher Step Size Normalised



Actual / Simulated Closed-Loop Step Response

b) Scavenger Step Size Normalised

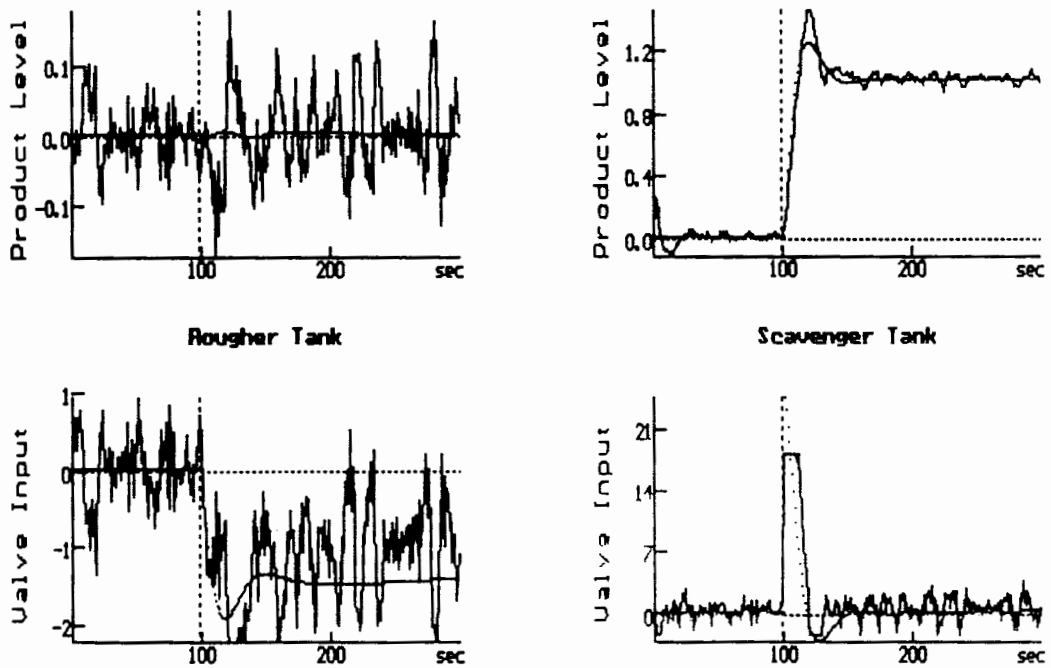


FIG. 4.9 Closed-loop system step response

It can be seen that the control system behaves in a manner as it was designed to do. The overshoot was limited to 0.3 times the step size. This can readily be confirmed by the previous step responses where the step sizes are normalised to 1. The noise sensitivity of the closed-loop system is also acceptable, as it does not impede the level control. The speed of response after a setpoint change are similar for both the Rougher and Scavenger tanks as they were designed to be.

4.9 CONCLUSION

The INA technique could successfully be applied to the flotation rig. Dominance could be achieved and single-loop PI controllers were designed by singlevariable methods for the two loops. The interaction was reduced considerably and the designed control scheme was adequate.

The similarity of the predicted and actual responses indicate that the model of the plant had been accurate enough for this application.

5. THE POLE ASSIGNMENT DESIGN TECHNIQUE

5.1 INTRODUCTION

This chapter will discuss a particular state space design method for multivariable systems, namely the Pole Assignment technique. It will show how Pole Assignment by state feedback can be implemented in multivariable systems and how it is related to single-input systems. It will focus on the dyadic approach and discuss the difficulties associated with the technique.

Observer design will also be discussed with particular reference to the Kalman filter for state estimation in a noisy environment. The latter must usually be included in any state space design method because multivariable systems tend to have a large number of states and only a few measurable outputs. The number of outputs are limited due to the high cost of instrumentation or unavailability of further measurements.

5.2 POLE ASSIGNMENT IN SYSTEM DESIGN

The pole assignment technique is well known for its application in single-input, single-output (SISO) plants to improve the closed-loop dynamic response of the system. The method is straightforward for SISO systems because the system zeroes are invariant to state feedback and the choice of closed-loop poles gives rise to a unique feedback gain

vector operating on the system states. Unfortunately other aspects of performance such as gain and integrity cannot be included into this state feedback design, because of the uniqueness of the feedback for a specific set of closed-loop pole positions.

An optimal design strategy(14) is possible by using dynamic feedback in conjunction with a cost function related to both states and inputs to increase the flexibility of the design, but considerable trial and error is involved until the resulting system has a satisfactory transient response.

In multivariable systems however a multiple of feedback configurations result in a specific set of pole locations. The associated degrees of freedom in this application complicate the design. A possible solution to achieve a more stringent design method is given by the dyadic approach to pole assignment.

5.3 DYADIC POLE ASSIGNMENT BY STATE FEEDBACK

Although pole assignment is possible by either output or state feedback the following discussion will be aimed toward the latter, because output feedback is in effect a design of proportional controllers, which is seldom adequate and in addition most multivariable system have less number of outputs than states, which may limit the number of poles that can be assigned.

5.3.1 SYSTEM MODEL FOR STATE FEEDBACK

To derive dyadic pole assignment the state equations of a linear, time-invariant multivariable system are considered,

because the basis for the method stems from the state space representation.

The state equation for a plant with n states, m inputs and l outputs is described by:

$$\begin{aligned} \dot{\mathbf{x}}(s) &= \mathbf{A}\mathbf{x}(s) + \mathbf{B}\mathbf{u}(s) \\ \mathbf{y}(s) &= \mathbf{C}\mathbf{x}(s) \end{aligned} \quad (5.1)$$

where \mathbf{A}, \mathbf{B} are real matrices with dimension $n \times n$, $n \times m$, $l \times n$, respectively. The vector \mathbf{x} represents the system states and vector \mathbf{u} represents the inputs. Fig. 5.1 shows the system model in block diagram form.

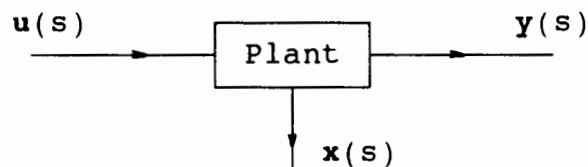


FIG. 5.1 Multivariable System Block Diagram

By applying pole assignment in state feedback the derivation is concerned with the state equation and the output equation may be omitted from the discussion.

The corresponding transfer-function matrix relating the inputs to the system states is given by matrix $\mathbf{G}(s)$ as follows:

$$\begin{aligned} \mathbf{x}(s) &= \mathbf{G}(s) \mathbf{u}(s) \\ \text{where } \mathbf{G}(s) &= (\mathbf{sI} - \mathbf{A})^{-1} \mathbf{B} \\ &= \frac{\text{Adj}(\mathbf{sI} - \mathbf{A}) \mathbf{B}}{|\mathbf{sI} - \mathbf{A}|} \end{aligned} \quad (5.2)$$

Matrix \mathbf{I} is the $n \times n$ identity matrix and $\text{Adj}()$ represents the Adjoint of a matrix.

The dynamic response of the system is then determined by its characteristic equation given by:

$$\phi(s) = |s\mathbf{I} - \mathbf{A}| = 0. \quad (5.3)$$

5.3.2 EQUIVALENT SINGLE-INPUT SYSTEM

The dyadic approach translates the multivariable system into an equivalent single input (ESI) system. The pole assignment strategy is then performed on this SI system by similar methods as used for single-variable systems. Only one particular method(12), related to dyadic or unity rank feedback controllers will be applied in this discussion.

As in SI systems, the resulting feedback will only affect the pole positions and not the zeroes of the initial ESI system. The final step is to translate the control law into its multivariable representation.

5.3.2.1 Open-Loop ESI System

To transform the multivariable system into an ESI system a vector \mathbf{q} is chosen such that the initial state equation:

$$\dot{\mathbf{x}}(s) = \mathbf{A}\mathbf{x}(s) + \mathbf{B}\mathbf{u}(s) \quad (5.4)$$

is transformed to

$$\dot{\mathbf{x}}(s) = \mathbf{A}\mathbf{x}(s) + \mathbf{b}w(s) \quad (5.5)$$

where

$$\mathbf{b} = \mathbf{B}\mathbf{q}$$

Vector \mathbf{q} is a $n \times 1$ vector and $w(s)$ is the single input.

The vector \mathbf{q} must be chosen such that the ESI system (\mathbf{A}, \mathbf{b}) is state-controllable. Such a vector can always be found if the original system (\mathbf{A}, \mathbf{B}) is controllable and only certain directions of the \mathbf{q} -vector must be avoided. Fig. 5.2 shows the block diagram of the ESI system.

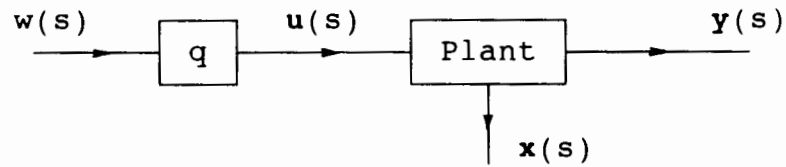


FIG. 5.2 Equivalent Single-input System

The open-loop ESI transfer function representation is then

$$\mathbf{x}(s) = \mathbf{G}_O(s) w(s),$$

where

$$\begin{aligned} \mathbf{G}_O(s) &= (s\mathbf{I} - \mathbf{A})^{-1} \mathbf{b} \\ &= \frac{\text{Adj}(s\mathbf{I} - \mathbf{A})^{-1} \mathbf{b}}{|s\mathbf{I} - \mathbf{A}|} \end{aligned} \quad (5.6)$$

which can be written as

$$\mathbf{G}_O(s) = \frac{\mathbf{g}_O(s)}{d_O(s)} \quad (5.7a)$$

$$= \frac{1}{s^n + d_n s^{n-1} + \dots + d_1} \begin{bmatrix} k_{11} + \dots + k_{1n} s^{n-1} \\ k_{n1} + \dots + k_{nn} s^{n-1} \end{bmatrix} \quad (5.7b)$$

where $\mathbf{g}_0(s)$ is a n -vector of polynomials in s describing the zero locations and $d_0(s)$ is the characteristic polynomial whose roots are the open-loop poles for the ESI system.

5.3.2.2 Closed-Loop ESI System

The closed-loop system description can be found by using a state feedback controller as follows:

$$\mathbf{w}(s) = \mathbf{v}(s) - \mathbf{f}^T \mathbf{x}(s), \quad (5.8)$$

where $\mathbf{v}(s)$ is the new external single input and \mathbf{f} is the scalar feedback $n \times 1$ vector.

Then the closed loop ESI system becomes

$$\dot{\mathbf{x}}(s) = (\mathbf{A} - \mathbf{b}\mathbf{f}^T) \mathbf{x}(s) + \mathbf{b}\mathbf{v}(s) \quad (5.9)$$

and the closed-loop ESI transfer function relating the input to the states is:

$$\mathbf{x}(s) = \mathbf{G}_C(s) \mathbf{v}(s) \quad (5.10)$$

$$\begin{aligned} \mathbf{G}_C(s) &= \{\mathbf{sI} - (\mathbf{A} - \mathbf{b}\mathbf{f}^T)\}^{-1} \mathbf{b} \\ &= \frac{\text{Adj}\{\mathbf{sI} - (\mathbf{A} - \mathbf{b}\mathbf{f}^T)\} \mathbf{b}}{|\mathbf{sI} - (\mathbf{A} - \mathbf{b}\mathbf{f}^T)|} \\ &= \frac{\mathbf{g}_C(s)}{d_C(s)} \end{aligned} \quad (5.11)$$

where $\mathbf{g}_C(s)$ and $d_C(s)$ are the corresponding representation as before, but for the closed-loop ESI system.

Alternatively the closed-loop system may be found by using Eqn. (5.6) and Eqn. (5.8) then:

$$\begin{aligned}
 \mathbf{x}(s) &= \frac{\mathbf{g}_O(s) w(s)}{d_O(s)} \\
 &= \frac{\mathbf{g}_O(s) \{v(s) - \mathbf{f}^T \mathbf{x}(s)\}}{d_O(s)} \\
 &= \frac{\mathbf{g}_O(s) v(s)}{d_O(s) + \mathbf{f}^T \mathbf{g}_O(s)}
 \end{aligned} \tag{5.12}$$

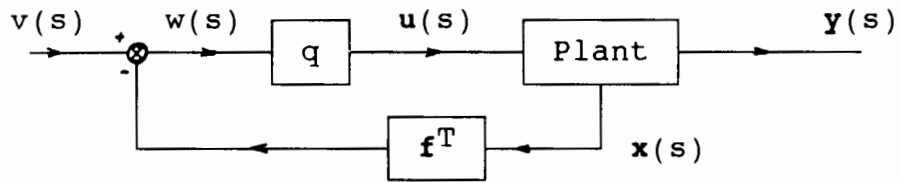


FIG. 5.3 Closed-loop ESI System

Fig. 5.3. shows the block diagram of the resulting closed-loop ESI system.

From equating Eqn. (5.7a) and Eqn. (5.12) it follows that:

$$\mathbf{g}_C(s) = \mathbf{g}_O(s) \tag{5.13}$$

and

$$d_C(s) = d_O(s) + \mathbf{f}^T \mathbf{g}_O(s) \tag{5.14}$$

From Eqn. (5.13) the invariability of the open- and closed-loop zeroes are confirmed.

Eqn. (5.14) is known as the *pole assignment equation* and determines the scalar state feedback vector \mathbf{f} for a given set of closed-loop pole positions. An examination of the relationship shows that if no poles are to be moved by the

feedback then $\mathbf{f} = 0$, which is an obvious but important result, when analysing system integrity.

From Eqn. (5.14) also follows that in general arbitrary pole assignment is possible for controllable systems(16). The constraints are that the desired poles, if complex must occur in conjugate pairs and all states must be available for feedback. If all states are not measurable in a observable system, they can be made available by using a Luenberger or reduced observer(7), eliminating the problems associated with incomplete state feedback, where only some poles can be assigned to specific positions.

5.3.3 CLOSED-LOOP MULTI-INPUT SYSTEM

To transform the resulting feedback system back into the multivariable system the final control law is given by:

$$\mathbf{K} = \mathbf{q}\mathbf{f}^T \quad (5.15)$$

such that

$$\mathbf{u}(s) = -\mathbf{K}\mathbf{x}(s) + \mathbf{v}(s) \quad (5.16)$$

where vector $\mathbf{u}(s)$ represents the plant inputs and $\mathbf{v}(s)$ is the new system input vector.

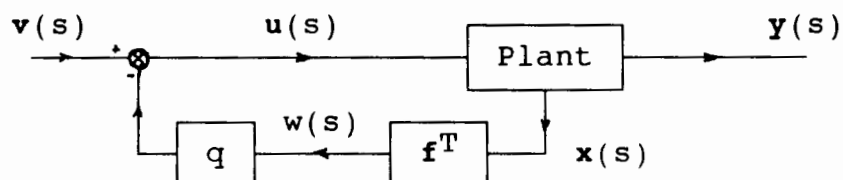


FIG. 5.4 Closed-loop Multi-input System

A block diagram of the closed-loop MI system is given in Fig. 5.4.

Matrix \mathbf{K} is termed a unity rank feedback controller because it is constructed from the product of two vectors or dyadic pair. The vector \mathbf{q} can be regarded as distributing the scalar state feedback value $\mathbf{f}^T \mathbf{x}$ across all the inputs to the plant.

The general closed-loop multivariable system becomes:

$$\begin{aligned}\dot{\mathbf{x}}(s) &= \mathbf{A}_C \mathbf{x}(s) + \mathbf{B} \mathbf{v}(s) \\ \mathbf{y}(s) &= \mathbf{C} \mathbf{x}(s) + \mathbf{D} \{-\mathbf{K} \mathbf{x}(s) + \mathbf{v}(s)\}\end{aligned}\quad (5.17)$$

where

$$\begin{aligned}\mathbf{A}_C &= (\mathbf{A} - \mathbf{B} \mathbf{K}) \\ &= (\mathbf{A} - \mathbf{b} \mathbf{f}^T)\end{aligned}$$

The complete closed-loop transfer function for a strictly proper system (i.e. $\mathbf{D}=0$) is then:

$$\begin{aligned}\mathbf{G}(s) &= \mathbf{C} (s\mathbf{I} - \mathbf{A}_C)^{-1} \mathbf{B} \\ &= \frac{\mathbf{C} \text{Adj}(s\mathbf{I} - \mathbf{A}_C) \mathbf{B}}{|s\mathbf{I} - \mathbf{A}_C|}\end{aligned}\quad (5.18)$$

The new characteristic equation being:

$$\phi_C = |s\mathbf{I} - \mathbf{A}_C| = 0 \quad (5.19)$$

containing the desired pole positions.

The transient response of the final multivariable system is then governed by the selected pole positions specified with $d_C(s)$ and zero locations given by $\mathbf{C} \text{Adj}(s\mathbf{I} - \mathbf{A}_C) \mathbf{B}$.

5.3.4 NUMERICAL TECHNIQUES IN DYADIC POLE ASSIGNMENT

The pole assignment technique contains considerable computational effort and would be extremely tedious to use if calculations were to be made by hand, but by programming a digital computer with a suitable algorithm its use can be simplified greatly. This section will show how the feedback law is computed and suggest appropriate numerical techniques. A complete FORTRAN listing of the program is available in the *Software Reference*.

Determination of Controllability

The first step of the numerical technique involves choosing an appropriate vector \mathbf{q} .

The ESI system will be controllable if and only if

$$\mathbf{P} = (\mathbf{Bq} \quad \mathbf{ABq} \quad \mathbf{A}^2\mathbf{Bq} \quad \dots \quad \mathbf{A}^{n-1}\mathbf{Bq}) \quad (5.20)$$

has rank n . (13)

To test for controllability a good numerical technique is to calculate the determinant of \mathbf{P} by manipulating it into echolon form and calculating the trace of the resulting matrix. (5) If any diagonal element of the resulting matrix is zero then the resulting determinant will be zero and the system will be rank deficient.

5.3.4.1 Frequency Domain Technique

A possible numerical technique to calculate the required state feedback matrix is related to the frequency domain representation of control systems.

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For this method, $\mathbf{g}_0(s)$ and $d_0(s)$ must be calculated from:

$$\frac{\mathbf{g}_0(s)}{d_0(s)} = \frac{\text{Adj}(s\mathbf{I}-\mathbf{A}) \mathbf{b}}{|s\mathbf{I}-\mathbf{A}|} \quad (5.21)$$

A recursive procedure by D.K. Faddeev to compute this has been shown previously in section 1.7.1.1.

The closed-loop characteristic polynomial $d_c(s)$ can simply be calculated from:

$$\begin{aligned} d_c(s) &= (s-p_1)(s-p_2)\dots(s-p_n) \\ &= s^n + d_{n-1}s^{n-1} + \dots + d_0 \end{aligned} \quad (5.22)$$

where the desired pole positions are given by p_i , $i=1,n$.

An approach to calculate the unity rank feedback controller for pole assignment by state feedback has been given by Fallside and Seraji(17).

The technique transforms the matrix $\mathbf{g}_0(s)$, with polynomials of s as its elements to a matrix \mathbf{M} of constant coefficients.

Specifically:

$$\mathbf{g}_0(s) = \mathbf{M}^T \mathbf{s} \quad (5.23)$$

where \mathbf{s} is a vector of powers of s :

$$\mathbf{s} = \begin{bmatrix} 1 \\ s \\ s^2 \\ \vdots \\ s^{n-1} \end{bmatrix} \quad (5.24)$$

The characteristic function $d_0(s)$ is also transformed from a polynomial of s to a constant coefficient vector \mathbf{a}_0 .

Then the closed-loop characteristic function becomes:

$$d_C(s) = s^n + \mathbf{a}_C^T \mathbf{s} \quad (5.25)$$

and that for the open-loop

$$d_O(s) = s^n + \mathbf{a}_O^T \mathbf{s} \quad (5.26)$$

The pole assignment equation given by:

$$d_C(s) = d_O(s) + \mathbf{f}^T \mathbf{g}_O(s) \quad (5.27)$$

becomes

$$\mathbf{a}_C^T \mathbf{s} = \mathbf{a}_O^T \mathbf{s} + \mathbf{f}^T \mathbf{M}^T \mathbf{s} \quad (5.28)$$

From Eqn. (5.28) it follows that:

$$\mathbf{a}_C = \mathbf{a}_O + \mathbf{fM} \quad (5.29)$$

The feedback vector \mathbf{f} is then found by solving the simultaneous equations given by:

$$\mathbf{Mf} = \mathbf{a}_C - \mathbf{a}_O \quad (5.30a)$$

where matrix \mathbf{M} is related to $\mathbf{g}_O(s)$, while \mathbf{a}_O and \mathbf{a}_C are related to $d_O(s)$ and $d_C(s)$ respectively.

Any numerical method to solve the simultaneous equations can be applied here. A less accurate method would be to use a matrix inversion routine to find \mathbf{M}^{-1} and then:

$$\mathbf{f} = \mathbf{M}^{-1}(\mathbf{a}_C - \mathbf{a}_O) \quad (5.30b)$$

5.3.4.2 Controllable Companion Form Technique

A different method which may be used as a check or as an alternative to the algorithm presented above is used by Borrie(5).

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The matrices \mathbf{A} and \mathbf{b} of the ESI system are converted to controllable companion form using the transformation $\mathbf{x}=\mathbf{Tz}$ to give the following open-loop state equation:

$$\dot{\mathbf{z}} = \mathbf{A}_0\mathbf{z} + \mathbf{b}_0w \quad (5.31)$$

where

$$\mathbf{A}_0 = \mathbf{T}^{-1}\mathbf{AT} \quad (5.32)$$

and

$$\mathbf{b}_0 = \mathbf{T}^{-1}\mathbf{b} = (0 \ 0 \ \dots \ 1)^T \quad (5.33)$$

The $n \times n$ matrix \mathbf{T} can be found from the controllability matrix \mathbf{P} given by Eqn.(5.20) as follows:

$$\mathbf{T}^{-1} = \begin{bmatrix} \mathbf{p}_n^T \\ \mathbf{p}_n^T\mathbf{A} \\ \vdots \\ \mathbf{p}_n^T\mathbf{A}^{n-1} \end{bmatrix} \quad (5.34)$$

where \mathbf{p}_n^T is the n th (last) row of \mathbf{P}^{-1} . Care must be taken that \mathbf{A}^i is computed first before it is multiplied by \mathbf{p}_n^T .

As before it is necessary for matrix \mathbf{P} to have rank n , i.e. the system (\mathbf{A}, \mathbf{b}) must be fully controllable.

It can be shown that the matrix \mathbf{T} is related to the matrix \mathbf{M} used in the method by Fallside(17) as follows:

$$\mathbf{T} = \mathbf{M}^T \quad (5.35)$$

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In the controllable form the closed-loop state equations become:

$$\dot{\mathbf{z}} = (\mathbf{A}_O - \mathbf{b}_O \mathbf{f}_C^T) \mathbf{z} + \mathbf{b}_O v \quad (5.36)$$

where \mathbf{f}_C is the state feedback vector in controllable form.

The closed-loop characteristic equation is found from the desired pole positions p_1, p_2, \dots, p_n as before:

$$(s-p_1)(s-p_2)\dots(s-p_n) = s^n + a_C(n-1)s^{n-1} + \dots + a_{C0} \quad (5.37)$$

The desired closed-loop state equations are then also given by:

$$\dot{\mathbf{z}} = \mathbf{A}_C \mathbf{z} + \mathbf{b}_C v \quad (5.38)$$

where the nth (last) row of \mathbf{A}_C is:

$$-a_{C0} \quad -a_{C1} \quad \dots \quad -a_{C(n-1)} \quad (5.49)$$

By equating Eqn. (5.36) and Eqn. (5.38) and using the fact that:

$$\mathbf{b}_O = \mathbf{b}_C \quad (5.50)$$

for both the open- and closed-loop system it is found that:

$$(\mathbf{A}_O - \mathbf{b}_O \mathbf{f}_C^T) = \mathbf{A}_C \quad (5.51)$$

and

$$\mathbf{b}_O \mathbf{f}_C^T = \mathbf{A}_O - \mathbf{A}_C \quad (5.52)$$

It can be shown that the nxn matrix $\mathbf{b}_O \mathbf{f}_C^T$ has as its nth (last) row the vector \mathbf{f}_C^T and all other elements equal to zero.

Then

$$\mathbf{f}_C = \mathbf{a}_C - \mathbf{a}_O \quad (5.53)$$

where $-\mathbf{a}_i^T$ are nth (last) rows of A_i respectively.

The feedback vector \mathbf{f} for the ESI system can then be determined from:

$$\begin{aligned} \mathbf{f}^T \mathbf{x} &= \mathbf{f}^T \mathbf{T} \mathbf{z} \\ &= \mathbf{f}_C^T \mathbf{z} \\ &= \mathbf{f}_C^T \mathbf{T}^{-1} \mathbf{x} \end{aligned} \quad (5.53)$$

and then

$$\begin{aligned} \mathbf{f}^T &= \mathbf{f}_C^T \mathbf{T}^{-1} \\ &= (\mathbf{a}_C - \mathbf{a}_O)^T \mathbf{T}^{-1} \end{aligned} \quad (5.54a)$$

and

$$\mathbf{f} = (\mathbf{T}^{-1})^T (\mathbf{a}_C - \mathbf{a}_O) \quad (5.54b)$$

Comparing Eqn. (5.30b) and Eqn. (5.54b) shows the similarity of the two methods. In the one technique matrix $(\mathbf{T}^{-1})^T$ is found from the controllability matrix \mathbf{P} , and in the other \mathbf{M}^{-1} is calculated by the Faddeev algorithm.

From this it follows that the two matrices are equivalent (Eqn. 5.35) and this fact can be used to compare the results of the alternative method to the algorithm presented before. As the computation involved differs for the two methods, it is found that \mathbf{T} will in fact be different to \mathbf{M}^T and as the system order increases they will diverge. This will be shown in detail in chapter six.

Both methods have been found not to be numerically adequate for ill-conditioned and high-order systems. For the plant used in this study however, the computational accuracy was

acceptable, but alternative methods have been found lately(18,19,20).

5.3.5 SUMMARY OF DYADIC FEEDBACK DESIGN

- 1) Choose the vector \mathbf{q} to transform the multi-input system to an ESI system and check for controllability.
- 2) Select the closed-loop system pole positions and calculate vector \mathbf{f}^T .
- 3) Insert the state feedback $\mathbf{K} = \mathbf{qf}^T$ into the multivariable system.
- 4) Simulate the transient response of the closed-loop system $(\mathbf{A}-\mathbf{BK})$ for step inputs and if unsatisfactory change the selection of \mathbf{q} and/or pole positions and repeat the procedure.

5.3.6 ANALYSIS OF ZERO MOVEMENT

This example will show the effects of dyadic pole assignment on a multivariable system. It will illustrate first the outcome of choosing a specific \mathbf{q} -vector and varying the pole positions and secondly fixing the pole positions and varying the \mathbf{q} -vector.

This illustration will concentrate on the affects of pole assignment on the system zeroes. The definition of multivariable system zeroes used here varies from those given by other authors(3,13).

Consider a system with transfer function:

$$\mathbf{y}(s) = \mathbf{G}(s) \mathbf{u}(s)$$

where

$$\mathbf{G}(s) = \begin{bmatrix} 1/(s+2) & 0 \\ 1/(s+1) & 1/(s+3) \end{bmatrix}$$

Then a possible state space representation of form:

$$\dot{\mathbf{x}}(s) = \mathbf{A}\mathbf{x}(s) + \mathbf{B}\mathbf{u}(s)$$

$$\mathbf{y}(s) = \mathbf{C}\mathbf{x}(s)$$

has

$$\mathbf{A} = \begin{bmatrix} -2 & 0 & 0 \\ 0 & -1 & 0 \\ 0 & 0 & -3 \end{bmatrix}, \quad \mathbf{B} = \begin{bmatrix} 1 & 0 \\ 1 & 0 \\ 0 & 1 \end{bmatrix}, \quad \mathbf{C} = \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 1 \end{bmatrix}$$

As the first step of the procedure choose

$$\mathbf{q}^T = (1, 1)$$

which is found to make the system (\mathbf{A}, \mathbf{b}) controllable i.e.

$$|\mathbf{b} \quad \mathbf{A}\mathbf{b} \quad \mathbf{A}^2\mathbf{b}| = 2$$

then from $\mathbf{b} = \mathbf{B}\mathbf{q}$

$$\mathbf{b}^T = (1, 1, 1)$$

5.3.6.1 Single-Input System Zeroes

The open-loop ESI system transfer function has:

$$\mathbf{g}_O(s) = \begin{bmatrix} s^2+4s+3 \\ s^2+5s+6 \\ s^2+3s+2 \end{bmatrix}$$

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The ESI system zeroes are therefore at:

$$s=-1,-3,-2,-3,-1 \text{ and } -2$$

It is important to note, that the definition of the system zeroes given above is not strictly correct, because the zeroes above would in fact vanish on evaluating the system transfer function $g_o(s)/d_o(s)$. It will become apparent later, that for the purpose of this example, it is however necessary to observe all the zeroes before cancellation.

To assign the closed-loop pole positions to

$$s=-2,-2 \text{ and } -3$$

the characteristic function for the open-loop system is:

$$d_o(s) = s^3+6s^2+11s+6$$

and that for the closed-loop system is:

$$d_c(s) = s^3+7s^2+16s+12$$

The resulting feedback law has

$$\mathbf{f}^T = (0,1,0)$$

The matrix A_c is found to be

$$\mathbf{A}_c = \begin{bmatrix} -2 & -1 & 0 \\ 0 & -2 & 0 \\ 0 & -1 & -3 \end{bmatrix}$$

with poles at:

$$s=-2,-2,-3$$

and zero positions given by:

$$\mathbf{g}_C(s) = \begin{bmatrix} s^2+4s+3 \\ s^2+5s+6 \\ s^2+3s+2 \end{bmatrix}$$

$$= \mathbf{g}_O(s)$$

The result above shows that the zero positions of the open- and closed-loop ESI system are invariant to pole shifting, as predicted by the theory.

The element zeroes of the transfer function $\mathbf{g}_C(s)/d_C(s)$ are in this case:

$$s=-1, -1$$

From this follows, that there is no relationship between the open-loop zeroes of $\mathbf{g}_O(s)/d_O(s)$ which had in fact none, and the closed-loop zeroes of $\mathbf{g}_C(s)/d_C(s)$. This again emphasises the need to analyse the zeroes before cancellation can take place as mentioned before.

5.3.6.2 Multi-Input System Zeroes

To analyse the effect of dyadic pole positioning on the zeroes of the multivariable system the following functions need to be calculated:

For the open-loop case:

$$\mathbf{T}_O(s) = \mathbf{C} \operatorname{adj}(s\mathbf{I}-\mathbf{A}) \mathbf{B}$$

and for the closed-loop multi-input (MI) system:

$$\mathbf{T}_C(s) = \mathbf{C} \operatorname{adj}(s\mathbf{I}-\mathbf{A}_C) \mathbf{B}$$

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As before it is noteworthy, that the zeroes found from the equations above could cancel when forming the transfer function.

Choosing $\mathbf{q}^T = (1, 1)$ as above, the open-loop zero positions are given by:

$$\mathbf{T}_O(s) = \begin{bmatrix} s^2+4s+3 & 0 \\ s^2+5s+6 & s^2+3s+2 \end{bmatrix}$$

i.e zeroes at $s = -1, -3, -2, -3, -1,$ and -2

and the open-loop transfer function is:

$$\mathbf{G}_O(s) = \begin{bmatrix} 1/(s+2) & 0 \\ 1/(s+1) & 1/(s+3) \end{bmatrix}$$

Assigning the poles to

$s = -2, -2, -3$ as before

then the closed-loop zero positions will be given by:

$$\mathbf{T}_C^a(s) = \begin{bmatrix} s^2+4s+3 & 0 \\ s^2+4s+4 & s^2+4s+4 \end{bmatrix}$$

$$+ \mathbf{T}_O(s)$$

The new zero positions are at:

$s = -1, -3, -2, -2, -2$ and -2

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The resulting transfer function will be:

$$\mathbf{G}_C^a(s) = \begin{bmatrix} (s+1)/(s+2)^2 & 0 \\ 1/(s+3) & 1/(s+3) \end{bmatrix}$$

The pole assignment method has not only shifted the poles, but also transformed element $\mathbf{G}_{O(1,1)}(s)$ from a first order system to a second order system.

Using $\mathbf{q}^T=(1,1)$ again and assigning the poles to:

$$s = -1, -3, -3$$

then

$$\mathbf{T}_C^b(s) = \begin{bmatrix} s^2+4s+3 & 0 \\ s^2+4s+5 & s^2+4s+3 \end{bmatrix}$$

$$\neq \mathbf{T}_C^a(s)$$

This design will move the zeroes to:

$$s = -1, -3, -2 \pm j, -1 \text{ and } -3$$

The closed-loop transfer function is now:

$$\mathbf{G}_C^b(s) = \begin{bmatrix} 1/(s+3) & 0 \\ (s+2-j)(s+2+j)/\{(s+1)(s+3)^2\} & 1/(s+3) \end{bmatrix}$$

Assigning poles to:

$$s = -1, -3, -3 \text{ as above}$$

and using $\mathbf{q}^T = (-1, 1)$ instead, which also assures controllability results in closed-loop zero positions given by:

$$\mathbf{T}_C^C(s) = \begin{bmatrix} s^2+4s+3 & 0 \\ s^2+6s+7 & s^2+4s+3 \end{bmatrix}$$

The zeroes are now moved to:

$$s = -1, -3, -4.4, -1.6, -1 \text{ and } -3$$

The closed-loop transfer function becomes:

$$\mathbf{G}_C^C(s) = \begin{bmatrix} 1/(s+3) & 0 \\ (s+4.4)(s+1.6)/\{(s+1)(s+3)^2\} & 1/(s+3) \end{bmatrix}$$

This example has shown that the zeroes of the ESI system are set by the vector \mathbf{q} only, but the zeroes of the MI system change as \mathbf{q} and/or pole positions are changed. In addition, it was shown that the closed-loop transfer function change considerably to accommodate the new pole positions.

5.3.7 DIFFICULTIES OF METHOD

This section will elaborate on the implications of choosing a specific \mathbf{q} and reasons for moving the poles. Additionally, the limitations associated with the selected pole positions and with the pole assignment technique in general are discussed.

5.3.7.1 Choice of vector \mathbf{q}

The \mathbf{q} vector is required to transform the MI system to an ESI system. The theory applied above implies that for a

specific vector \mathbf{q} and different closed-loop pole positions the open- and closed-loop zeroes remain the same, i.e.:

$$\text{Adj}(s\mathbf{I}-\mathbf{A}) \mathbf{B}\mathbf{q} = \text{Adj}\{s\mathbf{I}-(\mathbf{A}-\mathbf{b}\mathbf{f}^T)\} \mathbf{B}\mathbf{q} \quad (5.55)$$

but this does not apply for the multivariable case since:

$$\text{Adj}(s\mathbf{I}-\mathbf{A}) \mathbf{B} \neq \text{Adj}\{s\mathbf{I}-(\mathbf{A}-\mathbf{b}\mathbf{f}^T)\} \mathbf{B} \quad (5.56)$$

and

$$\mathbf{C} \text{Adj}(s\mathbf{I}-\mathbf{A}) \mathbf{B} \neq \mathbf{C} \text{Adj}\{s\mathbf{I}-(\mathbf{A}-\mathbf{b}\mathbf{f}^T)\} \mathbf{B} \quad (5.57)$$

This shows that the zeros of the MI system will change in a complicated way.

It follows that choosing \mathbf{q} will fix the closed-loop zeroes of the ESI system irrespective of pole position, i.e. only the selection of \mathbf{q} determines the closed-loop zeroes. But this is not the case for the MI system.

From Eqn. (5.15) it follows that \mathbf{q} distributes the scalar state feedback quantity $\mathbf{f}^T\mathbf{x}$ among the plant inputs. If the plant inputs have different ranges, \mathbf{q} can be used to scale the feedback quantity between the various inputs. Each input is then affected by the feedback in the same proportion.

5.3.7.2 Closed-Loop Zeroes

The zeroes of the closed-loop MI system are not invariant and cannot be fixed by a specific \mathbf{q} , instead the closed-loop zeroes are determined by both the choice of \mathbf{q} and the assigned pole positions. The actual movements of the zeroes from the open- to the closed MI system are complicated and a general formulation of the movement is laborious.

The closed-loop system may as a result have zeroes in the open right half plane resulting in a system with non-minimum

phase. The system will then have a negative response initially to a positive step input in a sense opposite to the response expected. This behaviour is similar to that of positive feedback and it will increase the difficulty of designing an appropriate control scheme for that system.

5.3.7.3 The Choice Of Pole Positions

The decisions that are involved in specifying the closed-loop pole positions cannot be designated by a set of fixed rules. In general \mathbf{K} is chosen such that the dominant poles of the closed-loop system have good damping factors and lie sufficiently far to the left of the origin, resulting in a well-behaved, quickly decaying dynamic response.

5.3.7.4 Limitations In Pole Selection

Although \mathbf{K} can be chosen to move the poles of the closed-loop system to any position, this is in practice not possible. If the poles are moved by too large an amount the elements of matrix \mathbf{K} are found to be large thus saturating the inputs to the plant. In addition small parameter changes of the plant result in large changes in the closed-loop pole positions. Furthermore, the steady-state gains of the closed-loop system, which are related to the zeroes produced by the matrix \mathbf{K} , may be too large and cause saturation of the system outputs.

5.3.7.5 Resulting Noise Sensitivity

An important factor governed by the gain of the feedback matrix \mathbf{K} is the system sensitivity to noise. If the state measurements are contaminated with noise and the feedback

gains are too large, the system inputs will be driven by noise thus impairing the control system considerably, or even resulting in a so-called Bang-Bang controller. These problem can avoided by keeping the elements of the \mathbf{K} matrix sufficiently small and by proper tuning of an observer, which is discussed in section 5.4.

5.3.7.6 System Interaction

The resulting interaction between elements of the closed-loop system from a choice of \mathbf{K} cannot be formally predicted by the theory and may also increase the problem of finding a suitable control scheme. Decoupling is possible in pole assignment(21,22) by designing an additional input compensator.

5.3.7.7 Closed-Loop Transient Response

The example given in section 5.3.6 has shown that the resulting transfer function will from a dynamic point of view be governed by the assigned pole positions. It is very difficult however, to deduce the transient response to step inputs from the choice of \mathbf{q} and pole positions. The transient response may in fact be unsatisfactory.

The design of a suitable feedback configuration is thus a matter of trial and error and must be combined with a simulation of the closed-loop system to analyse the transient response to step inputs and from it deduce the effects of the feedback matrix \mathbf{K} on the system.(23)

5.4 OBSERVER DESIGN

The pole assignment technique discussed above assumes that all the system states are available for measurement. In most multivariable plants this is not the case and the pole assignment design must include a state estimator. An observer can always be designed to estimate all the system states if the system is fully observable. If the system is not completely observable, then only some states can be estimated limiting the scope of pole selection.

For most practical applications, where the available measurements are contaminated with noise it is found that the Luenberger observer is unsatisfactory and the discussion will focus instead on the Kalman Bucy filter.(13)

5.4.1 THE KALMAN FILTER

The Kalman filter is a state estimator, that is usually used for sampled stochastic systems utilising digital computer control(24). Many different types of Kalman filters(25) are available and they have been successfully applied for linear time-invariant, linear time-variant and also nonlinear system(26).

5.4.2 SAMPLED DATA STOCHASTIC SYSTEMS

Sampled data stochastic systems appear in most digital control schemes where the measurements are made at discrete time intervals and the systems are contaminated by noise.

A state space description of a linear time invariant stochastic system is:

$$\begin{aligned}\dot{\mathbf{x}} &= \mathbf{Ax} + \mathbf{Bu} + \mathbf{w} \\ \mathbf{y} &= \mathbf{Cx} + \mathbf{v}\end{aligned}\tag{5.58}$$

where the covariance of the system input white noise with zero mean is:

$$\text{cov}(\mathbf{w}) = E[\mathbf{w} \mathbf{w}^T] = \mathbf{Q} \delta(\tau)\tag{5.59}$$

and the covariance of the measurement white noise with zero means is:

$$\text{cov}(\mathbf{v}) = E[\mathbf{v} \mathbf{v}^T] = \mathbf{R} \delta(\tau)\tag{5.60}$$

The Kronecker Delta function is denoted by $\delta(\tau)$ and \mathbf{Q} and \mathbf{R} are the system noise and the observation noise covariance matrices respectively.

The Kalman filter requires that the measurement and the system input noise is uncorrelated, i.e.:

$$E[\mathbf{w} \mathbf{v}^T] = 0$$

The corresponding state equations for the sampled data system, sampled at period T , are as follows:

$$\begin{aligned}\mathbf{x}(n+1) &= \mathbf{\phi} \mathbf{x}(n) + \mathbf{\Phi} \mathbf{u}(n) + \mathbf{w}_d(n) \\ \mathbf{y}(n) &= \mathbf{Cx}(n) + \mathbf{Du}(n) + \mathbf{v}_d(n)\end{aligned}\tag{5.61}$$

where

$$\text{cov}(\mathbf{w}_d(n)) = E[\mathbf{w}_d(n) \mathbf{w}_d^T(n)] = \mathbf{Q}_d \delta(\tau)\tag{5.62}$$

$$\text{cov}(\mathbf{v}_d(n)) = E[\mathbf{v}_d(n) \mathbf{v}_d^T(n)] = \mathbf{R}_d \delta(\tau)\tag{5.63}$$

The relationship between the discrete and continuous system(5) is:

$$\mathbf{\phi} = e^{\mathbf{AT}} \approx \mathbf{I} + \mathbf{AT}\tag{5.64}$$

$$\Phi = \int_0^T e^{\mathbf{A}\tau} \mathbf{B} d\tau \approx \mathbf{B}T \quad (5.65)$$

$$\mathbf{Q}_d = \int_0^T e^{\mathbf{A}\tau} \mathbf{Q} (e^{\mathbf{A}\tau})^T d\tau \approx \mathbf{Q}T \quad (5.66)$$

$$\mathbf{R}_d = \mathbf{R} \quad (5.67)$$

The approximations shown above only hold for short sample periods T compared to the time constants associated with the matrix \mathbf{A} .

5.4.3 KALMAN FILTER EQUATIONS

There are many different ways to implement the Kalman filter(27). The following asymptotic state estimator equations were used for linear time invariant (LTI) systems to implement the Kalman filter.

The system must be observable, allowing all states to be estimated, i.e.:

$$\mathbf{O} = (\mathbf{C}^T (\mathbf{CA})^T (\mathbf{CA}^2)^T \dots (\mathbf{CA}^{n-1})^T)$$

has rank n .

then the discrete-time model is:

$$\hat{\mathbf{x}}(n+1) = \Phi \hat{\mathbf{x}}(n) + \mathbf{M}(n) \{ \mathbf{y}(n) - \mathbf{C}\hat{\mathbf{x}}(n) - \mathbf{D}\mathbf{u}(n) \} + \Phi \mathbf{u}(n) \quad (5.68)$$

$$\mathbf{P}(n) = \mathbf{R}_d + \mathbf{C} \mathbf{G}(n) \mathbf{C}^T \quad (5.69)$$

$$\mathbf{M}(n) = \Phi \mathbf{G}(n) \mathbf{C}^T \mathbf{P}(n)^{-1} \quad (5.70)$$

$$\mathbf{G}(n+1) = \{ \Phi - \mathbf{M}(n)\mathbf{C} \} \mathbf{G}(n) \Phi^T + \mathbf{Q}_d \quad (5.71)$$

where

$\hat{\mathbf{x}}(n+1)$ is the estimate of the actual states $\mathbf{x}(n+1)$.

The matrix \mathbf{M} is termed the *Kalman filter gain* and \mathbf{G} is referred to as the *Error covariance matrix*. The initial value of $\mathbf{G}(0)$ can be assumed to be zero. If the value of $\mathbf{G}(0)$ is known more accurately, it can be used to reduce the duration of the initial transient.

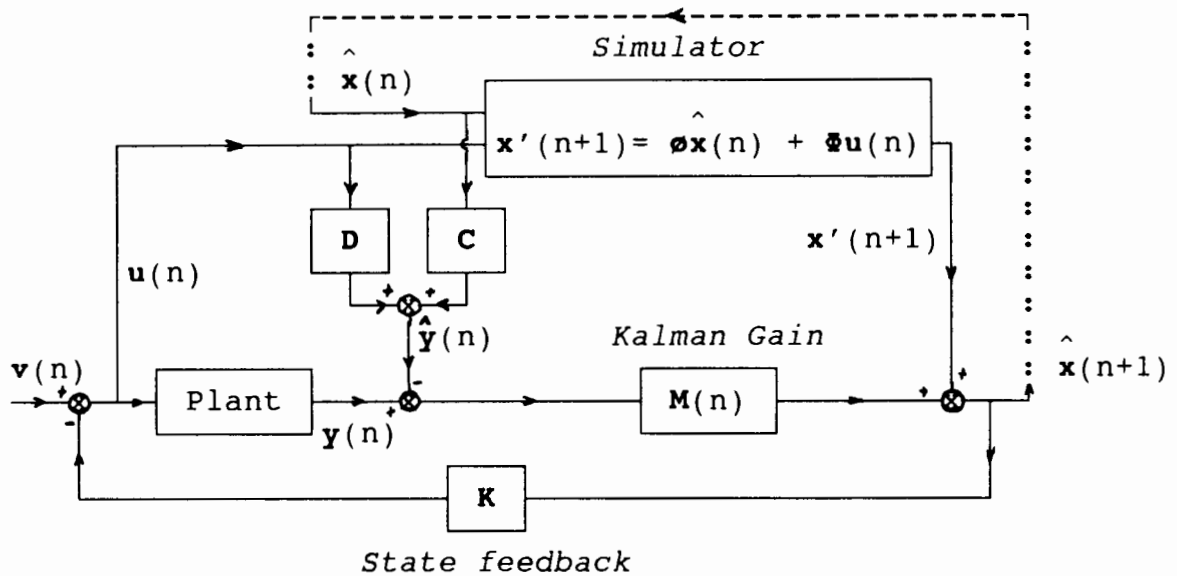


FIG. 5.5 State Feedback System with Kalman Filter

Fig. 5.5 shows the system configuration in block diagram form to implement pole assignment with the use of a Kalman filter. The diagram includes a simulator that calculates the new system states $\hat{\mathbf{x}}'(n+1)$ using the previous states $\hat{\mathbf{x}}(n)$ and the current plant input $u(n)$. The evaluated states are then corrected through the Kalman gain matrix to produce the new state estimates $\hat{\mathbf{x}}(n+1)$, which will replace $\hat{\mathbf{x}}(n)$ on the next cycle. The amount by which the states are corrected depends

on the error between the estimated $\hat{\mathbf{y}}(n)$ and actual plant outputs $\mathbf{y}(n)$.

From Eqs. (5.69), (5.70) and (5.71) it can be seen that the matrix $\mathbf{M}(n)$ develops purely from the covariance matrices \mathbf{Q}_d and \mathbf{R}_d , and will approach limiting values independent of $\mathbf{G}(0)$ if the LTI system is stable. It follows that matrix $\mathbf{M}(n)$ can be calculated off-line and only Eqn. (5.68) needs to be computed at each iteration $n = 0, 1, 2, \dots, \infty$. This is only true for LTI systems and in the case of time variant system matrices $\mathbf{P}, \mathbf{M}, \mathbf{G}$ must be computed for each step.

It is important to note, that both \mathbf{R}_d and \mathbf{Q}_d may not be zero, because then the algorithm fails to find an optimal matrix $\mathbf{M}(n)$. The matrix \mathbf{Q}_d may be zero, but then $\mathbf{G}(0)$ must contain some non-zero elements.

5.4.4 ESTIMATION OF VARIANCES

The difficulty of designing a Kalman filter lies in the estimation of the covariance matrices \mathbf{Q}_d and \mathbf{R}_d . (28,29) Both these matrices are usually assumed to be diagonal, as the individual noise signals are generally uncorrelated. The coefficients then represent the variance or amplitude of the noise signals affecting the states and outputs of the system.

In most cases it is simple to find \mathbf{R}_d because the variance or uncertainty of the measurements can be deduced from the inaccuracies of the instruments used. Alternatively, \mathbf{R}_d can be calculated from a series of measurements while the external noise input is removed or sufficiently reduced.

Finding the matrix \mathbf{Q}_d however, poses a problem because it is difficult to deduce which states are contaminated by noise

and to estimate the magnitude of the noise signals. A detailed discussion on the calculation of the variance matrices, if they are known for the continuous case, has been given by Brown.(30)

An alternative approach is related to the design of Luenberger observers(5). After having chosen some matrices R_d and Q_d iterate Eqs. (5.69), (5.70) and (5.71) until matrix $M(n)$ reaches its limiting values M and then the response of the estimator is governed by

$$\begin{aligned}\dot{\hat{x}} &= \mathbf{A}\hat{x} + \mathbf{B}u + \mathbf{M}(y - \mathbf{C}\hat{x}) \\ &= (\mathbf{A} - \mathbf{M}\mathbf{C})\hat{x} + \mathbf{B}u + \mathbf{M}y\end{aligned}\quad (5.72a)$$

Where the 'error' of the estimator behaves according to:

$$\dot{(\hat{x} - x)} = (\mathbf{A} - \mathbf{M}\mathbf{C})(\hat{x} - x)\quad (5.72b)$$

The matrices R_d and Q_d should be selected to ensure that the eigenvalues of $(\mathbf{A} - \mathbf{M}\mathbf{C})$ result in transient responses of the estimator errors that are stable and well-behaved.

If in addition, the time constants of the estimator error equation are kept sufficiently fast to allow the estimator to track the system states, but yet slow enough to be ignorant to system noise, the resulting filter should be adequate.

An intuitive approach to estimate the system input covariance matrix for the flotation rig in particular, will be discussed in detail in chapter six. This method uses a simulation of the plant to estimate the variances of the system noise input vector w . A white noise signal, with specific variance, is applied to a plant simulator and the variance of the output is computed. The variance of the

input signal is then adjusted until the simulated output variance corresponds to that found at the plant. The input variance so found is then used to develop \mathbf{Q}_d .

5.5 CONCLUSION

Although greater degrees of freedom are available in the design of pole assignment in multivariable than in single-variable system it is very difficult to take advantage of them in a formal way, because of the problems associated with the zero locations, steady state gain, and interaction of the resulting closed-loop system.

It was also shown that the amount by which the poles can be shifted in practice is severely limited.

A further disadvantage of the pole assignment technique is the need to design an observer to estimate the system states, which is usually necessary for multivariable systems. The choice of the system model is thus critical not only for the pole assignment design, but also for the estimation of the states.(31) If the model used by the observer is unsatisfactory then the pole assignment method will not operate properly.

6. APPLICATION OF POLE ASSIGNMENT

6.1 INTRODUCTION

Application of the theory on pole assignment and Kalman filter design, which has been discussed previously in chapter five is discussed. The application is specific to the flotation rig and aimed at controlling the Rougher and Scavenger tanks in particular.

A Kalman filter is designed to estimate the states of the two-tank system, because they could not be measured directly from the plant. An intuitive method to estimate the covariance matrices by simulation techniques is developed.

The pole-assignment technique is applied to the system by state feedback to improve its speed of response.

6.2 FLOTATION RIG MODEL

The state-space description of the two-tank model is constructed from chapter two, where

$$\begin{aligned}\dot{\mathbf{x}}(s) &= \mathbf{Ax}(s) + \mathbf{Bu}(s) \\ \mathbf{y}(s) &= \mathbf{Cx}(s)\end{aligned}\tag{6.1}$$

with

$$\mathbf{A} = \begin{bmatrix} -3.95\text{E-}2 & -5.9\text{E-}4 & 0 & 0 & 0 & 0 \\ 1 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & -4.07\text{E} & -2.20\text{E-}4 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & -1.87\text{E-}2 & 0 \\ 0 & 0 & 0 & 0 & 0 & -1.19\text{E-}2 \end{bmatrix}$$

$$\mathbf{B} = \begin{bmatrix} 1 & 0 \\ 0 & 0 \\ 0 & 1 \\ 0 & 0 \\ 1 & 0 \\ 0 & 1 \end{bmatrix}$$

and

$$\mathbf{C} = \begin{bmatrix} 1.40\text{E-}2 & 6.83\text{E-}5 & 0 & 1.53\text{E-}4 & 0 & 0 \\ 0 & 0 & 0 & 0 & -1.22\text{E-}2 & 5.97\text{E-}3 \end{bmatrix}$$

In this model y_1 and y_2 refer to the Rougher and Scavenger tank levels respectively, u_1 and u_2 corresponds to the Rougher and Scavenger valves respectively.

6.3 A KALMAN FILTER FOR THE FLOTATION RIG

It was necessary to design a Kalman filter for the flotation rig before applying the pole assignment technique, because the states of the plant could not be measured from it directly.

The model must include noise inputs for the design of the Kalman filter.

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The model describing the flotation rig with system noise vector w and measurement noise vector v is then

$$\begin{aligned}\dot{\mathbf{x}} &= \mathbf{Ax} + \mathbf{Bu} + \mathbf{w} \\ \mathbf{y} &= \mathbf{Cx} + \mathbf{v}\end{aligned}\tag{6.2}$$

6.3.1 CALCULATION OF SAMPLE MEAN AND VARIANCE

At this point it is necessary to recall how the variance of a collection of measurements can be found. (6)

The mean value of a sample x_1, x_2, \dots, x_n is defined by the formula:

$$\bar{x} = \frac{1}{n} \sum_{j=1}^n x_j\tag{6.3}$$

The variance of a sample is given by:

$$\sigma^2 = \frac{1}{n-1} \sum_{j=1}^n (x_j - \bar{x})^2\tag{6.4}$$

where $\sigma = \sqrt{\sigma^2}$ is the standard deviation of the sample.

6.3.2 ESTIMATION OF MEASUREMENT NOISE MATRIX

The level of each tank was observed under stationary conditions to find the measurement co-variance matrix \mathbf{R} . The Rougher and Scavenger tanks were filled with water. All pumps were switched off and all valves closed. When the levels \mathbf{y} had settled down, a number of measurements of the levels were taken to estimate \mathbf{v} .

A time-series of the observed level measurements of the Rougher and Scavenger tanks are shown in Fig. 6.1. It can be

CHAPTER 6 APPLICATION OF POLE ASSIGNMENT

The variance of the measurements are calculated using Eqn. (6.4), and found to be

$$\begin{aligned}\sigma^2_{\text{Rougher}} &= 0.98 \approx 1 \text{ Units}^2 \\ \sigma^2_{\text{Scavenger}} &= 0.90 \approx 1 \text{ Units}^2\end{aligned}\tag{6.5}$$

The measurement covariance matrix is then simply

$$\mathbf{R}_d = \mathbf{R} = \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix}\tag{6.6}$$

The off-diagonal elements of \mathbf{R}_d are zero, because the quantization error of the Rougher measurement is uncorrelated with that of the Scavenger.

6.3.3 ESTIMATION OF SYSTEM INPUT NOISE MATRIX

It was relatively easy to find the measurement noise covariance matrix \mathbf{R} . To estimate the system input noise covariance matrix \mathbf{Q} from a theoretical basis does however pose a problem. Instead of using an explicit approach, the solution can be found from the following intuitive treatment of the problem, which was developed specifically for the flotation rig.

The system input noise covariance matrix \mathbf{Q} is estimated in the following manner. Firstly, the plant output noise variance is determined from a set of measurements done on the plant during normal operation at steady-state. From it the measurement noise variance found previously is subtracted and an input noise variance resulting in that output variance is determined by simulation.

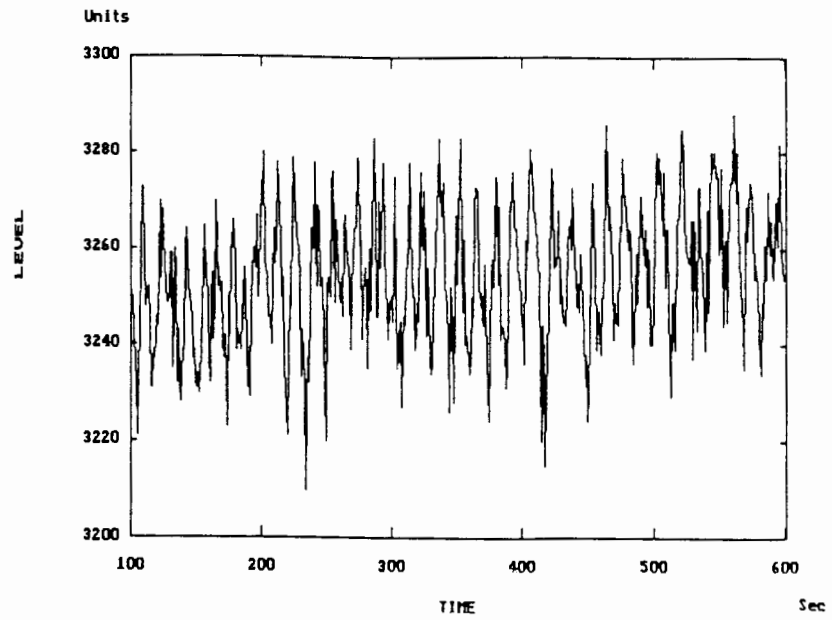
The input noise variance so obtained can then be used to estimate the covariance matrix \mathbf{Q} .

6.3.3.1 Determination of Plant Output Variance

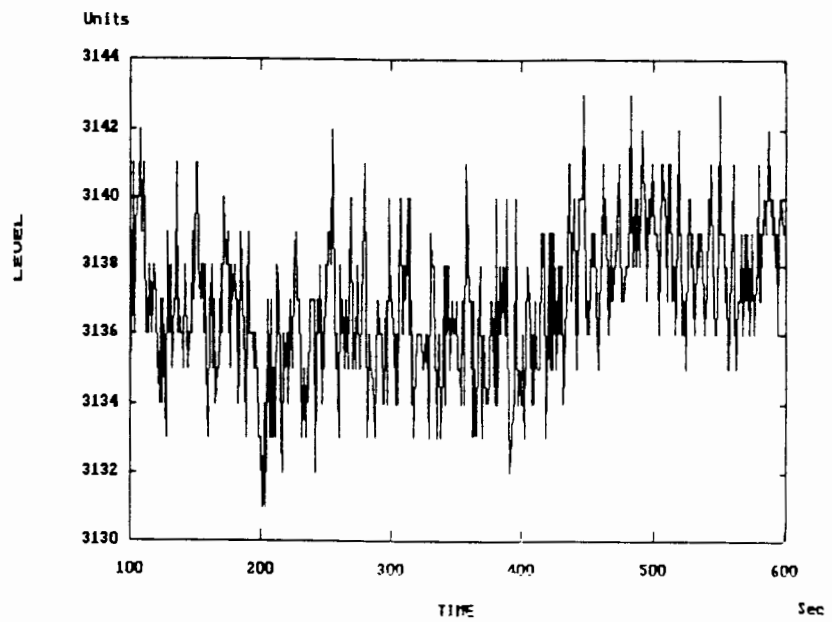
To estimate the system output noise variance, measurements of the levels of the Rougher and Scavenger tanks at steady-state were taken. The levels of all tanks were brought to their operating levels by the use of the single-loop PI controller as discussed in chapter two. When the tanks attained the desired levels the valves were fixed at their current setting.

After a period of about 10 minutes had elapsed to allow the rig to settle down and reach steady-state, a number of measurements of the Rougher and Scavenger Tanks were taken. The time-series for these measurements, which were done at 1 second intervals, are shown in Fig. 6.2.

CHAPTER 6 APPLICATION OF POLE ASSIGNMENT



a) Rougher Tank



b) Scavenger Tank

FIG. 6.2 Steady-state level measurements at operating levels

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The variance of the above measurements, which now include the system input noise, is calculated and found to be:

$$\begin{aligned}\sigma^2_{\text{Rougher}} &= 199 \text{ Units}^2 \\ \sigma^2_{\text{Scavenger}} &= 5.20 \text{ Units}^2\end{aligned}\tag{6.7}$$

It is important to determine whether the variances found above do converge. If they do not converge then this will be an indication that either too few samples were taken or that the levels drifted. If the levels did indeed drift then the plant had not been at steady state, because the plant is open-loop stable and in that case the variances found above would not be correct.

The variances of the level measurements are calculated at each sampling interval using the past samples and a time-series of the variance versus time (or number of samples) for both the Rougher and Scavenger outputs are shown in Fig. 6.3.

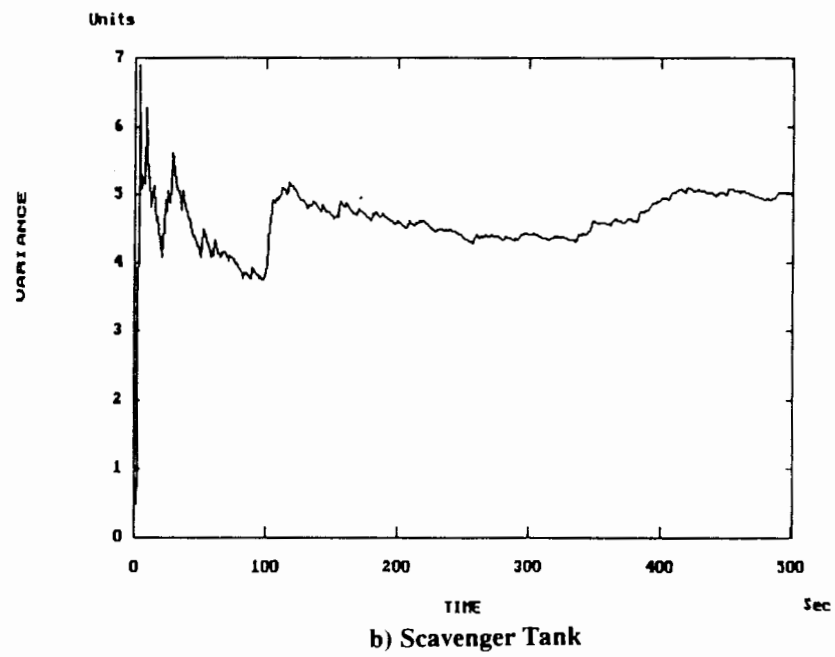
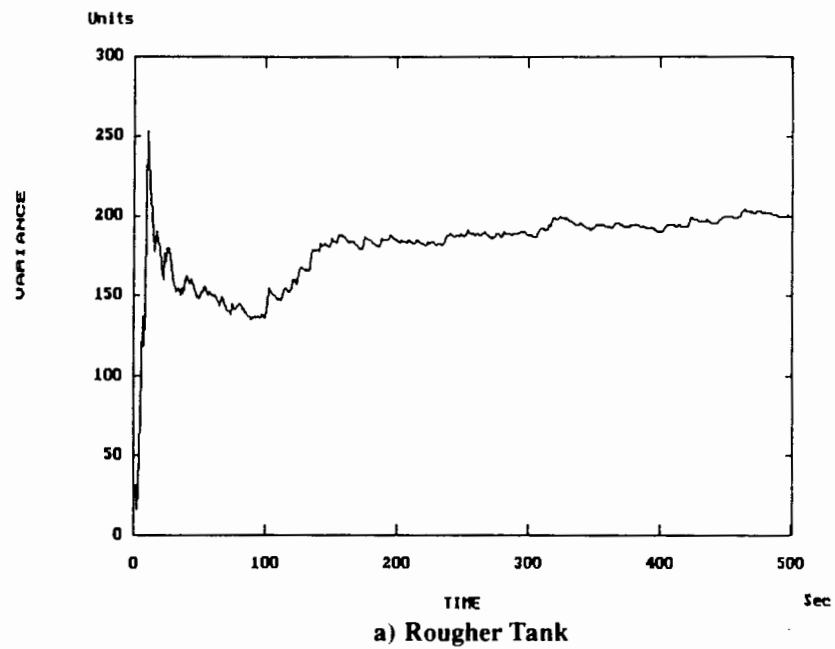


FIG. 6.3 Calculation of variances

From Fig. 6.3, it can be seen that the respective variances do indeed converge to limiting values as the number of samples increases.

Assuming that the input and measurement noise signals are uncorrelated, then the respective variances, due to input noise only are

$$\begin{aligned}\sigma^2_{\text{Rougher}} &= 199-1 \approx 200 \text{ Units}^2 \\ \sigma^2_{\text{Scavenger}} &= 5.2-1 \approx 4 \text{ Units}^2\end{aligned}\quad (6.8)$$

To justify the above calculation, it is important to note that the variance of the sum of independent random variables equals the sum of the variances of these variables.(6)

6.3.3.2 System Simulation With White Noise Inputs

Having established the output variances that are due to the system white noise $\mathbf{w}(s)$ vector only, it is now necessary to estimate the variances of $\mathbf{w}(s)$ itself, that would result in the system output having the variances given in Eqn. (6.8). To derive this analytically from the system model is cumbersome as mentioned before and instead the following technique is applied.

The plant is simulated on a digital computer. A white noise signal of given variance is then applied to the individual inputs \mathbf{u} of the system and the noise on the corresponding system output \mathbf{y} is determined. These are then compared to that of the real plant and the variance of the input noise is adjusted until the variance of the output of the simulated plant is approximately the same as that of the real plant.

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To perform the simulation the noise signals of the plant are included in the model in the following way:

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \\ \dot{x}_3 \\ \dot{x}_4 \\ \dot{x}_5 \\ \dot{x}_6 \end{bmatrix} = \mathbf{A} \begin{bmatrix} x_1 \\ x_2 \\ x_3 \\ x_4 \\ x_5 \\ x_6 \end{bmatrix} + \begin{bmatrix} 1 & 0 \\ 0 & 0 \\ 0 & 1 \\ 0 & 0 \\ 1 & 0 \\ 0 & 1 \end{bmatrix} \begin{bmatrix} u_{ro} \\ u_{sc} \end{bmatrix} + \begin{bmatrix} w_1(\sigma_{ro}^2) \\ 0 \\ 0 \\ 0 \\ 0 \\ w_6(\sigma_{sc}^2) \end{bmatrix} \quad (6.9)$$

where σ_{ro}^2 and σ_{sc}^2 are the variances of the uncorrelated white noise inputs to the Rougher and Scavenger tank levels respectively.

For the ensuing discussion, it is necessary to recall that states x_1 and x_2 are related to the Rougher level, x_3 - x_5 correspond to the interaction of the two tank, and x_6 is related to the Scavenger level.

The above model is not a true account of the real plant because the following simplifications were performed.

In the model (6.9) above, the fluctuations of the Rougher tank level are due to a single noise input (w_1) only. In a similar fashion the Scavenger level is only affected by the noise input w_6 . Both noise signals do not affect the interaction between the two tanks.

For the real plant, it can be argued that the noise injected onto the Rougher would affect the level of the Scavenger, but a more precise model of the plant would have resulted in an unnecessarily complicated description. The results, that

will be obtained later, will show, that the model was in fact adequate.

6.3.3.3 Simulation Of The Normal Distribution

Having established the model that is to be used to simulate the plant with noise inputs, it is now necessary to derive a method to simulate those white noise inputs numerically.

The pseudo-random-number generators that are available for personal computers through *BASIC* or *TURBO PASCAL*, produce sequences of random numbers, that are uniformly distributed from 0 to 1. Hansen(32) has shown that by summing these numbers a Gaussian distribution can be attained.

The function *random* in *TURBO PASCAL* produces real numbers x_i such that

$$0 \leq x_i < 1 \quad (6.10)$$

The fact that $x_i=1$ is excluded is of little consequence and can be ignored.

The mean value of x_i is then

$$\bar{x} = \frac{1}{2} \quad (6.11)$$

To obtain a normal distribution, the sum S of n such random numbers is computed

$$S = \sum_{i=1}^n x_i \quad (6.12)$$

then the mean value of S is

$$\bar{S} = \frac{1}{2}n \quad (6.13)$$

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with the maximum deviation from the mean for any sample

$$\text{deviation}_{\max} = \frac{1}{2}n \quad (6.14)$$

and the corresponding variance is

$$\sigma^2 = 1/(12n) \quad (6.15)$$

It can be seen from Eqn. (6.14) that n determines the maximum deviation from the mean for any sample. It is therefore necessary to choose n sufficiently large to achieve a wide spread of samples. In addition, as n is increased, the distribution of the simulated sequence will tend to that of a pure Gaussian distribution by the Central Limit Theorem(6).

To obtain a random sample r_σ with specified variance σ^2 , the following algorithm is used:

A) The sum of n random number is computed:

$$S = \sum_{i=1}^n x_i$$

where x_i is obtained from the internal function *random*.

B) Adjusting the sum to have a mean of zero as follows:

$$S_0 = S/n - 0.5$$

C) The sample r_1 with unity variance is computed from

$$r_1 = S_0 \sqrt{12n}$$

D) A random sample r_σ with variance σ^2 is obtained from

$$r_\sigma = \sigma r_1$$

(6.16)

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Steps C) and D) are valid statistically and have been proved elsewhere. (6)

The procedure above is repeated to obtain a sequence of normally distributed numbers with zero mean and with fixed variance.

A value of $n=50$ is used for the simulation done below. This value results in an acceptable distribution and computational times for the simulation are tolerable.

The following test sequence was performed, initially for the Rougher tank and then for the Scavenger tank.

The input noise variance was selected arbitrarily and used to generate normally distributed samples. The actual input noise variance was found from the samples so generated. These samples were then applied to the simulated tank noise inputs. The variance of the resulting tank level was then found and tabulated.

This procedure was repeated for each selected input variance, to give an indication of the repeatability of the experiments. The input variance was then increased until the output variance was similar to that of the real plant.

The noise input variances corresponding to a system output variance as found in Eqn. (6.8) can be read from Tables (6.1), (6.2) and estimated.

Input Noise Variance	Actual Input Noise Variance	Output Variance
1	0.980	0.00177
1	1.020	0.00174
1,000	975.000	2.73000
1,000	1,067.000	1.78000
100,000	97,800.000	341.00000
100,000	95,400.000	247.00000

TABLE 6.1 Rougher tank simulation results

Input Noise Variance	Actual Input Noise Variance	Output Variance
1	0.98	0.00177
1	1.02	0.00174
1,000	975.00	2.73
1,000	1,067.00	1.78
100,000	97,800.00	341.00
100,000	95,400.00	247.00

TABLE 6.2 Scavenger tank simulation results

The variance of the system noise signal w_1 is thus

$$\sigma_{ro}^2 \approx 100,000$$

and that for w_6 is

$$\sigma_{sc}^2 \approx 10,000 \tag{6.17}$$

The input noise signals were assumed to be uncorrelated and a sampling period τ of 1 second is used. The system noise covariance matrix is then

$$\mathbf{Q}_d \approx \mathbf{Q}\tau = E(\mathbf{w} \mathbf{w}^T)\tau = \begin{bmatrix} 100,000 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 10,000 \end{bmatrix} \quad (6.18)$$

6.3.4 KALMAN GAIN MATRIX

The resulting Kalman gain matrix was calculated using the equations from chapter five.

After 414 iterations the gain matrix converged with 4 digit accuracy to

$$\mathbf{M} = \begin{bmatrix} 65.40 & 0 \\ 71.14 & 0 \\ 0 & 0 \\ 0 & 0 \\ 0 & 0 \\ 0 & 72.85 \end{bmatrix} \quad (6.19)$$

6.3.5 DYNAMIC RESPONSE OF FILTER

From matrix \mathbf{M} above, it can be seen that only states $\mathbf{x}_1, \mathbf{x}_2$ and \mathbf{x}_6 will be corrected by the Kalman filter. The remaining states are estimated solely from a plant simulation. This is as expected because of the block-diagonal structure of matrix \mathbf{A} and the format of the chosen noise vector \mathbf{w} .

The dynamic behaviour of the estimator 'error' can be predicted from the eigenvalues of $(\mathbf{A}-\mathbf{MC})$. (4)

$$\mathbf{A-MC} = \begin{bmatrix} -0.9550 & -0.00506 & 0 & -0.01000 & 0 & 0 \\ 0.00404 & -0.00486 & 0 & -0.01090 & 0 & 0 \\ 0 & 0 & -0.0407 & -0.00022 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & -0.0187 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0.8890 & -0.447 \end{bmatrix}$$

with eigenvalues in rad/sec corresponding to states x_i are at

$$\begin{aligned} s_1 &= -9.5508E-01 + 0j \\ s_2 &= -4.8815E-03 + 0j \\ s_3 &= -3.4283E-02 + 0j \\ s_4 &= -6.4172E-03 + 0j \\ s_5 &= -1.8700E-02 + 0j \\ s_6 &= -4.4681E-01 + 0j \end{aligned} \quad (6.20)$$

It can be seen that all eigenvalues have real parts only. The dynamic response of the filter 'error' will therefore be well-behaved.

Comparing the eigenvalues above to those of Eqn. (6.21) shows that the states x_3 - x_5 have identical time-constants as those of the model, which is to be expected. The time-constants associated with states x_1 , x_2 and x_6 have however changed drastically. The states x_1 and x_6 are estimated with time-constants that are faster than those of the model by a factor of 50, which is excellent. The eigenvalue associated with state x_2 is however very small compared to that of the model. From a point of asymptotic observer design, it can be argued that this fact may impede the performance of the Kalman filter, because the settling time for the estimation of x_2 if the plant remains at steady-state is about

$$4/4.88E-3 \approx 820 \text{ seconds.}$$

Because the true states of the plant are unknown, it is difficult to ascertain how well the Kalman filter operates. To judge the filter's success by comparing the estimated with the actual output levels is ineffective because the algorithm is based on correcting the states based on that information. It is thus not possible to determine from an application of the estimator alone, if the large time-constant does in fact impede its performance. All that could be determined in this manner is whether the states reach limiting values, if the tank is in steady-state.

As the pole assignment technique by state feedback relies on the correct estimation of the system states, the employment of pole assignment can be used not only to discuss its success, but also the quality of the Kalman filter.

6.4 APPLICATION OF POLE ASSIGNMENT

This section will demonstrate the application of pole assignment on the laboratory flotation rig. The main purpose of the discussion will be to show the difficulty of determining gain margins and to what extent the simulated response will correspond to that of the real plant. The results that will be obtained can then be used to judge the performance of pole assignment on a real plant.

6.4.1 OPEN-LOOP POLE CONSIDERATIONS

The eigenvalues of the matrix \mathbf{A} in the plant model, give an indication of the dynamic response of the system. As pole assignment is primarily concerned with moving these eigenvalues to 'better' positions, the open-loop pole positions have to be analysed first.

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The eigenvalues in rad/sec of \mathbf{A} that are related to the i th state are found to be:

$$s_1 = -1.9750E-02 - 1.4175E-02j$$

$$s_2 = -1.9750E-02 + 1.4175E-02j$$

or

$$s_2 = -1.9750E-02 - 1.4175E-02j$$

$$s_1 = -1.9750E-02 + 1.4175E-02j$$

and

$$s_3 = -3.4283E-02 + 0j$$

$$s_4 = -6.4172E-03 + 0j$$

or

$$s_4 = -3.4283E-02 + 0j$$

$$s_3 = -6.4172E-03 + 0j$$

and

$$s_5 = -1.8700E-02 + 0j$$

$$s_6 = -1.1900E-02 + 0j \quad (6.21)$$

The above results are obtained from the eigenvalue routine listed in the *Software Reference*. Due to the block diagonal structure of matrix \mathbf{A} , the eigenvalues could be related to specific states. For a general \mathbf{A} matrix this is not possible.

Analysis of the above eigenvalues shows that the open-loop poles all in the left-half of the s -plane which ensures stability. This was expected because the plant showed no signs of instability at the chosen operating levels. Unfortunately, the main feature of pole assignment, namely

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to improve stability, can thus not be demonstrated in this case.

The poles can however be moved further away from the origin to improve the stability margin. If the inherent nonlinearities of the rig, which have been ignored in the model, should move these poles nearer to the origin, a larger stability margin will be advantageous.

In addition, moving the poles away from the origin will also improve the speed of the dynamic response of the system. As the flotation rig is a very slow process, with time-constants ranging from 1 to 3 minutes [see Eqn. 6.21], it is desirable to improve its speed of response.

A further improvement on the pole positions can be achieved by forcing the poles to be real. Although no oscillations were detected from the plant step responses, it will be better to make the imaginary parts of the complex poles as small as physically possible.

The following approach will be used to analyse the performance of pole assignment. The imaginary parts of the eigenvalues are reduced by a factor of 10 and the poles are moved progressively further away from the origin.

No considerations are given to system performance criteria such as interaction and steady-state gain during the initial design, because these are difficult to predict from the selected vector \mathbf{q} and pole positions, as has been shown previously in chapter five. It was in fact found that the closed-loop step responses were generally unpredictable, which becomes apparent from the results discussed later.

6.4.2 CONTROLLABILITY CRITERION

The \mathbf{q} -vector was arbitrarily selected to be

$$\mathbf{q} = (1, 1)^T \quad (6.22)$$

This choice fulfilled the controllability criterion, because the determinant of the controllability matrix \mathbf{P} was found to be

$$|\mathbf{P}| = 1.3\text{E-}24 \neq 0 \quad (6.23)$$

This value is very small numerically, which is to be expected because the elements of \mathbf{A} are in the order of 1/100. This does however show the limitations in the numerical technique to determine controllability. If the order of the model is very large and the elements of \mathbf{A} are not ≈ 1 , then the resulting determinant will either be too large and cause an overflow, or be too small and result in a value of zero. In both cases the calculated determinant of \mathbf{P} will give no indication of controllability or otherwise.

6.4.3 CLOSED-LOOP POLE POSITIONS

Four different sets of pole positions were selected to increase the speed of response of the flotation rig progressively as depicted in Table 6.3 (An increase of speed by 100% corresponds to doubling the speed of response). O/L indicates the approximate open-loop system pole positions.

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Speed	Closed-Loop Pole Positions
O/L	$(-2.00E-2, -1.50E-2), (-2.00E-2, +1.50E-2), (-3.50E-2, 0), (-6.50E-3, 0), (-1.90E-2, 0), (-1.20E-2, 0)$
1: 10%	$(-2.20E-2, -1.50E-3), (-2.20E-2, +1.50E-3), (-3.85E-2, 0), (-7.15E-3, 0), (-2.09E-2, 0), (-1.32E-2, 0)$
2: 20%	$(-2.40E-2, -1.50E-3), (-2.40E-2, +1.50E-3), (-4.20E-2, 0), (-7.80E-3, 0), (-2.28E-2, 0), (-1.44E-2, 0)$
3: 50%	$(-3.00E-2, -1.50E-3), (-3.00E-2, +1.50E-3), (-5.25E-2, 0), (-9.75E-3, 0), (-2.85E-2, 0), (-1.80E-2, 0)$
4: 100%	$(-4.00E-2, -1.50E-3), (-4.00E-2, +1.50E-3), (-7.00E-2, 0), (-1.30E-3, 0), (-3.80E-2, 0), (-2.40E-2, 0)$

TABLE 6.3 Selected closed-loop pole positions

The corresponding state feedback matrices K_i are calculated with the aid of the routines listed in Appendix D. Both the frequency domain and the controllable companion technique of chapter five result in

$$K_1 = \begin{bmatrix} 1.01E-2 & 2.94E-5 & 2.03E-3 & 3.52E-5 & 1.38E-4 & 7.03E-4 \\ 1.01E-2 & 2.94E-5 & 2.03E-3 & 3.52E-5 & 1.38E-4 & 7.03E-4 \end{bmatrix}$$

$$K_2 = \begin{bmatrix} 1.73E-2 & 2.68E-4 & 4.08E-3 & 1.05E-4 & 5.17E-4 & 2.28E-3 \\ 1.73E-2 & 2.68E-4 & 4.08E-3 & 1.05E-4 & 5.17E-4 & 2.28E-3 \end{bmatrix}$$

$$K_3 = \begin{bmatrix} 1.25E-2 & 7.09E-4 & 3.11E-2 & 1.06E-3 & 1.03E-3 & 1.33E-2 \\ 1.25E-2 & 7.09E-4 & 3.11E-2 & 1.06E-3 & 1.03E-3 & 1.33E-2 \end{bmatrix}$$

$$K_4 = \begin{bmatrix} -1.30E-1 & -2.20E-3 & 3.69E-1 & 1.27E-2 & -5.19E-2 & -7.29E-2 \\ -1.30E-1 & -2.20E-3 & 3.69E-1 & 1.27E-2 & -5.19E-2 & -7.29E-2 \end{bmatrix}$$

(6.24)

6.4.4 OPEN-LOOP GAIN CONSIDERATIONS

This section discusses the effect of variations in the open-loop gain of the plant when state feedback is employed.

From the results above (Eqn. 6.24) and in general it is noteworthy that there is no linear relationship between the elements of matrix \mathbf{K} and the amount by which the poles are moved. It is thus not possible to multiply \mathbf{K} by some constant c to move all the poles by the same proportion. In fact it is difficult to predict in general how the poles will move if \mathbf{K} is replaced by $\alpha\mathbf{K}$. A block diagram of this situation is shown in Fig. 6.4. \mathbf{I}_m is an identity matrix of dimension $m \times m$, where m corresponds to the number of outputs and inputs.

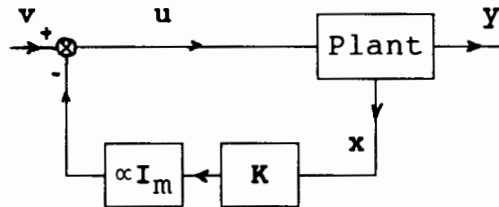


FIG. 6.4 Feedback gain configuration

The reason for this can be found from chapter five, eqn.4.30 where it was shown that the feedback vector \mathbf{f} of $(\mathbf{K}=\mathbf{qf}^T)$ is constructed from the coefficients of the characteristic polynomials for the open- and closed-loop system. By changing some or all poles of the closed-loop system in a linear fashion, the coefficients of the closed-loop characteristic polynomial will not change in a linear way.

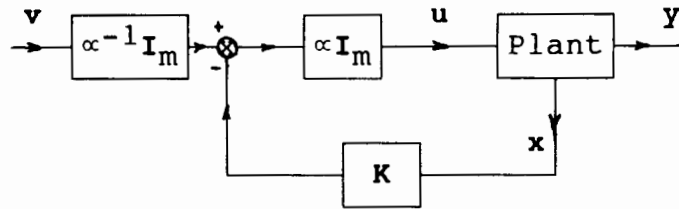


FIG. 6.5 Gain moved into forward path

The feedback gain matrix $\alpha \mathbf{I}_m$ can be moved into the forward path as depicted in Fig. 6.5. In this way α can be regarded as a variation of the open-loop plant gain or as an inaccuracy in the model obtained from the plant.

6.4.5 STABILITY ANALYSIS

Although pole assignment assures stability if the selected pole positions are in the stable region, this can be misleading. The discussion in the previous section has shown that a variation in the open-loop gain of the plant can affect the pole positions of the closed-loop system considerably and could indeed make it unstable.

It is obvious that variations other than open-loop gain could also impede the stability of the system. This can be argued for any control system design method and is therefore not significant for this discussion.

It is however important for a control scheme to give an indication of gain margins. This is especially so in the design of a control system for the flotation rig, because of the inherent non-linearities of the valves, which affect the open-loop gain of the plant.

The valve characteristics could be partially linearised in the same way, that level transducer outputs were linearised in a previous project(11). This is not a satisfactory solution in control system design however, because in most industrial applications the inherent non-linearities can often not be determined numerically. The designed control system should thus be robust enough to tolerate non-linear behaviour of the plant.

6.4.5.1 Gain Margin

The pole assignment technique does not lend itself to an elegant method to determine gain margins of a system. The closed-loop pole positions, including a gain variations matrix \mathbf{P} with diagonal element equal to α_i and off-diagonal elements zero, are given by the roots of

$$|s\mathbf{I}-(\mathbf{A}-\mathbf{PBK})| \quad (6.25)$$

which shows that it is extremely difficult to determine stability margins for \mathbf{P} .

A possible solution would be to examine the root-loci as the open-loop gain matrix \mathbf{P} is varied. This would give an indication of whether the poles remain stable over that range. This method is extremely tedious and relies heavily on the accuracy of the algorithm that computes the roots of Eqn.(6.35).

The alternative, namely to analyse the step response of the system with state feedback, which can also be used to determine stability, is employed here.

6.4.6 CLOSED-LOOP STEP RESPONSE

6.4.6.1 Step Test Procedure

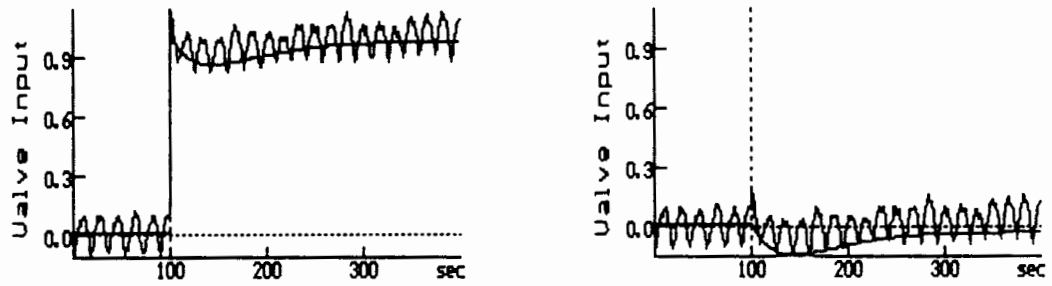
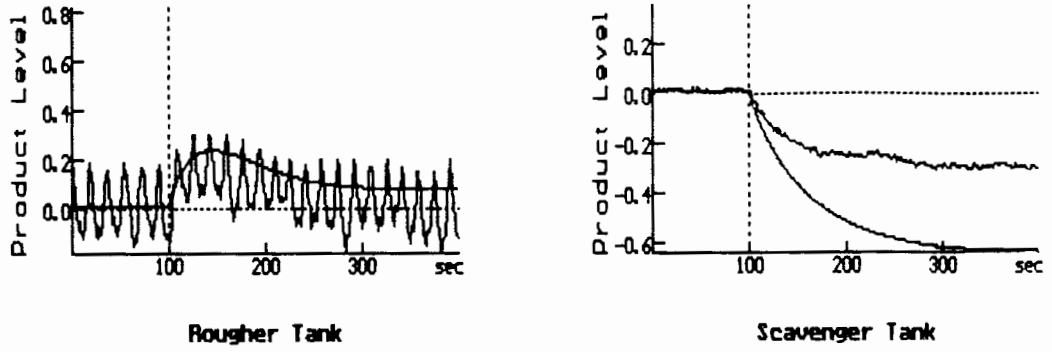
Step responses were performed for the various selections of pole positions on the flotation rig. The step size for all tests was fixed at 10% = 401 units. The step was introduced after 100 seconds. The data is normalised by subtracting the offset and dividing the measurements and the valve inputs by the step size. The offset has to be calculated by averaging the first 100 samples due to the periodic variation. The normalisation is necessary such that the simulated response can be superimposed on the graphs. The original step responses can be found in Appendix C .

6.4.6.2 Step Test 1

The closed-loop step response to increase the speed of response by 10% by is shown in Fig. 6.6.

Actual / Simulated Closed-Loop Step Response

a) Rougher Step Size Normalised



Actual / Simulated Closed-Loop Step Response

b) Scavenger Step Size Normalised

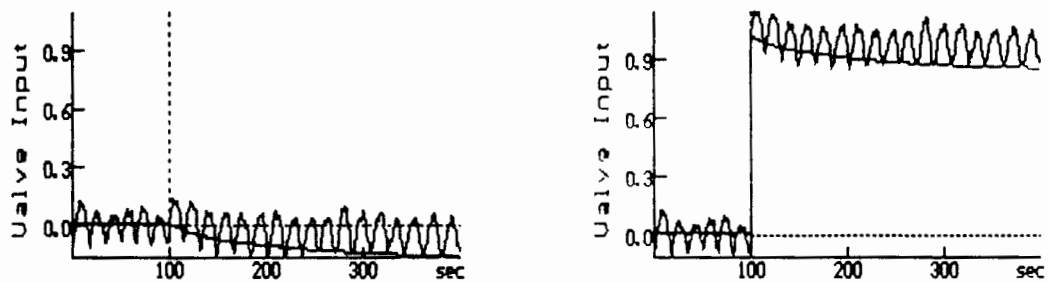
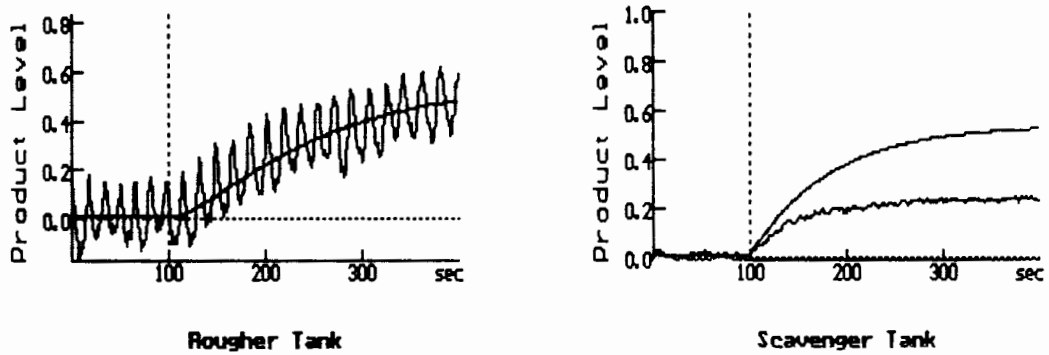


FIG. 6.6 Closed-loop response with 10% increase in speed

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The step responses exhibit a sinusoidal wave that is superimposed on the Rougher level. This phenomena has been discussed in detail in chapter two and found to be due to the pumps cavitating. It is important to note here that these periodic variations are not due to the changing valve inputs, but rather that they cause the sinusoidal behaviour of the inputs.

Analysing the Rougher step response shows that the gain or slope of the cyclic variations on the Rougher level are much larger than that introduced by the step in valve opening, which indicates that the waves on the Rougher level could not have been caused by the Rougher valve.

It can be seen from both the Rougher step and Scavenger step results ignoring the superimposed sinusoid that the dynamic responses of both the levels and the plant inputs correspond very well with the simulated one. This shows that the pole assignment design has produced the expected results.

It is noticeable that the steady-state gain of the Scavenger level is less than predicted by the simulation by a factor of $\frac{1}{2}$. This could have arisen from the non-linearity of the valves. The step in the valve settings may have occurred over a region of low gain, limiting the amount by which the Scavenger level will rise or fall to.

Alternatively, the levels of the four tanks may have moved out of the operation region, from which a model was obtained. If all four step tests are consistently wrong then a probable explanation is that the model is incorrect. This is possible because some valves were replaced during the course of this investigation.

Due to the small increase of 10% in the closed-loop speed of response compared to the open-loop it is difficult to determine whether the designed speed improvement has in fact been achieved in practice. However the experimental and simulated dynamics suggest that it has.

6.4.6.3 Kalman Filter Response

Fig. 6.6 c) depicts the states estimated by the Kalman filter during the above Rougher step with 10% increase in speed of response.

Flotation System Closed-Loop Step Response

c) Rougher Step Size= 410 Units (10%)

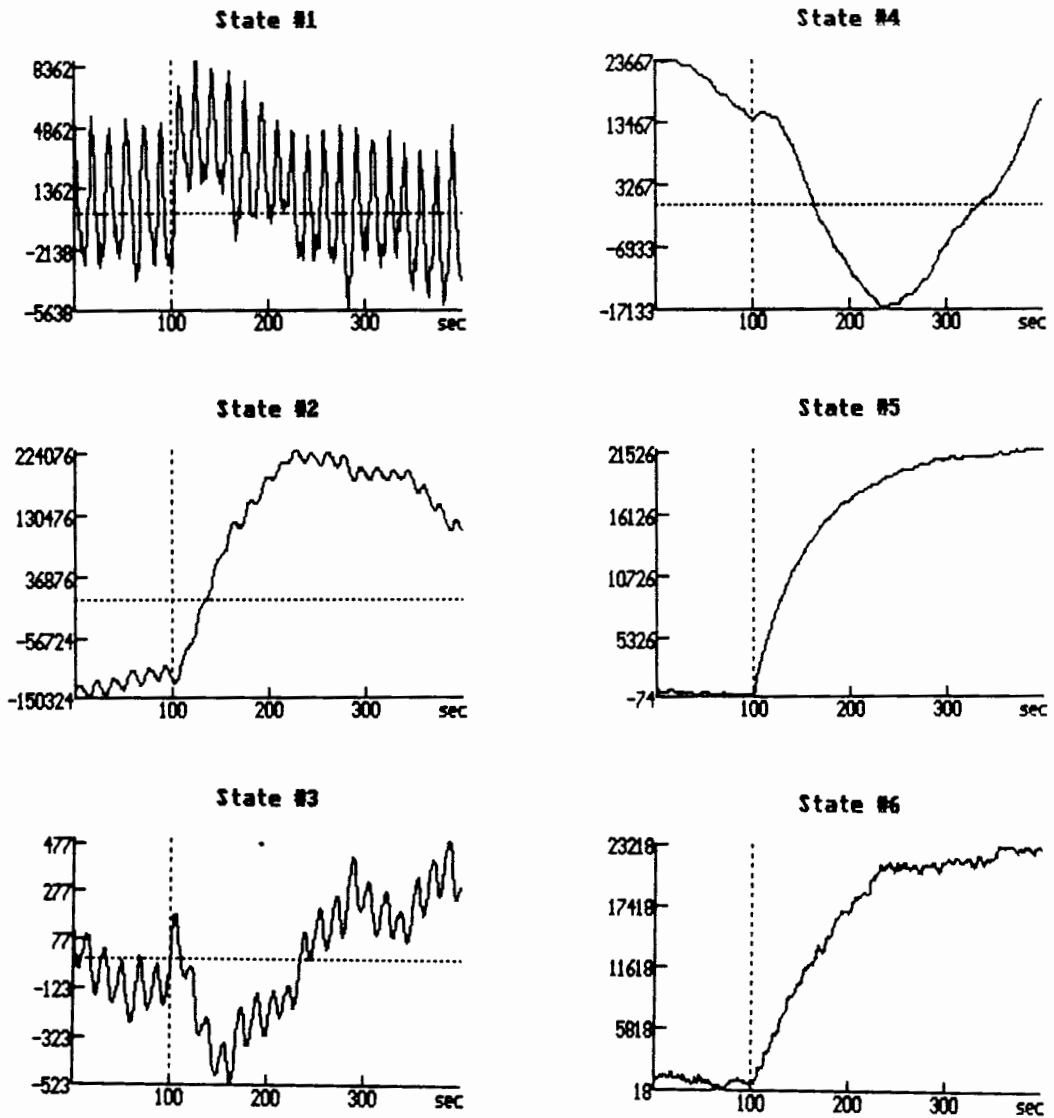


FIG. 6.6 c) Rougher step state response (10% increase in speed)

Analysing the response for state x_2 gives an indication of the long time-constant associated with it, as it had not attained steady state after 400 seconds. This has been mentioned before in [Section 6.3.5]. State x_4 did also not reach steady state. These two states are related to the acceleration of the Rougher level and are thus difficult to interpret from a physical point of view.

In general the states are well behaved with exception of the superimposed sinusoids, which are not introduced by the Kalman filter. It is noticeable, that the states give rise to large numbers and it is important that the digital computer used will be able to treat these without problems or that a normalised model is chosen for use in the filter. In this application, the *TURBO PASCAL* real number format was sufficient.

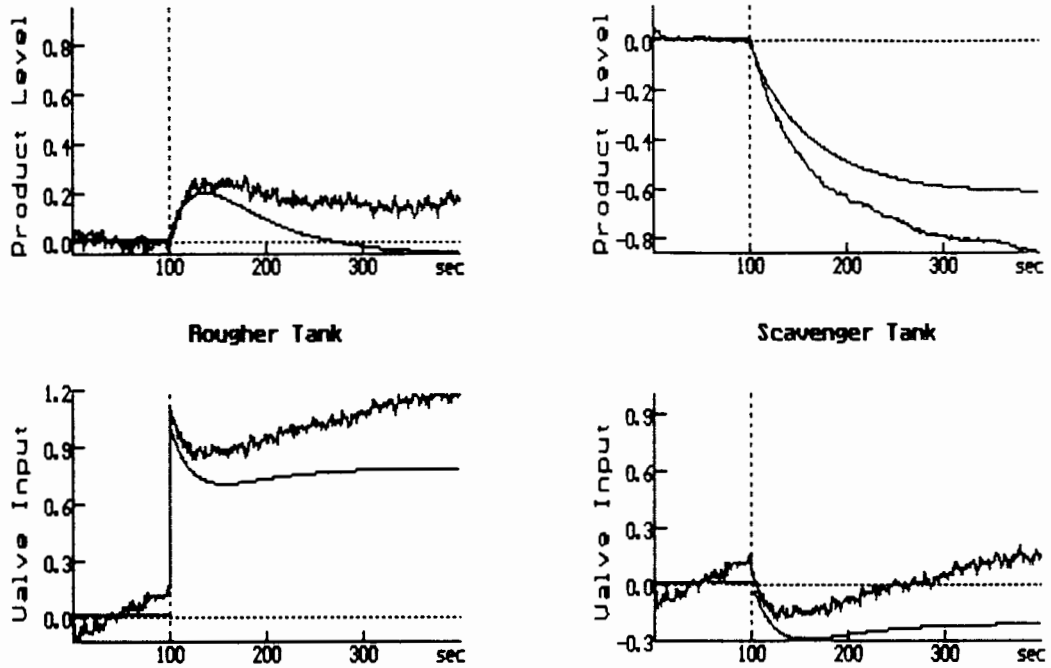
To conclude the discussion on the Kalman filter, the results obtained up to this point have shown convincingly that it operated suitably well. The step responses in Fig. 6.6 agree with those of the simulator and the states in Fig. 6.7 are well behaved.

6.4.6.4 Step Test 2

In Fig. 6.7 the step test results for an increase in speed of 20% are depicted.

Actual / Simulated Closed-Loop Step Response

a) Rougher Step Size Normalised



Actual / Simulated Closed-Loop Step Response

b) Scavenger Step Size Normalised

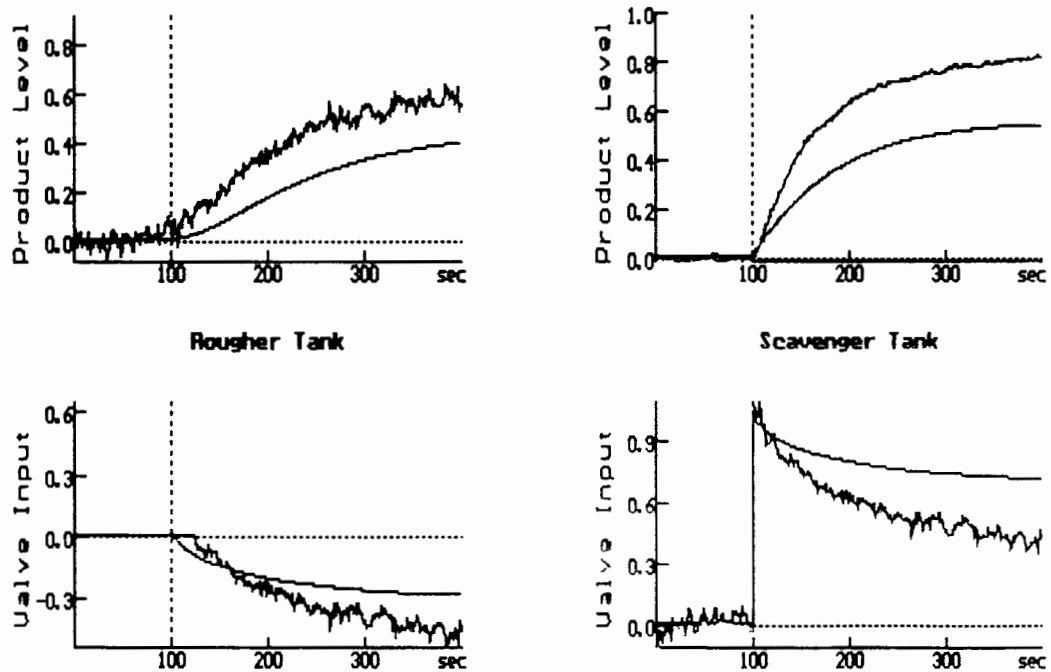


FIG. 6.7 Closed-loop response with 20% increase in speed

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The results in Fig. 6.7 a) show a moderate deviation from the expected response. This fact can be explained by observing that the plant was not completely at steady-state. The rising valve inputs indicate that the levels were drifting. Close examination would show that the Rougher level did indeed drop steadily. This problem has been discussed in chapter two.

The plant response to a Scavenger step input [Fig. 6.7 b)] also deviated from the simulated response. This can be accounted for by inspecting the Rougher valve input, which was at its limit and could not open even more. It did take a significant amount of time (25 sec) for the input to move into the operating range and this will have definitely obscured the plant response.

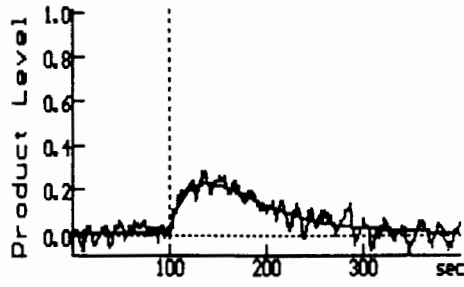
This test in particular underlines the necessity for the plant to be completely at steady-state and for the valves to remain in their operating region throughout the experiment. Only then can the response be successfully compared to a simulated one.

6.4.6.5 Step Test 3

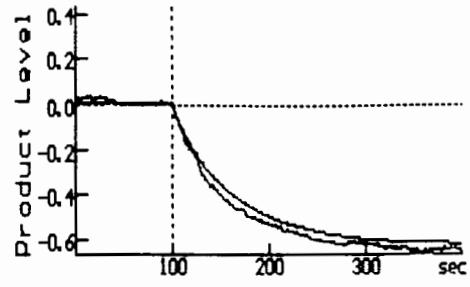
The experiment in Fig. 6.8 used state-feedback to improve the system response time by 50%.

Actual / Simulated Closed-Loop Step Response

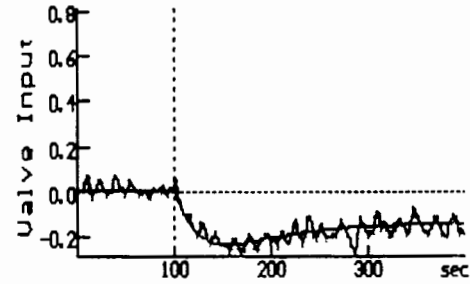
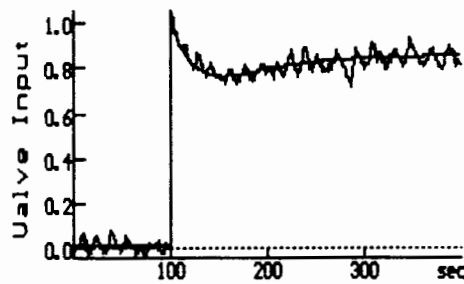
a) Rougher Step Size Normalised



Rougher Tank

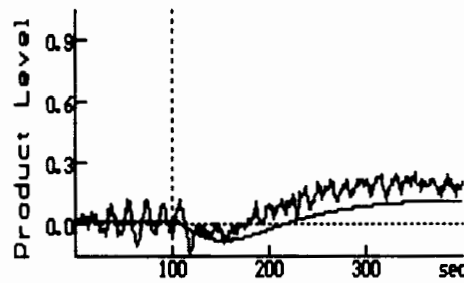


Scavenger Tank

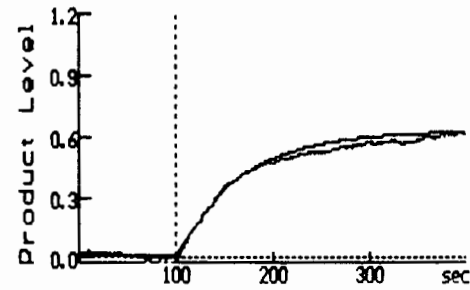


Actual / Simulated Closed-Loop Step Response

b) Scavenger Step Size Normalised



Rougher Tank



Scavenger Tank

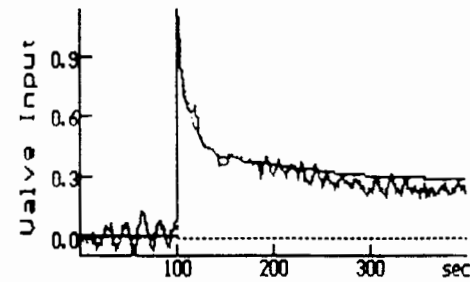
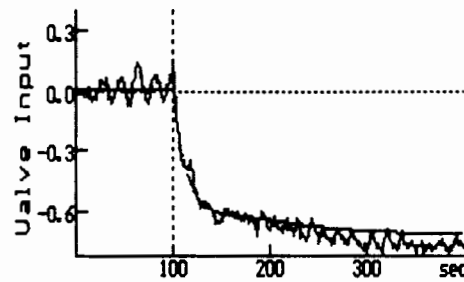


FIG. 6.8 Closed-loop response with 50% increase in speed

The correspondence obtained in this trial was exceptionally good. This result proves the success of state-feedback on a real plant and the achievement of the Kalman filter to predict the states correctly.

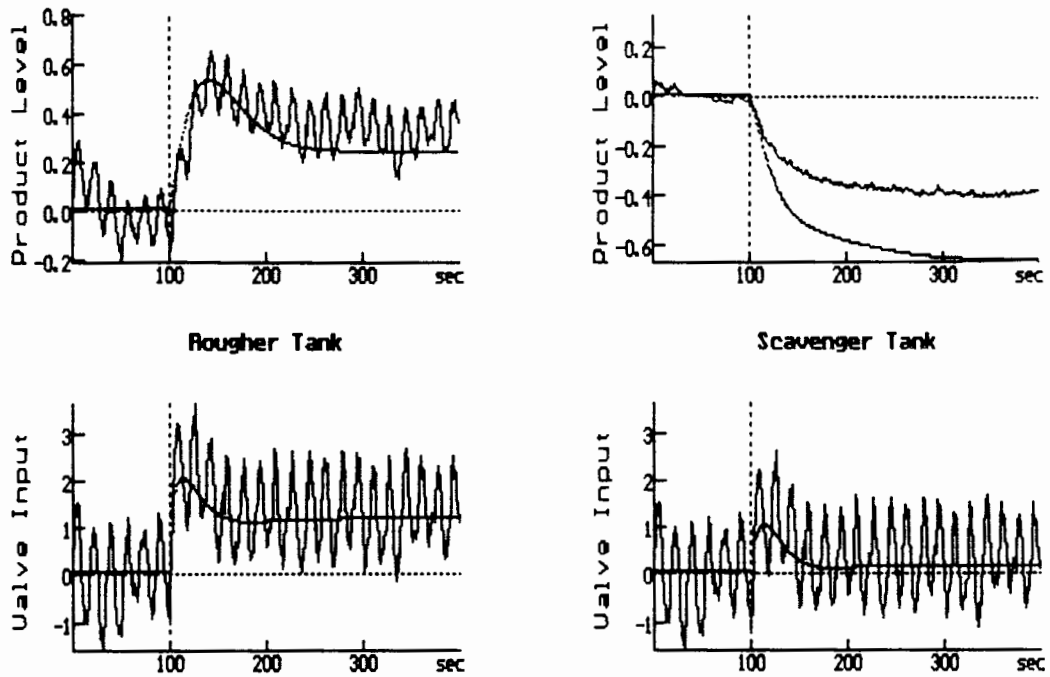
The behaviour of the Rougher tank level to a Scavenger input change exhibits a non-minimum phase response. This may be unsatisfactory for a setpoint tracking control scheme and different pole positions would have to be selected to remove this problem.

6.4.6.6 Step Test 4

The final step test with the intention to double the speed of response is shown in Fig. 6.9.

Actual / Simulated Closed-Loop Step Response

a) Rougher Step Size Normalised



Actual / Simulated Closed-Loop Step Response

b) Scavenger Step Size Normalised

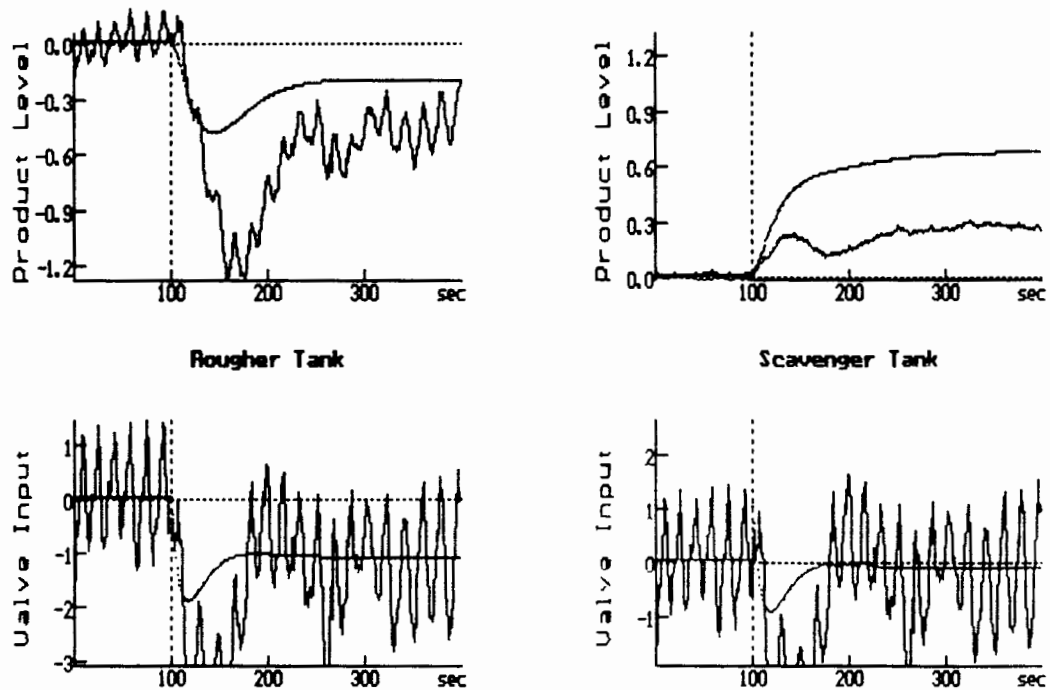


FIG. 6.9 Closed-loop response with 100% increase in speed

The experiment in Fig. 6.9a) shows that although the levels of both tanks were drifting in the first 50 seconds, this variation was successfully counteracted by the valve inputs before the step took place. The predicted transient response corresponds well to the actual, except for the Scavenger level. This can again be ascribed to the fact that the valve settings may have been in a low gain region, or that the plant had moved out of the operating region for which its model was determined.

Analysing the findings in Fig. 6.9 b) shows large deviations from the predicted results. This can be attributed to the fact that both valve inputs were saturated for about 50 seconds. The over-driven inputs affected the Scavenger level adversely. Whereas a response similar to first order was expected a complicated one of high order governed that tank. This shows that pole assignment can be unfavorably affected by extreme non-linearities.

It is interesting to observe that the responses here have reversed in sign compared to the other three step tests discussed previously. It is thus important to analyse the step response of a particular selection of poles when developing a setpoint tracking scheme for the system.

It is further noticeable that the Scavenger step results in the valve inputs behaving as if the Rougher had been stepped with a negative step. This gives rise to a situation where it will be difficult or even impossible to design a setpoint tracking controller for this system as the levels cannot be controlled independently. The system has in this case only one input effectively.

6.4.6.7 General Analysis

By analysing the last step test (Fig. 6.9), it is apparent that the system has indeed improved on its speed of response. The settling time for the transient response has halved compared to that of the first test (Fig. 6.6). Close inspection of the predicted Scavenger level response shows that it is not of first order anymore, but instead exhibits a pronounced bend justifying the increase in speed.

An examination of the amplitude of the sinusoid on the valve inputs for all four step tests, shows that the feedback gain varies from one set of poles to the other. The variation is large for a 10% and 100% improvement of speed. For the 20% and 50% improvement however the gain is small. This is again not a linear relationship, i.e. the gain does not increase as the poles are moved progressively further from the origin.

The diversity of transient responses, that were observed for various pole positions has been demonstrated by the results above and shows that the pole assignment technique must include a critical analysis of the closed-loop system transient response to step inputs before any setpoint tracking scheme can be employed.

The closed-loop step responses have also shown that the plant remained stable as no signs of instability could be found.

6.5 CONCLUSION

In this chapter an intuitive method for the design of Kalman filters has been developed and applied successfully.

CHAPTER 6 APPLICATION OF POLE ASSIGNMENT

It was also shown that pole assignment by state feedback could be achieved on a real plant. The sensitivity of state feedback to parameter changes or non-linearities have been demonstrated.

The various step responses of different sets of poles have again emphasised that the closed-loop system behaviour cannot be directly predicted from a choice of \mathbf{q} and a set of poles.

7. CONCLUSION

7.1 INTRODUCTION

The fact that both the Inverse Nyquist Array (INA) and pole assignment techniques could be applied successfully to the flotation rig has been demonstrated in previous chapters.

The discussion is concluded in this chapter with a direct comparison of the two methods and suggestions for future work.

7.2 MODEL DETERMINATION

The INA technique is applied in the frequency domain, requiring a transfer function representation of the plant.

In addition to using an existing state space description, a transfer matrix model of a multivariable plant can be obtained with relative ease from step response analysis as demonstrated in chapter two. It is further possible and usually adequate to minimise the order of the individual transfer functions to simplify the model.

The state space model needed to perform pole assignment can be established from the transfer matrix, which usually results in a system with a large number of states. This strains the numerical accuracy of any design technique and makes physical interpretations difficult.(10)

The alternative method to obtain a model in state space is by describing the plant in terms of differential equations.

This however can only be applied to multivariable systems of which the various elements are known scientifically allowing construction of these equations. A black-box type identification is thus not possible and it is further difficult to establish to what degree of accuracy these formulations must be performed.

7.3 CONTROL SYSTEM DESIGN CRITERIA

A discussion on desirable properties of control systems has been given by Layton (7). These and additional features are used to compare the two techniques.

7.3.1 STABILITY

The main criterion in system design is that of stability.

In pole assignment stability is theoretically guaranteed if the desired pole positions lie in the left half plane.(31) However, even if these lie in stable regions, it is found in practice that instability can occur for a number of reasons.

If the inputs to the plant saturate, the system may become unstable. Referring to Fig. 7.1, input saturation is equivalent to the feedback path being broken, as the plant inputs are not affected by further changes in the states. The stability of the resulting open-loop system depends on the open-loop stability of the plant. If the plant is open-loop unstable then saturation will cause instability.

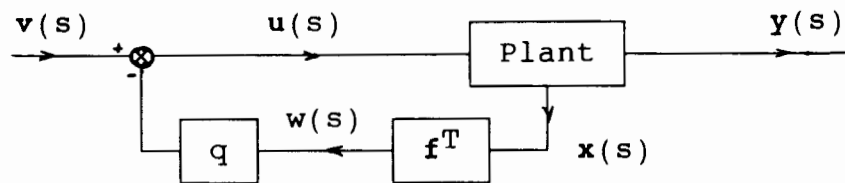


FIG. 7.1 Pole Assignment by State Feedback

In addition, if the states are not measurable directly from the plant and an estimator is used, the effects of saturation are more difficult to predict. Fig. 5.5 in chapter five shows an implementation of a Kalman filter, where the plant inputs are used to estimate the states. The Kalman filter may be unaware of saturation of the inputs and then estimate the states incorrectly, and may cause instability.

A similar situation can occur if the plant outputs saturate, as these are also used to estimate the states of the plant. If they saturate, they may distort the estimated states and result in unstable operation of the control system.

Changes in the open-loop gain caused by non-linear behaviour of the inputs or outputs can also adversely affect the control scheme employing pole assignment. To predetermine how changes in the gain will affect the closed-loop system is difficult. This was discussed in detail in chapter six, section 6.4.5.1.

The pole assignment technique gives no distinct indication of how these factors influence the stability and this omission limits its usefulness in practice.

In this respect the INA technique is much better, because not only does it determine stability by the application of

CHAPTER 7 CONCLUSION

the Nyquist criterion, but it also indicates a stability or gain margin with the aid of Gershgorin and Ostrowski circles. From these a stability region or gain space can be constructed [see Chapter 3, Section 3.4.4]. The knowledge of the maximum and minimum gains of the nonlinear inputs of a plant can thus be included in the design. Similarly, saturation, which is equivalent to the gain becoming zero, can be incorporated. And if these extremes lie within the gain space, stability is assured. This is not a stringent design criterion as the system may remain stable even though the gains lie outside this region.(2)

The problem of changes in the dynamics of a plant is always difficult to include in any design procedure. The only way to experiment with these parameter changes is to insert a number of different models of the plant in the final control scheme and analyse their effects.

7.3.2 INTEGRITY

The concept of system integrity is also related to stability. A good feature of control systems is to remain stable even if failures such as disruption of some or all the feedback paths occur. The INA technique allows investigation of such an event, which can be emulated by setting the corresponding elements of matrix F equal to zero and analysing the resulting gain space. The pole assignment technique does not have this feature although it is very sensitive to failure in the state feedback path. This can result in instability in a similar way as saturation of the plant inputs [Section 7.3.1].

7.3.3 INTERACTION

The main feature of the INA technique lies in its ability to reduce the interaction of system inputs and outputs. Graphical techniques can be used to 'measure' the amount of interaction. If the method can be successfully applied then individual inputs of the closed-loop system control individual outputs. The multivariable system can then be approximated by a number of single-input, single-output processes, simplifying the controller design considerably.

The amount of interaction that results by applying pole assignment is difficult to predict and can only be established by simulation.

7.3.4 NOISE IMMUNITY

Another important feature of system design is noise immunity.

The INA method allows single-loop PI controllers to be designed for the dominant system, which can be used to limit the noise sensitivity of the system. The sensitivity can be established from the INA diagrams.

The pole assignment techniques does not have this feature. As noted in chapter six, no relationship exists between pole location and resulting noise sensitivity. It is extremely difficult to predict the system behaviour to noise even by simulation. It can only be established by applying the control scheme to the plant directly and observing the noise on the plant inputs.

7.3.5 TRACKING BEHAVIOUR

The INA technique allows single-loop PI controllers to be designed for the dominant system to limit the amount of overshoot, speed and error in setpoint tracking.

As the pole assignment method does not result in a dominant or non-interaction system, it is difficult to design single-loop PI controllers for it. It does however allow the designer to change the dynamic behaviour of the plant. If the system response is oscillatory, a damped response can be achieved by moving the poles to better positions. The speed of response can also be improved by moving the poles as demonstrated in chapter six.

7.3.6 CONTROLLER STRUCTURE

The structure of the controller resulting from the INA technique depends on the complexity of the plant model. For small system with two inputs and two outputs, a constant pre-compensator is usually sufficient to ensure dominance.(2) As the order of the individual elements of $G(s)$ and the number of inputs and outputs increases dynamic controllers become necessary. Standard PI controllers can be inserted to complete the control scheme as shown in chapter four.

The pole assignment technique employs constant gain state feedback which is simple to implement if the states can be measured directly from the plant. If however a state estimator is required the structure of the control system becomes more intricate [Chapter 6].

In both cases thus, the controller structure is relatively complicated.

7.3.7 DESIGN TRADE-OFFS

To design a control system that contains all the above features is usually not possible and compromise is essential. By increasing the controller gain for example, the speed may be improved but the noise sensitivity will also increase. It is thus at the discretion of the designer to decide which features are more important.

A good design technique should allow the designer to compromise between different requirements. It should thus be possible to predict system behaviour with respect to the above features.

In this respect, the INA technique contains most information on the closed-loop system behaviour. The amount of interaction, noise sensitivity, stability with gain margins and integrity of the closed-loop system are contained in the INA diagrams and by application of the Gershgorin and Ostrowski circles. These factors were used to derive a control scheme for the flotation rig in chapter four.

The pole assignment method gives little insight into the problem as most of the features of the resulting closed-loop system are not fully predictable. No quantitative indications can be obtained of characteristics such as interaction, noise sensitivity, integrity, gain margins and stability during the design process. These can only be established by simulation or on the plant itself. Furthermore, no clear strategy exists on how to improve or design around individual requirements.

The failure of the pole assignment technique in this respect is related to the state space description of control system. It is easy to obtain the dynamic behaviour of a system from

CHAPTER 7 CONCLUSION

its state space model, but to recover further information is difficult.

7.4 FUTURE WORK

7.4.1 CONTROL OF FULL FLOTATION RIG

Although only a subsystem of the flotation rig was used as a practical example for this discussion, the full model was developed in chapter two which can be used to design a control system for the rig. A project of this nature would generate considerable interest especially for the mineral extraction industry.

The suitability of the Inverse Nyquist Array technique for this purpose has been well demonstrated during the course of this dissertation. Industrial flotation rigs do however consist of a large number of circuits, which complicates the design process. Large systems have recently become an area of interest and the INA technique can be extended towards these with the concept of block-dominance(34).

7.4.2 A GRAPHICAL TECHNIQUE FOR POLE ASSIGNMENT

The success of pole assignment by state feedback has been demonstrated, but difficulties arise from the resulting closed-loop zero positions. A graphical technique that plots the closed-loop zero positions as the direction of the q vector is varied, while the closed-loop poles remain fixed, could ease the design process.

A similar technique could be used to show the movement in pole positions of the closed-loop system as the open-loop

CHAPTER 7 CONCLUSION

gain is varied. This would give an indication of the system response to nonlinear changes in the behaviour of the plant.

The flotation rig did not necessitate the application of pole assignment as the pole positions of the model were, except for their slowness, acceptable. A system with oscillatory or even unstable behaviour would be more suitable. Such a system must however not be too large, i.e. contain more states than ± 10 , which diminishes the computational accuracy of the technique.

Further research could be done to use state feedback to decouple a plant(21). This technique however limits the number of assignable poles, which in the case of the flotation rig could be acceptable, if the resulting system has limited interaction.

CHAPTER 7 CONCLUSION

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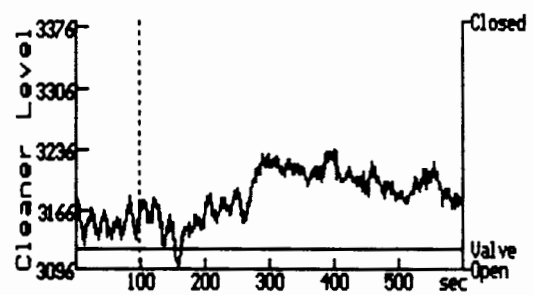
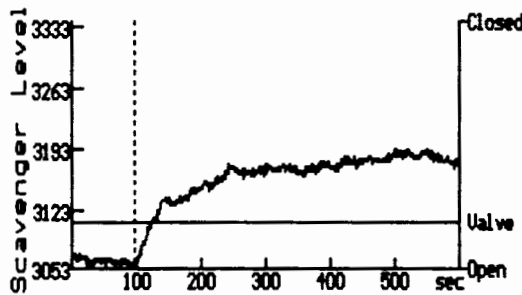
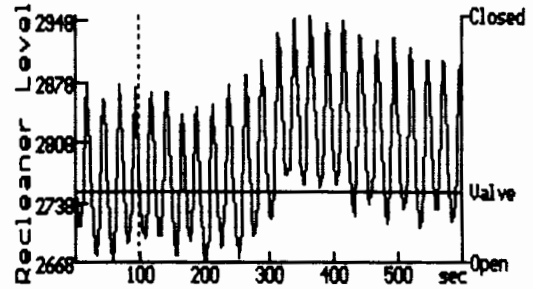
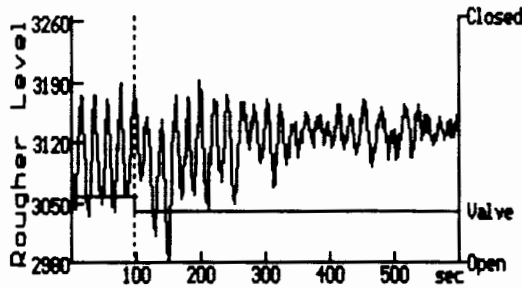
APPENDIX A OPEN-LOOP STEP RESPONSES

A) OPEN-LOOP STEP RESPONSES

APPENDIX A OPEN-LOOP STEP RESPONSES

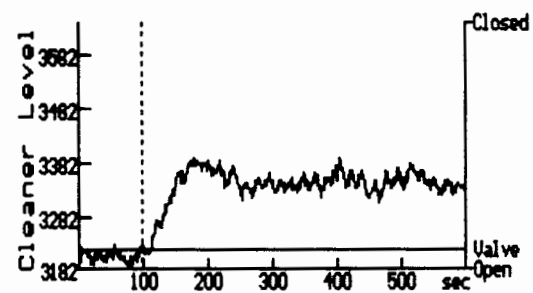
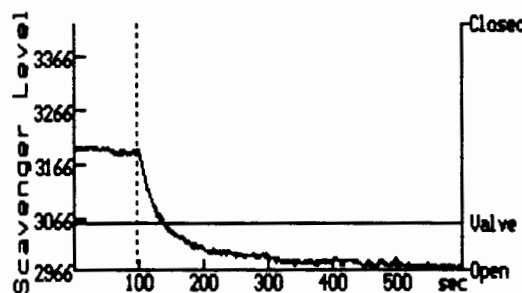
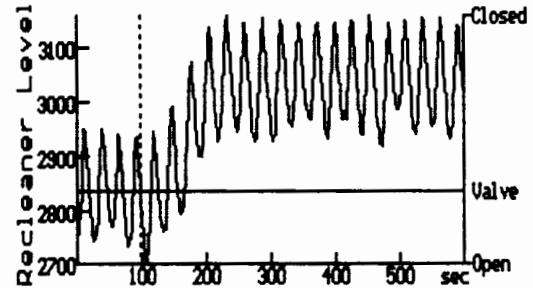
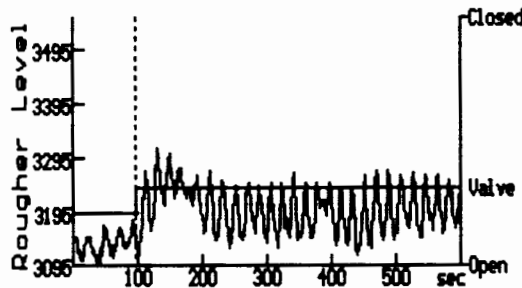
Flotation System Open-Loop Step Response

Test 1a) Rougher Step Size= -216 Units (-4%)



Flotation System Open-Loop Step Response

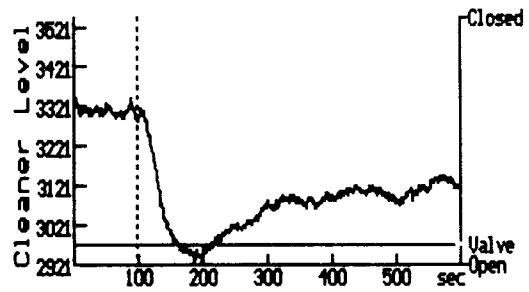
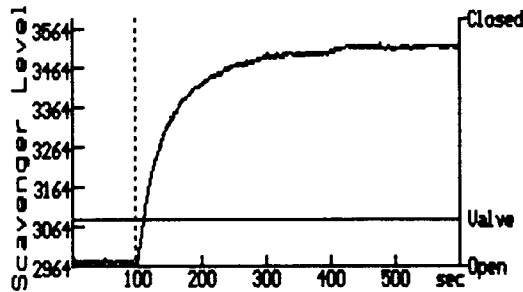
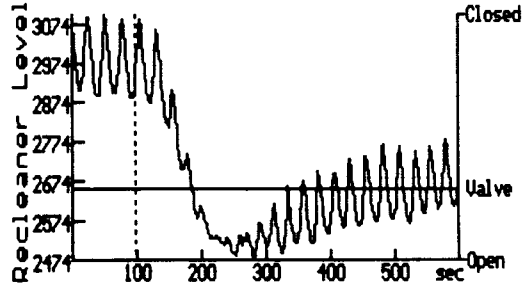
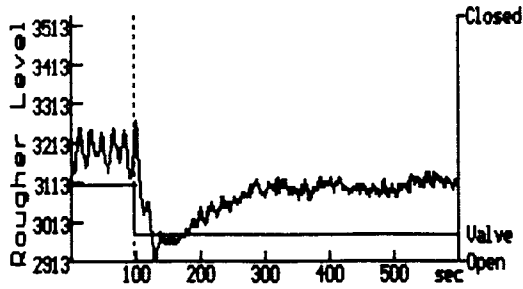
Test 1b) Rougher Step Size= 410 Units (10%)



APPENDIX A OPEN-LOOP STEP RESPONSES

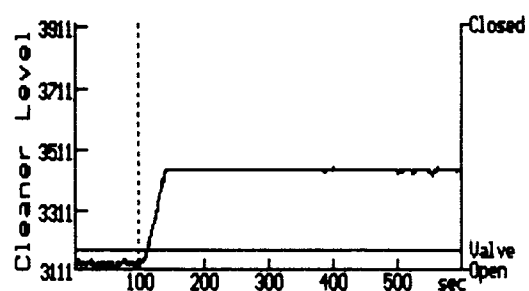
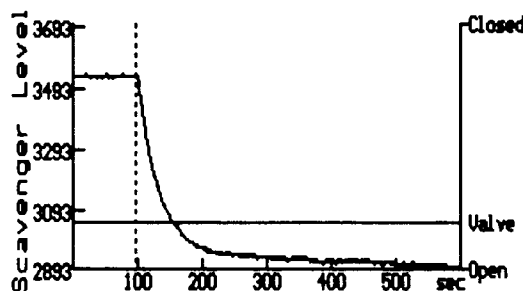
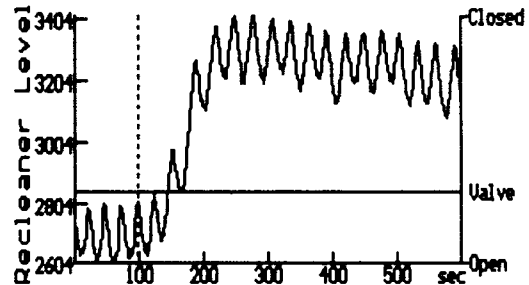
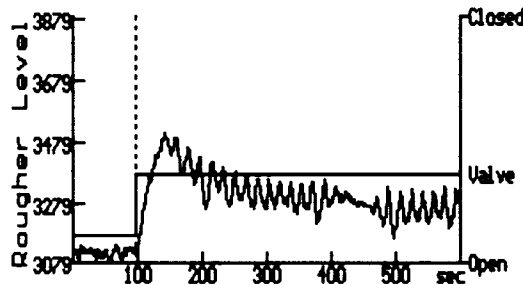
Flotation System Open-Loop Step Response

Test 1c) Rougher Step Size= -19 Units (-19%)



Flotation System Open-Loop Step Response

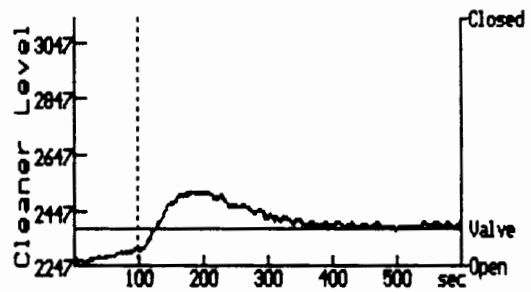
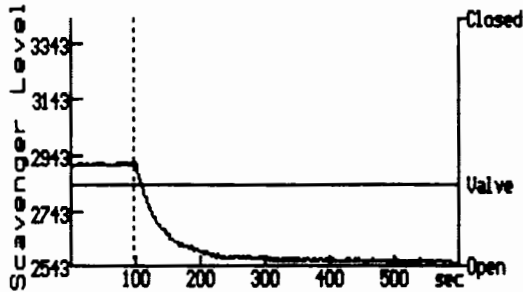
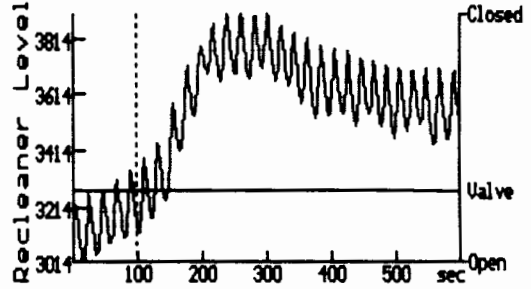
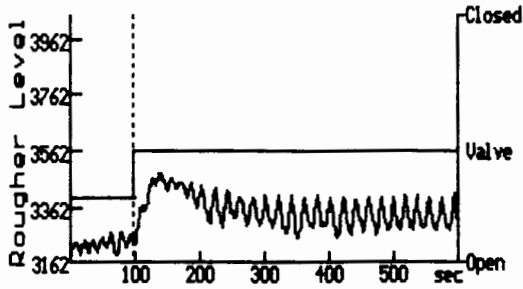
Test 1d) Rougher Step Size= 1024 Units (25%)



APPENDIX A OPEN-LOOP STEP RESPONSES

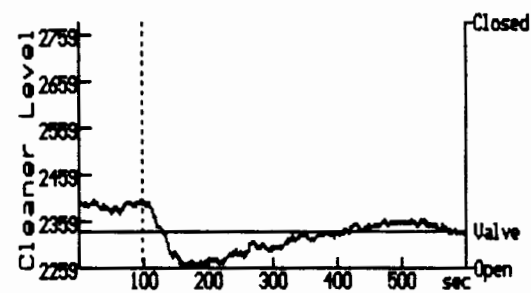
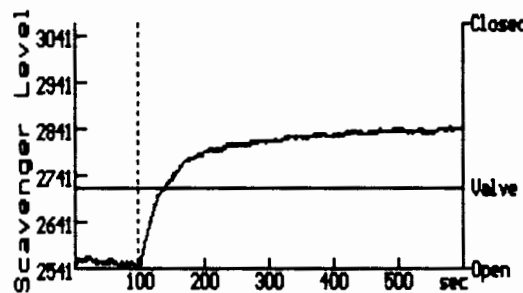
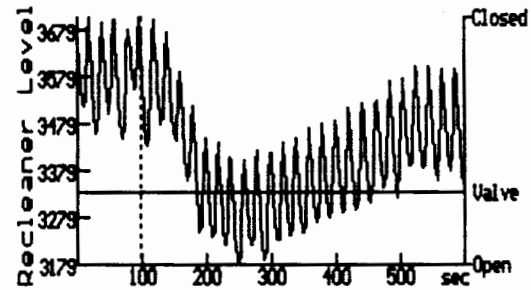
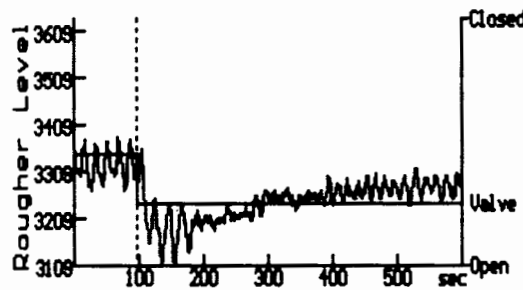
Flotation System Open-Loop Step Response

Test 1e) Rougher Step Size= 807 Units (20%)



Flotation System Open-Loop Step Response

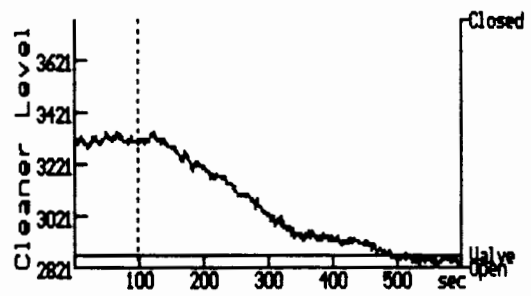
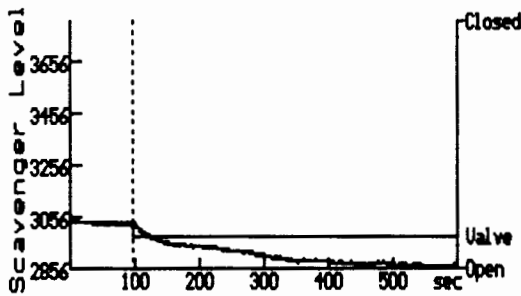
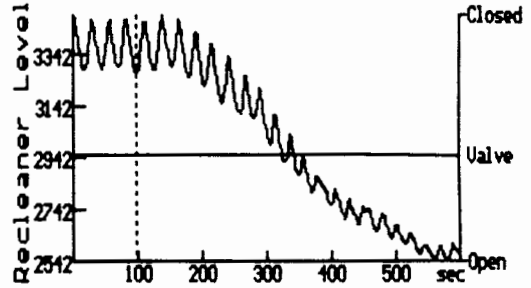
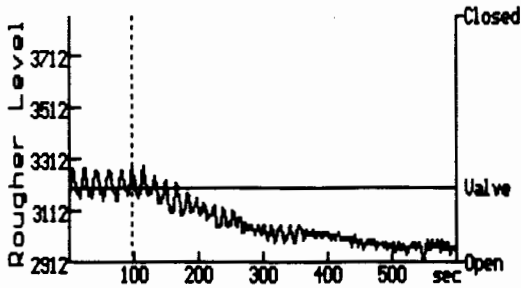
Test 1f) Rougher Step Size= -819 Units (-19%)



APPENDIX A OPEN-LOOP STEP RESPONSES

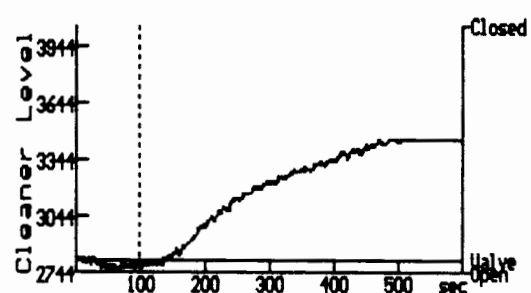
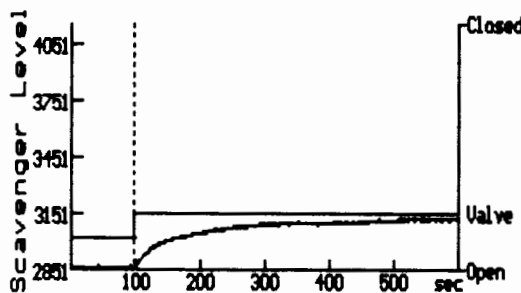
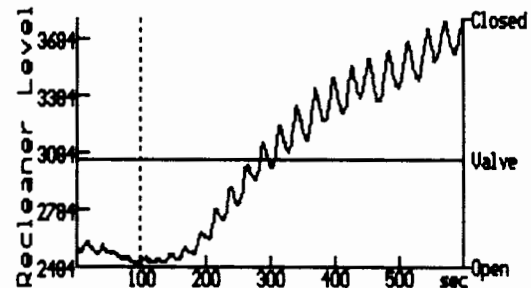
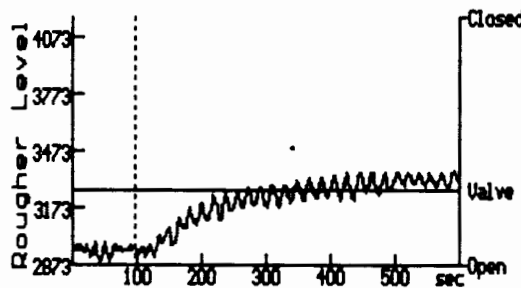
Flotation System Open-Loop Step Response

Test 2a) Scavenger Step Size= -224 Units (-4%)



Flotation System Open-Loop Step Response

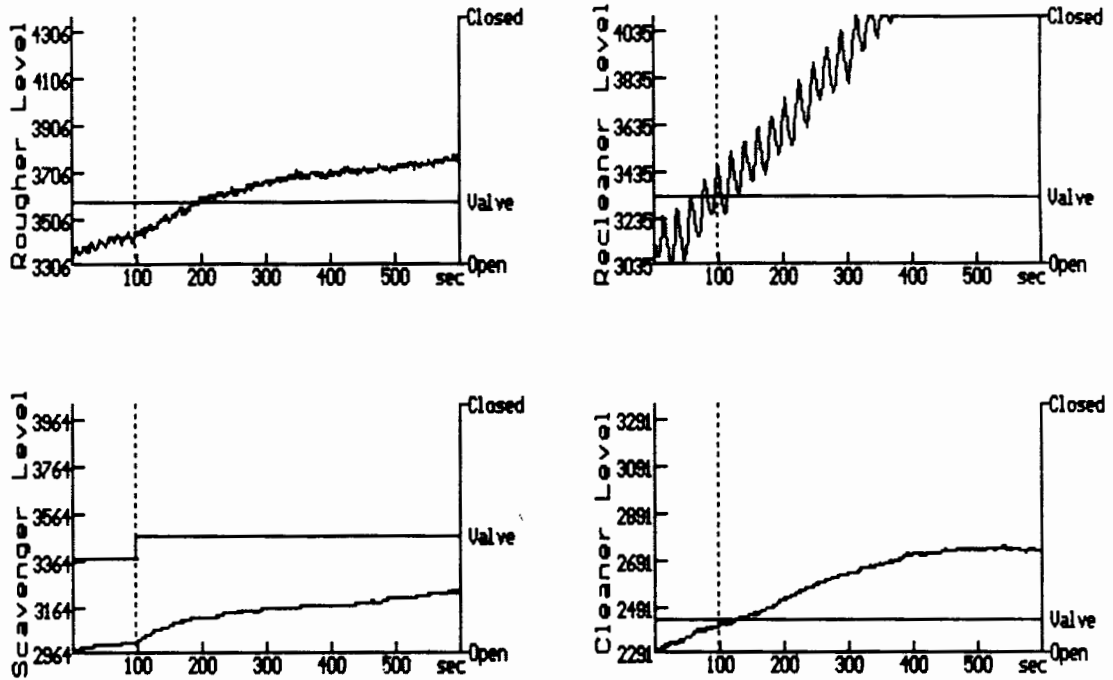
Test 2b) Scavenger Step Size= 409 Units (10%)



APPENDIX A OPEN-LOOP STEP RESPONSES

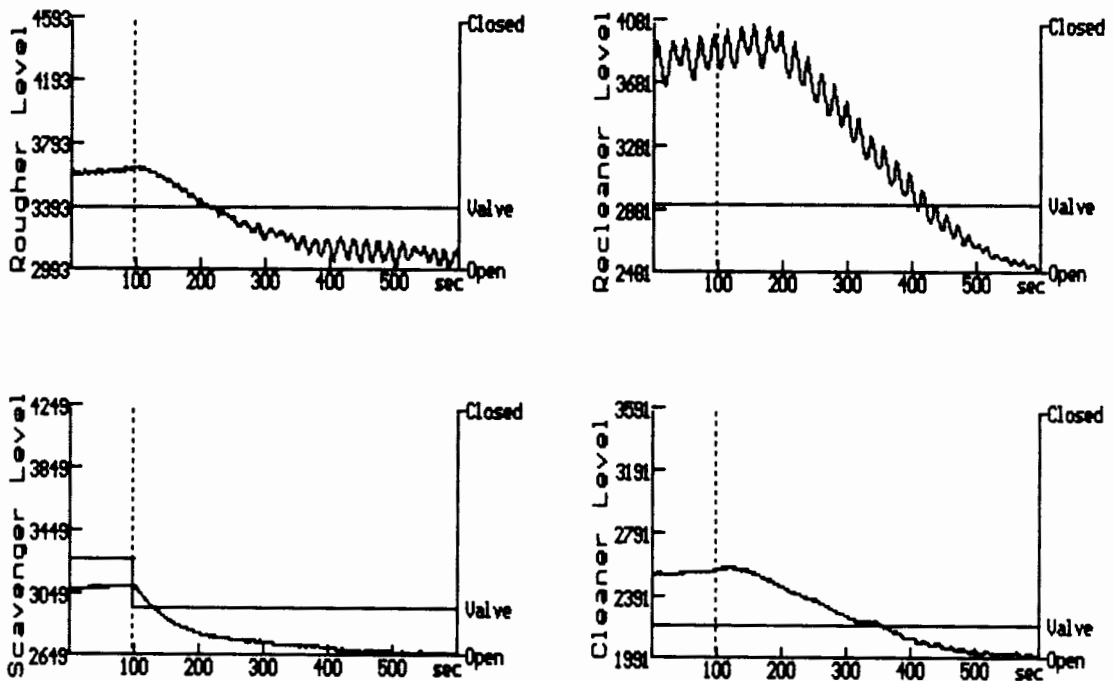
Flotation System Open-Loop Step Response

Test 2c) Scavenger Step Size= 408 Units (10%)



Flotation System Open-Loop Step Response

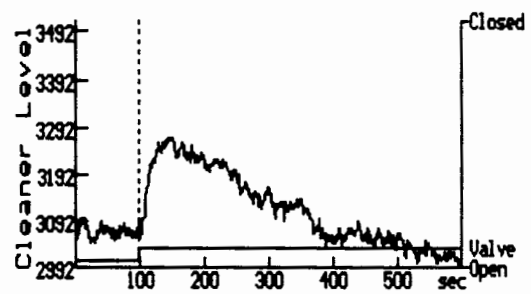
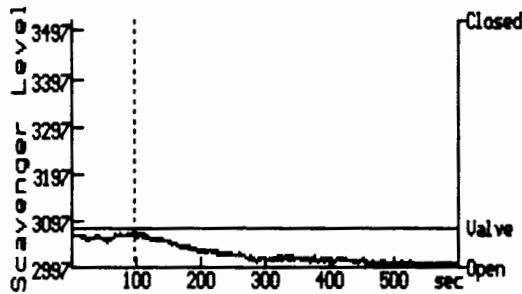
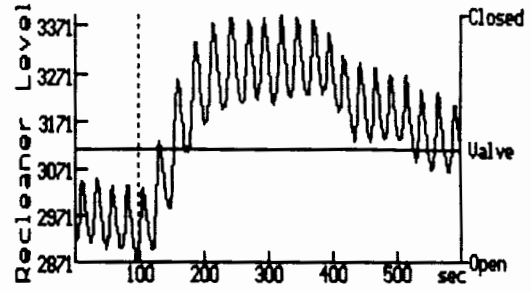
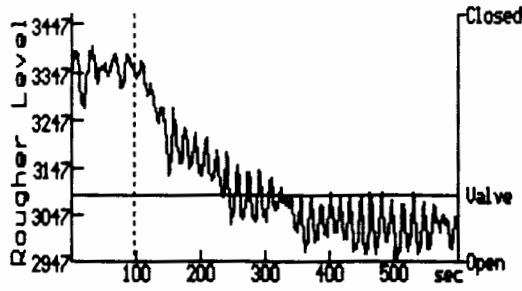
Test 2d) Scavenger Step Size= -814 Units (-19%)



APPENDIX A OPEN-LOOP STEP RESPONSES

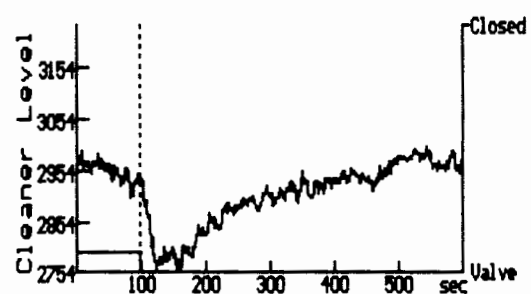
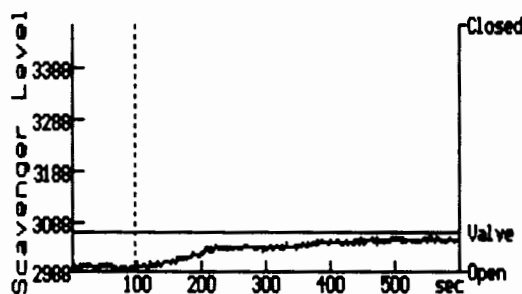
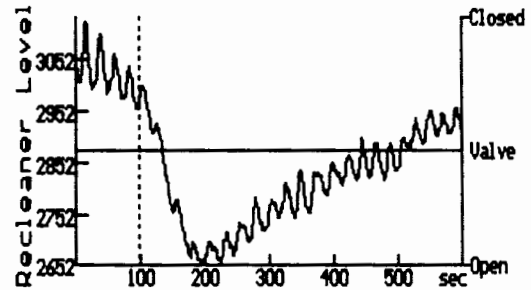
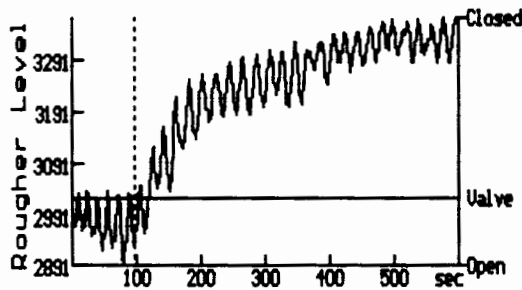
Flotation System Open-Loop Step Response

Test 3a) Cleaner Step Size= 218 Units (5%)



Flotation System Open-Loop Step Response

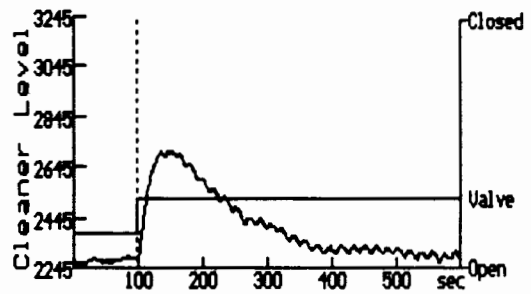
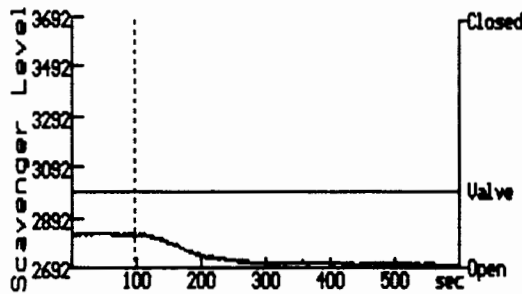
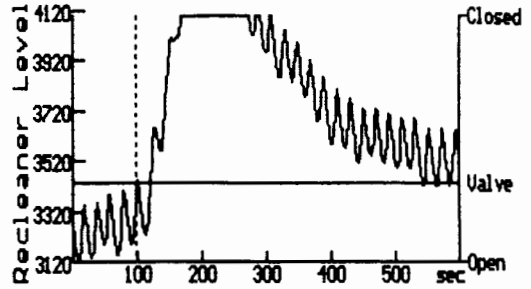
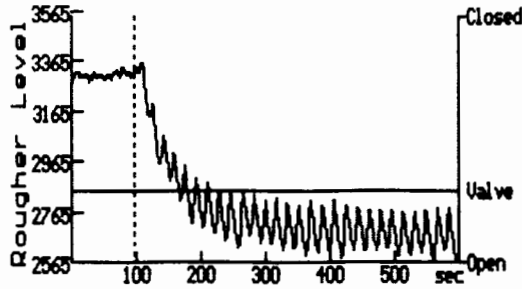
Test 3b) Cleaner Step Size= -368 Units (-8%)



APPENDIX A OPEN-LOOP STEP RESPONSES

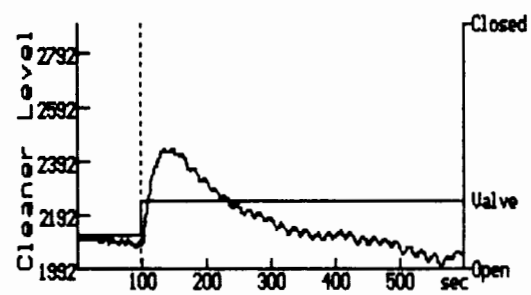
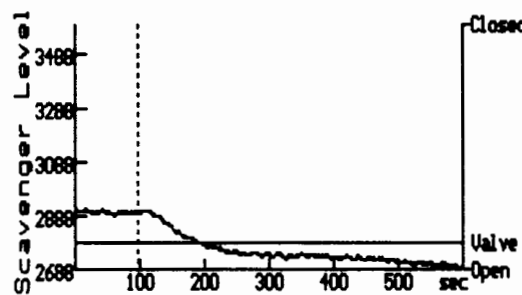
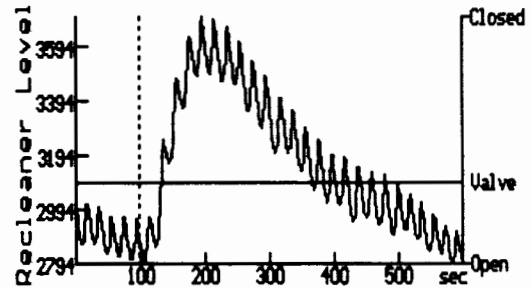
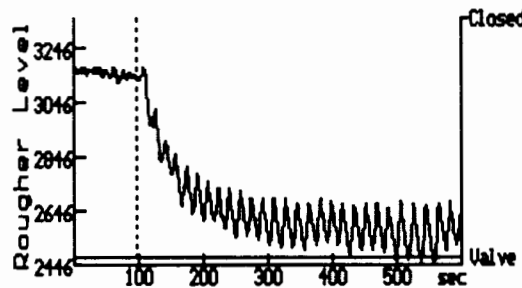
Flotation System Open-Loop Step Response

Test 3c) Cleaner Step Size= 611 Units (15%)



Flotation System Open-Loop Step Response

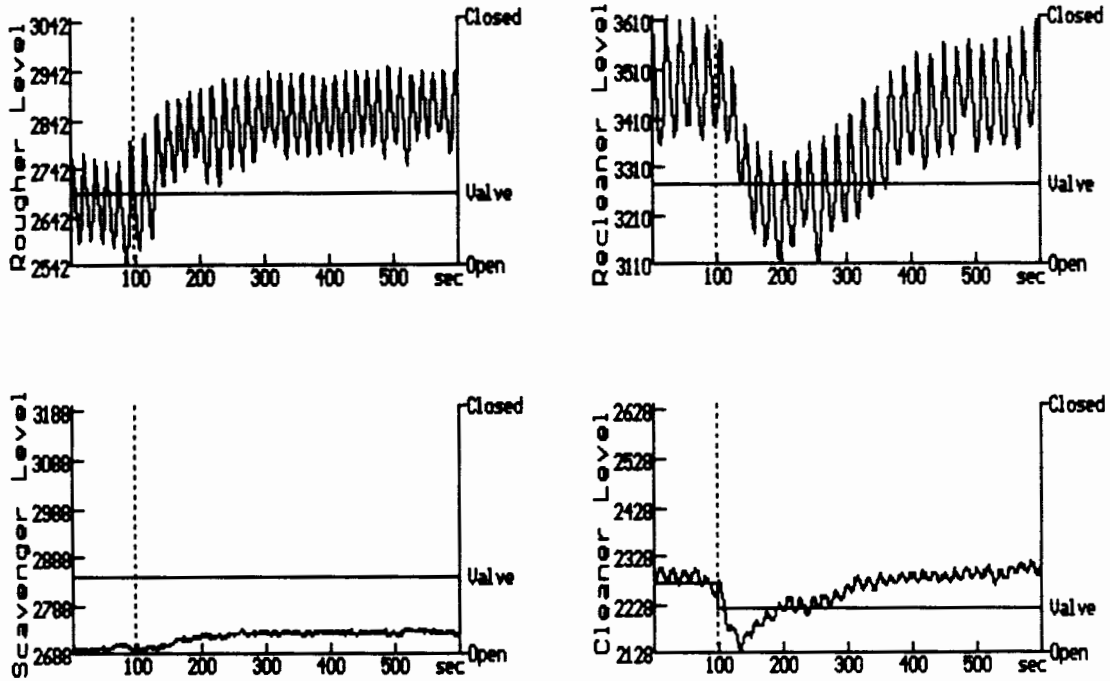
Test 3d) Cleaner Step Size= 604 Units (15%)



APPENDIX A OPEN-LOOP STEP RESPONSES

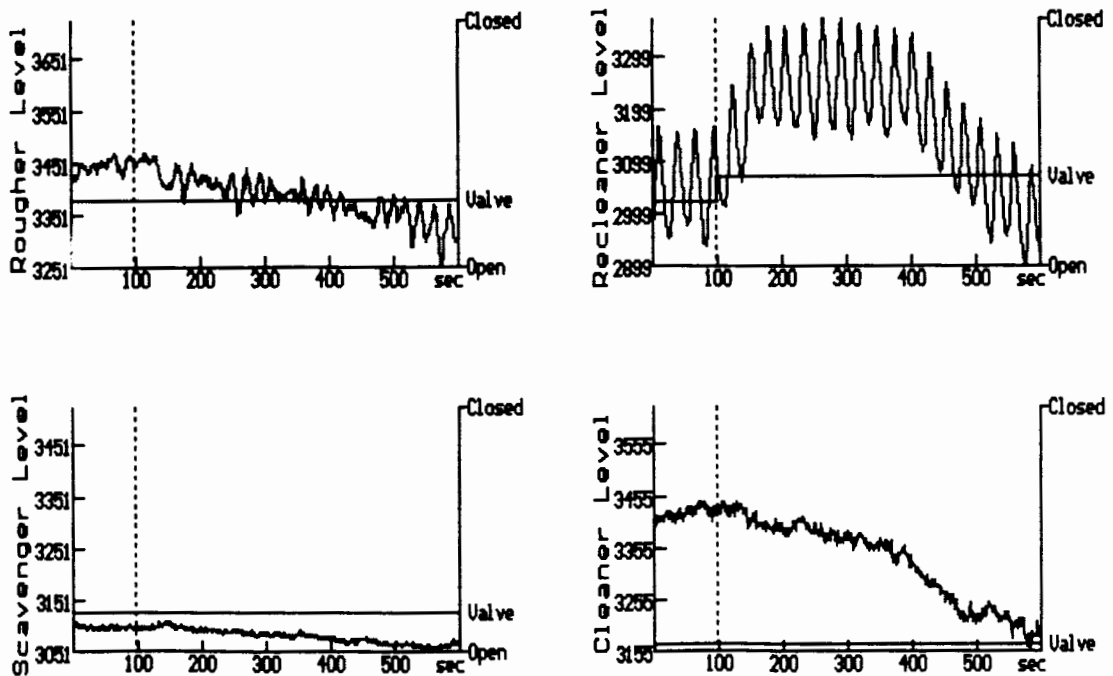
Flotation System Open-Loop Step Response

Test 3e) Cleaner Step Size= -409 Units (-9%)



Flotation System Open-Loop Step Response

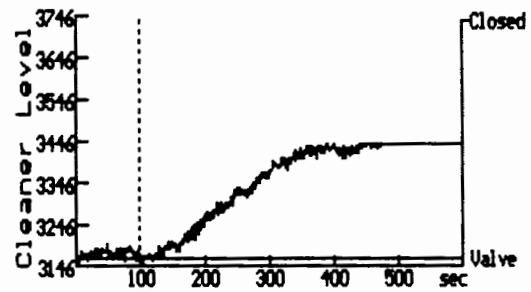
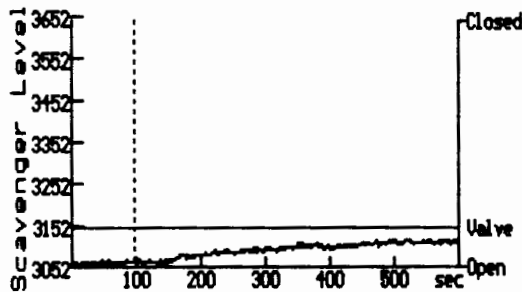
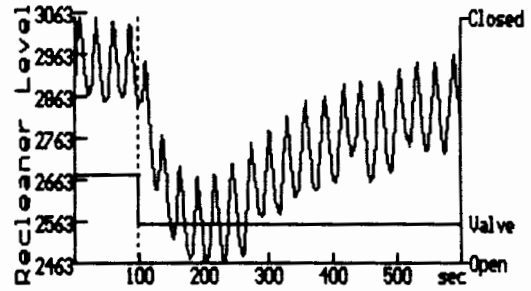
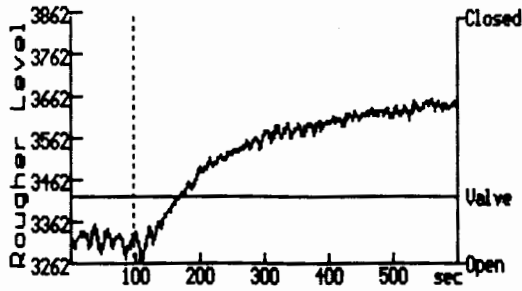
Test 4a) Recleaner Step Size= 416 Units (10%)



APPENDIX A OPEN-LOOP STEP RESPONSES

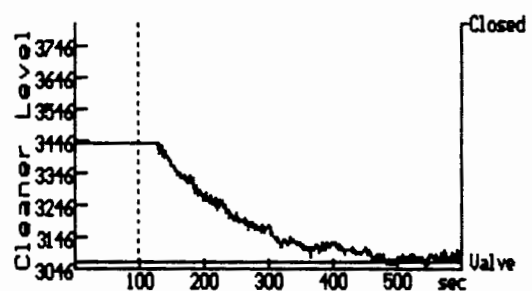
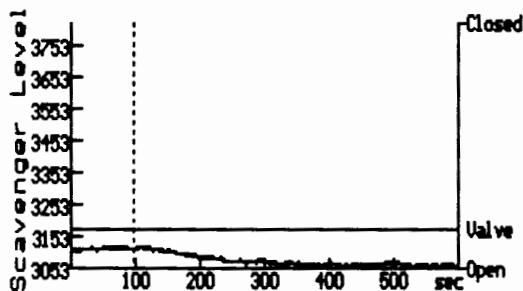
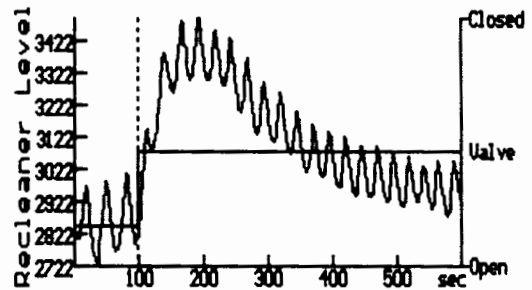
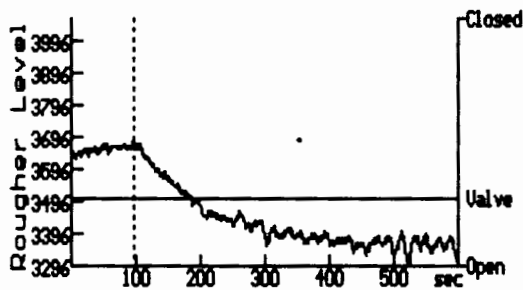
Flotation System Open-Loop Step Response

Test 4b) Recleaner Step Size= -819 Units (-19%)



Flotation System Open-Loop Step Response

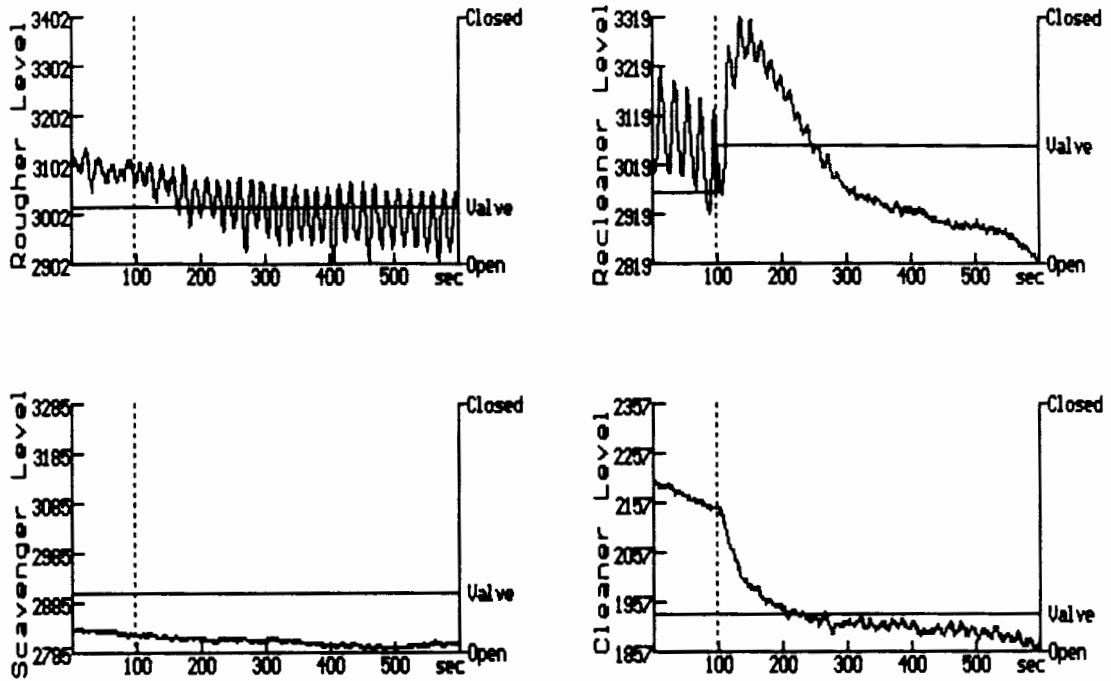
Test 4c) Recleaner Step Size= 1228 Units (30%)



APPENDIX A OPEN-LOOP STEP RESPONSES

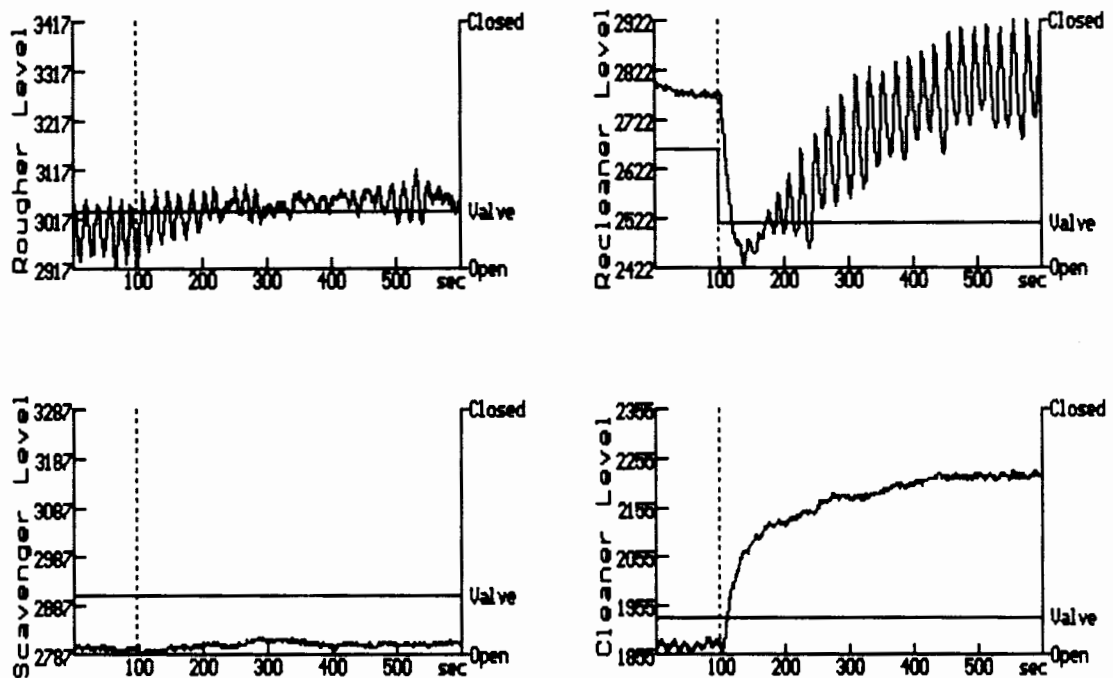
Flotation System Open-Loop Step Response

Test 4d) Recleaner Step Size= 812 Units (20%)



Flotation System Open-Loop Step Response

Test 4e) Recleaner Step Size= -1228 Units (-29%)

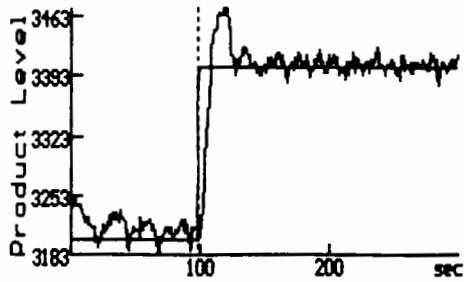


B) CLOSED-LOOP STEP RESPONSE (INA TECHNIQUE)

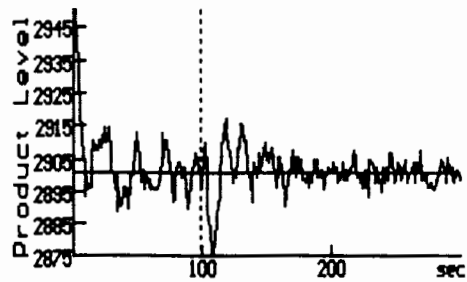
APPENDIX B CLOSED-LOOP STEP RESPONSES (INA TECHNIQUE)

Closed-Loop Step Response

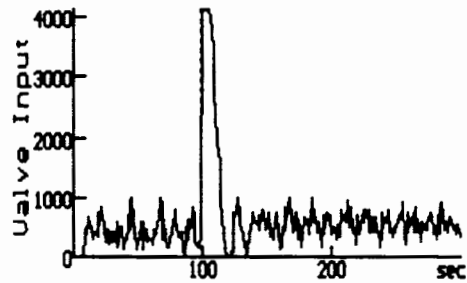
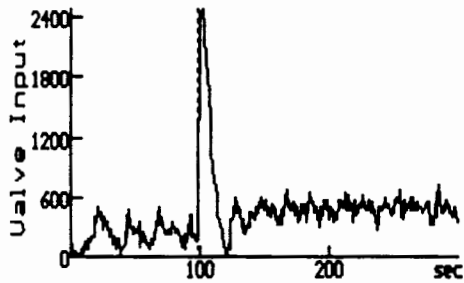
Rougher Step Size= 200 Units



Rougher Tank

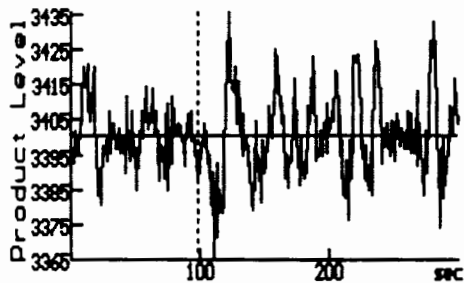


Scavenger Tank

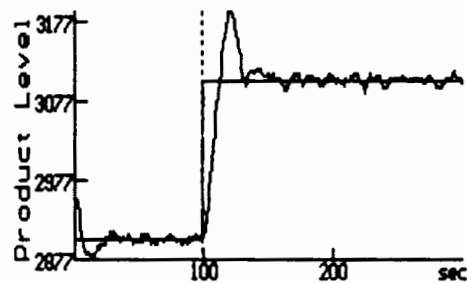


Closed-Loop Step Response

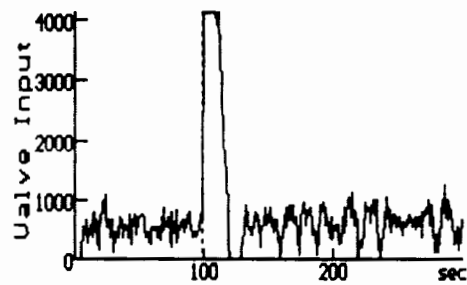
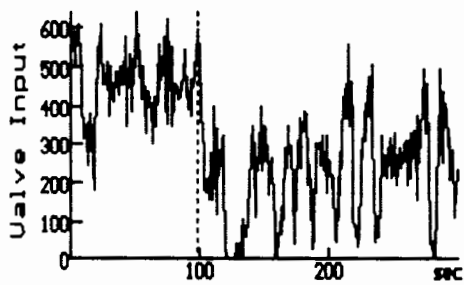
Scavenger Step Size= 200 Units



Rougher Tank



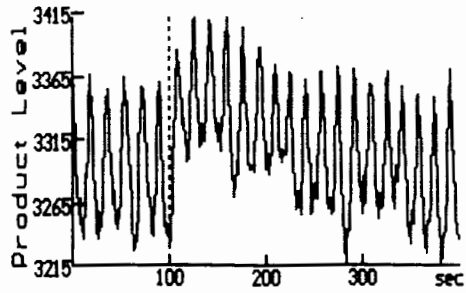
Scavenger Tank



C) CLOSED-LOOP STEP RESPONSE (POLE ASSIGNMENT)

Flotation System Closed-Loop Step Response

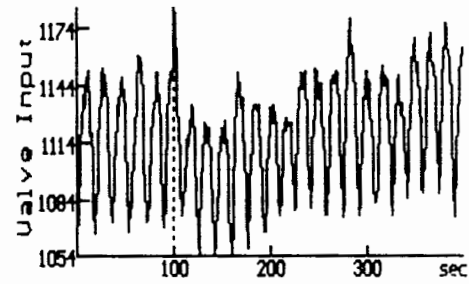
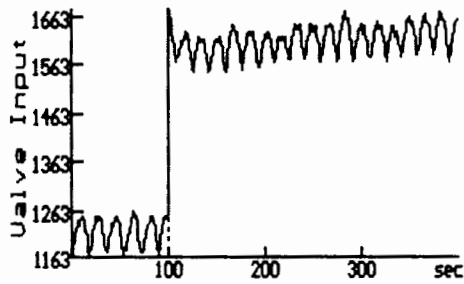
Rougher Step Size= 410 Units (10%)



Rougher Tank

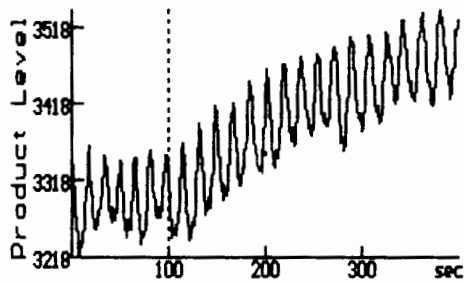


Scavenger Tank

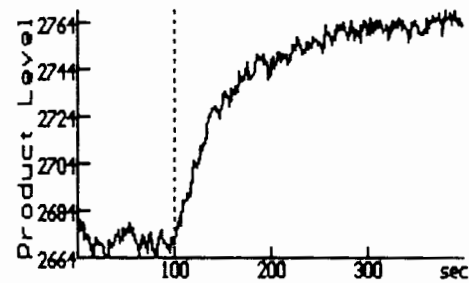


Flotation System Closed-Loop Step Response

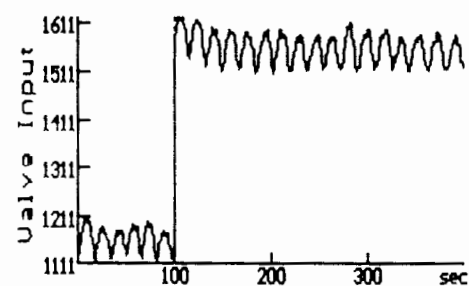
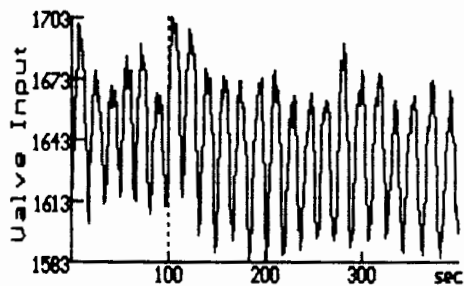
Scavenger Step Size= 410 Units (10%)



Rougher Tank

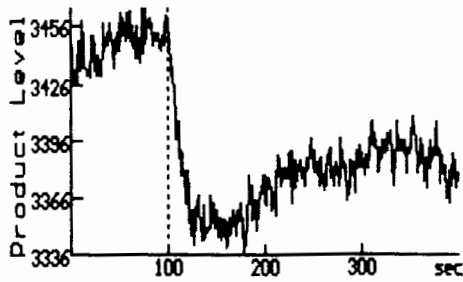


Scavenger Tank

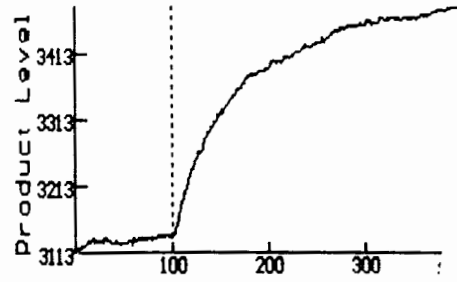


Flotation System Closed-Loop Step Response

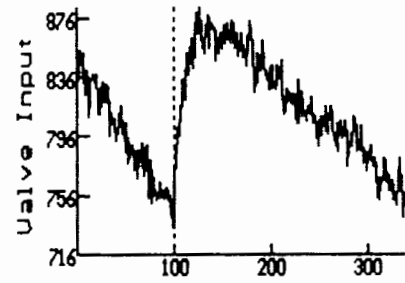
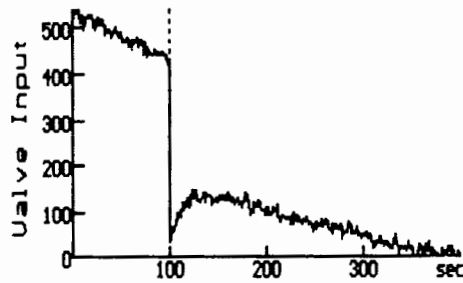
Rougher Step Size= -410 Units (-9%)



Rougher Tank

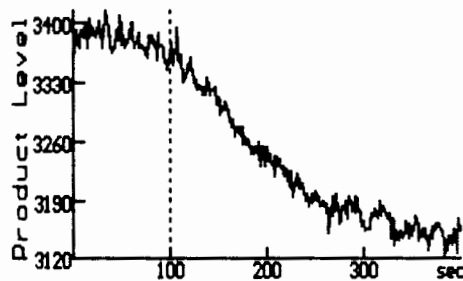


Scavenger Tank

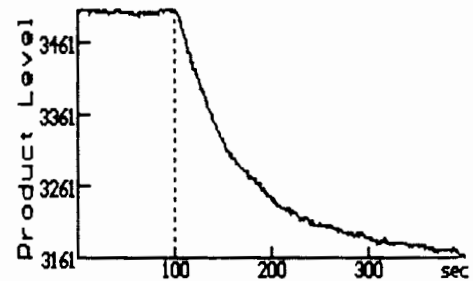


Flotation System Closed-Loop Step Response

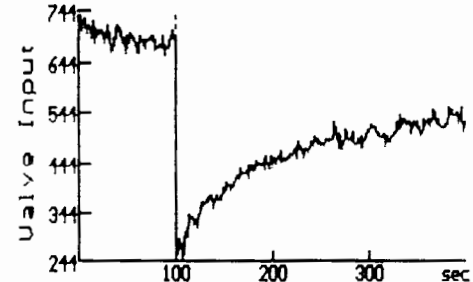
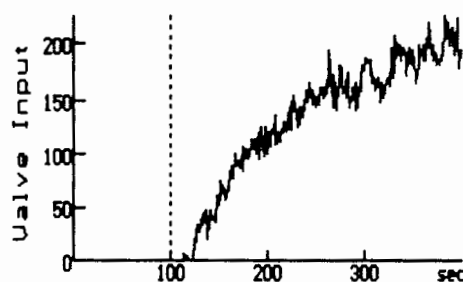
Scavenger Step Size= -410 Units (-9%)



Rougher Tank

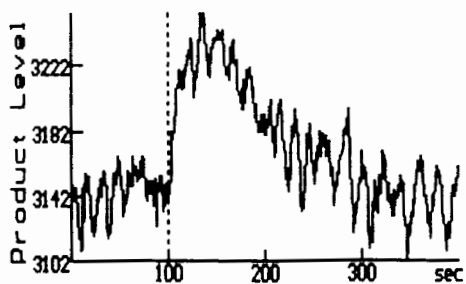


Scavenger Tank

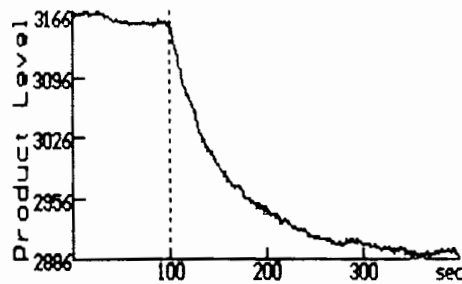


Flotation System Closed-Loop Step Response

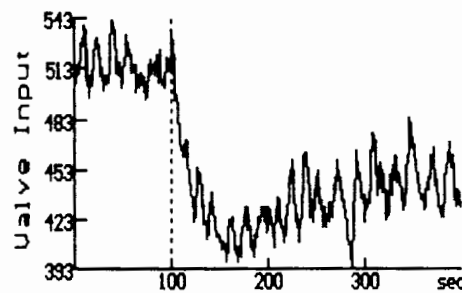
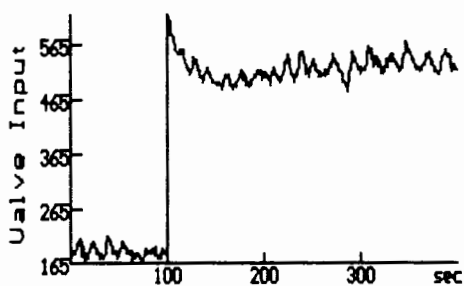
Rougher Step Size= 410 Units (10%)



Rougher Tank

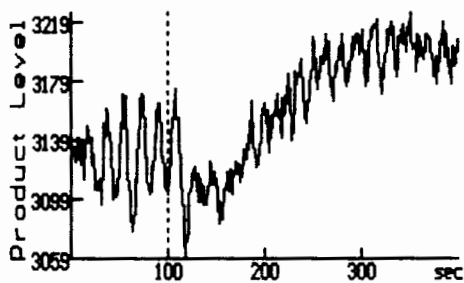


Scavenger Tank

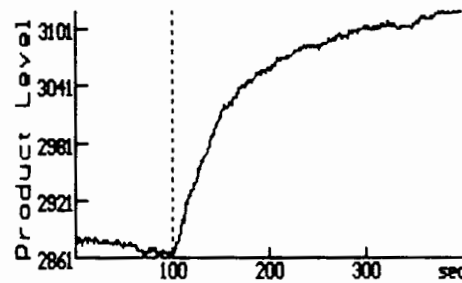


Flotation System Closed-Loop Step Response

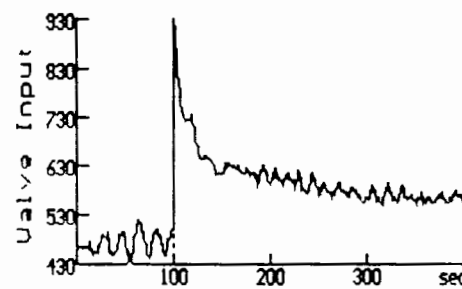
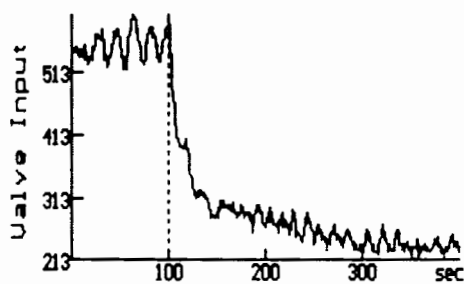
Scavenger Step Size= 410 Units (10%)



Rougher Tank



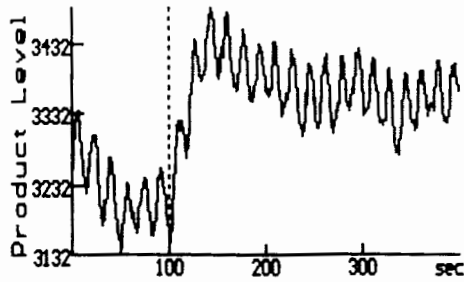
Scavenger Tank



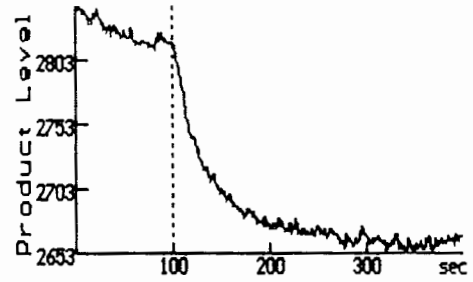
APPENDIX C CLOSED-LOOP STEP RESPONSES (POLE ASSIGNMENT)

Flotation System Closed-Loop Step Response

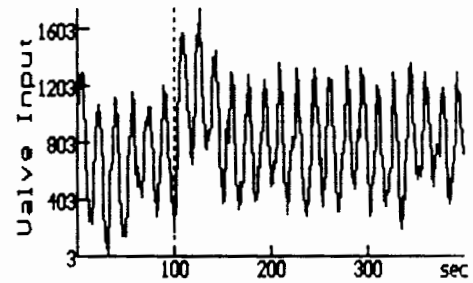
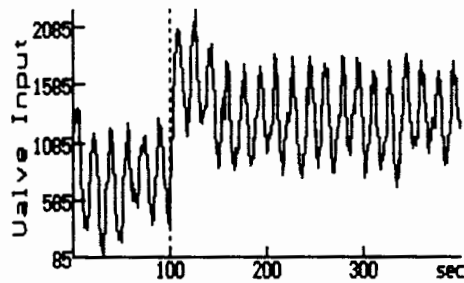
Rougher Step Size= 410 Units (10%)



Rougher Tank

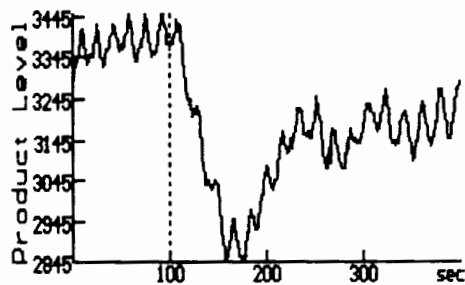


Scavenger Tank

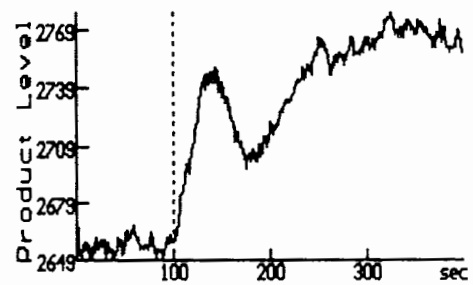


Flotation System Closed-Loop Step Response

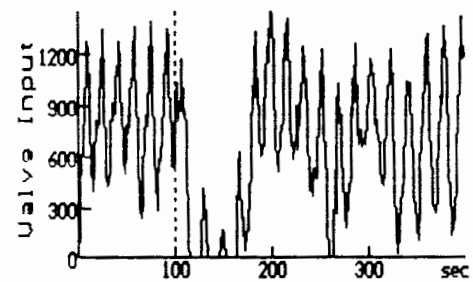
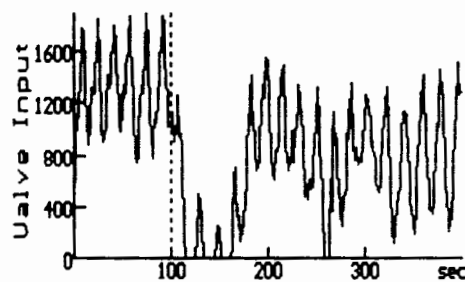
Scavenger Step Size= 410 Units (10%)



Rougher Tank



Scavenger Tank



APPENDIX C CLOSED-LOOP STEP RESPONSES (POLE ASSIGNMENT)

APPENDIX D SOFTWARE REFERENCE

D) SOFTWARE REFERENCE

1. INACAD PROGRAM SOURCE LISTING

1.1 SUBROUTINE OVERVIEW

addelm	Add two functions in s
addpoly	Add two polynomials in s
calc2wf	Calculate frequency points
calcf	Calculate frequency points
calcpw	Calculate polynomial for given s
calcqi	Calculate Q(s) for s=jw
calctf	Calculate frequency reponse of function
calcwf	Calculate frequency points
clrbot	Clear bottom line of display
clrdsn	Clear all design parameters
clrdsp	Clear status line
clreol	Clear to end of line
clrtop	Clear second status line
cls	Clear text screen
cominv	Invert matrix
comm2	Display command menu
commnd	Display command menu
dcirc	Draw circle
deltmp	Delete temporary files
diagon	Diagonalisation menu
dimtf	Find dimension of transfer function
disk	Construct filenames
docol	Perform column operation
dorow	Perform row operation
dos	Enter DOS
drawc	Plot complex point
dsnrst	Initialise design parameters
editmlt	Edit multiplier
edittf	Edit transfer function
editwf	Edit frequency data file
erasel	Clear line of display
error	Error routine
frange	Select frequency range
getchc	Get character from keyboard
getname	Get filename
getord	Get process order
getqu2	Calculate multiplier for row/col multiply
getquot	Calculate multiplier for row/col operation
getscale	Get graph scale from operator
gotorc	Move cursor
help	Display help file
inacad	Main program
inadsn	INA design routine

APPENDIX D SOFTWARE REFERENCE

inputtf	Input transfer function coefficients
invers	Display characters in inverse
kxcol	Multiply column by function
kxrow	Multiply row by function
lnwf	Natural logarithmic frequency table
loadrc	Get old cursor position
loadtf	Load transfer function from disk
loadwf	Load frequency table from disk
logwf	Logarithmic frequency table
mark	Draw cross at given point
matmlt	Multiply two matrices
mcircle	Draw M=1.3 circle
mltcol	Multiply column by function
mltrow	Multiply row by function
mnurst	Initialise menus
multpoly	Multiply two polynomials
nelm	Optimisation routine
normal	Print characters white on black
nyqstp	Nyquist diagram options
optim	Optimisation routine
pltax2	Plot axis
pltaxs	Plot axis
pltger	Plot Gershgorin circles
plthe2	Plot heading
plthed	Plot heading
pltina	Plot INA diagram
pltmlt	Plot multiplier
pltpts	Plot frequency points
polyxe	Expand e^x to series expansion
prcpar	Display design parameters
printtf	Print transfer function
prtml2	Print multiplier
prtmlt	Print multiplier
prtnyq	Print frequency reponse
prtplt	Print multiplier points
rcmlt	Perform row/column multiplication
readln	Read input
redokl	Perform operation
redowf	Recalculate frequency points
rowope	Do row operation
saverc	Save cursor position
savetf	Save transfer function to disk
savewf	Save frequency table to disk
setmde	Set text mode
setpfd	Select parameter file directory
shwpar	Show parameter selections
specwf	Calculate special frequency table
swop	Swop rows or columns
swopcol	Swop columns
swoprow	Swop rows
syscal	Perform DOS system call

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undoch Undo change
wait Display wait message

1.2 SUBROUTINE INDEX

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1.3 INCLUDE FILE LISTING

file ADD.BLK - Debug option

```
$DEBUG or $NODEBUG
```

file DESDTA.BLK - Global temporary storage

```
integer noofw
logical ksaved,lsaved
real w(200)
real gnum(1000),gden(1000),glag(100)
real knum(1000),kden(1000),klag(100)
real lnum(1000),lden(1000),llag(100)
real fnum(1000),fden(1000),flag(100)
common /desdta/
+ w,noofw,gnum,gden,glag,knum,kden,klag,
+ lnum,lden,llag,fnum,fden,flag,
+ ksaved,lsaved
```

file DESIGN.BLK - Design parameters

```
integer order,mxsord,si,sj,gerint,ostint
logical qexist,qinvrt,gexist,kexist,lexist,fexist
logical wexist,single
real inadim,xdim,ydim
character*8 gfilen,kfilen,lfilen,ffilen,wfilen
character*20 tfdir,pfdir,dsnme
common /design/
+ order,mxsord,si,sj,gerint,ostint,
+ qexist,qinvrt,gexist,kexist,lexist,fexist,
+ wexist,single,inadim,xdim,ydim,
+ gfilen,kfilen,lfilen,ffilen,wfilen,dsnme,
+ tfdir,pfdir
```

file DIM.BLK - Graph axis scale selection

```
real xlo,xhi,ylo,yhi
common/dim/ xlo,xhi,ylo,yhi
```

file MENU.BLK - Menu structure

```
logical escape
integer menunb
integer depth,oldmnu(10)
integer chcdf1(10)
integer top(2)
integer mnuinf(2,10)
character*20 choice(60)
character*45 messge(60)
common /menu/
+ mnuinf,choice,messge,depth,
+ chcdf1,top,oldmnu,menunb
```

file ROWOP.BLK - Row operation selections

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```

integer      ri,rj,ruse,cuse,rsord,wint
real         rkd(21),rkl,rkn(21),stp,eps
complex      quotient(200)
common       /rowop/
+           ri,rj,ruse,cuse,rsord,
+           rkd,rkl,rkn,stp,eps,wint,
+           quotient

```

1.4 SOURCE LISTING

```

$include:'add.blk'
*****
* INACAD * PROGRAM TO DO INA DESIGN *
*
*      written by R.VENZKE      All rights reserved. (c)86,87,88 *
*
*****
* Descr:  Uses the Inverse Nyquist Array technique to help design *
*          a controller for a multivariable control system.      *
*
* Notes:  The program must be linked with FOR2GRPH.OBJ (Graphx Support) *
*          and with MICROSOFT FORTRAN C LIBRARY for SYSTEM function and *
*          C type strings.                                         *
*
*          EXECUTION: Before INACAD can be used INT10 and HARDCOPY *
*                      must be run for GRAPHX support.           *
*
* File Support : INACAD.HLP - Online help fascility.             *
*
* Calls:   ansisup,DSNRST,CLRDSN,MNURST,INADSN,DELTMP             *
*****

```

```

program inacad
integer i
character*30 copy

```

```

$INCLUDE:'DESIGN.BLK'
$INCLUDE:'MENU.BLK'
$INCLUDE:'DESDTA.BLK'

```

```

copy='(c) RHE Venzke 86,87,88'
write(*,*)' INACAD Multi-Variable Control System',
+' Design Aid ',copy
write(*,*)' '
write(*,*)' '
tfdir=' '
pfdir='a:'
open(1,file='default.cad',iostat=ioccheck)
read(1,'(a40)',err=4) tfdir
read(1,'(a40)',err=4) pfdir
4 close(1)
call dsnrst
call clrdsn
call mnurst
open(1,file='default.ws',iostat=ioccheck)
read(1,'(i3)',err=2)noofw
do 1 i=1,noofw
1 read(1,'(e13.7)',err=2)w(i)

```

APPENDIX D SOFTWARE REFERENCE

```

        close(1)
        goto 3
2       close(1)
        noofw=51
        call calcwf(6,2)
3       inadim=20.
        multdim=2.
        wfilen='Default '
        call setmde
        call inadsn
        call deltmp
        open(1,file='default.cad',status='new')
        write(1,'(a40)',err=5) tmdir
        write(1,'(a40)',err=5) pmdir
5       close(1)
        call cls
        write(*,*)
+      ' INACAD ',copy,' terminated.'
        end

```

c Interface to Assembly routine QQGETCH

```

integer function getch
integer qqgetch,i
external qqgetch

i=qqgetch()

```

c Convert to lowercase

```

if ((i.gt.64).and.(i.le.90)) i=i+32
getch=i
return
end

```

c Interface to Assembly routine QQREADCH

```

integer function readch
integer qqreadch
external qqreadch

readch=qqreadch()
return
end

```

```

*****
* IOSUP.ASM I/O SUPPLEMENT - Assembly language *
*****
* Descr: The following Input routines were defined from Assembly language *
* to improve FORTRAN I/O. *
* *
*****

```

TITLE I/O LIBRARY

```

;SUBTL Copyright 1986 by R.Venzke
;LAST REVISION: 27-9-1986
;NAME I/O support for MS-Fortran

```

DATA SEGMENT PUBLIC 'DATA'

APPENDIX D SOFTWARE REFERENCE

```
DATA      ENDS

DGROUP   GROUP DATA

CODE      SEGMENT 'CODE'

ASSUME   CS:CODE
ASSUME   DS:DGROUP
ASSUME   SS:DGROUP

;QQreadch is a function returning ASCII code of key typed
;no echo
;INTEGER*4 READCH

PUBLIC   QQREAD
QQREAD   PROC FAR
        PUSH        BP
        MOV         BP,SP
        MOV         AH,7
        INT         21H
        MOV         AH,0
        MOV         DX,0
        MOV         SP,BP
        POP         BP
        RET
QQREAD   ENDP

;QQgetch flushes the input buffer and reads a key
;echo turned off
;INTEGER*4 GETCH

PUBLIC   QQGETC
QQGETC   PROC FAR
        PUSH        BP
        MOV         BP,SP
        MOV         AH,0CH
        MOV         AL,7
        INT         21H
        MOV         AH,0
        MOV         DX,0
        MOV         SP,BP
        POP         BP
        RET
QQGETC   ENDP

;Kbhit is a function to test if a key was pressed
;(returns TRUE if so)
;LOGICAL*4 KBHIT =0 if nokey was pressed

PUBLIC   KBHIT
KBHIT    PROC FAR
        PUSH        BP
        MOV         BP,SP
        MOV         AH,0BH
        INT         21H
        MOV         AH,AL
        MOV         DX,AX
        MOV         SP,BP
        POP         BP
        RET
KBHIT    ENDP
```

APPENDIX D SOFTWARE REFERENCE

CODE ENDS

END

```
$include:'add.blk'
*****
* ANSISUP.FOR ANSI.SYS SUPPLEMENT *
*****
* Descr: Screen interface subroutines. Uses ANSI.SYS driver to manipulate *
* screen output. *
* *
* Calls: none *
*****
```

c Clear the screen

```
subroutine cls
write(*, '( /1x,A1,A3,\)')27, '[0m'
write(*, '(A1,A3,\)')27, '[2J'
return
end
```

c Clear the bottom line

```
subroutine clrdsb
call normal
call gotorc(25,1)
call clreol
return
end
```

c Save cursor position

```
subroutine saverc
write(*, '(a1,a2,\)')27, '[s'
return
end
```

c Restore cursor position

```
subroutine loadrc
write(*, '(a1,a2,\)')27, '[u'
return
end
```

c Move cursor to ROW, COLUMN position

```
subroutine gotorc(row,column)
integer row,column
write(*, '(A1,A1,I2.2,A1,I2.2,A1,\)')27, '[' ,row
+, ';' ,column, 'H'
return
end
```

c Erase line

```
subroutine erasel
write(*, '(A1,A1,a1,\)')27, '[' , 'K'
```

APPENDIX D SOFTWARE REFERENCE

```
return  
end
```

c Clear to end of line

```
subroutine clreol  
write(*,'(A1,A1,a1,\)')27,['','K'  
return  
end
```

c Set black and white 80x25 text mode

```
subroutine setmde  
write(*,'(/1X,A1,A4,\)')27,['=2h'  
return  
end
```

c Set foreground WHITE and background BLACK

```
subroutine normal  
write(*,'(A1,A3,\)')27,['0m'  
return  
end
```

c Set inverse character display

```
subroutine invers  
write(*,'(A1,A3,\)')27,['7m'  
return  
end
```

c Clear bottom line using inverse bar

```
subroutine clrbot  
call gotorc(25,1)  
call invers  
call erasel  
return  
end
```

c Clear 24th row

```
subroutine clrtop  
call gotorc(24,1)  
call normal  
call erasel  
return  
end
```

c Convert character to lower case

```
integer function lowercase(i)  
integer i  
  
if ((i.ge.65).and.(i.le.90)) then  
i=i+32  
endif  
lowercase=i  
return  
end
```

APPENDIX D SOFTWARE REFERENCE

c Display wait message

```

subroutine wait
call normal
call gotorc(25,1)
call clreol
call gotorc(25,64)
write(*,'(a\)' ) ' Please wait...'
return
end

```

\$INCLUDE: 'ADD.BLK'

```

*****
* CALCPW * CALCULATE POLYNOMIAL AT (0,jw) *
*****
* Descr: The polynomial specified by real coefficients of POLY is evalu- *
* ated at (0,jw) as given by W. *
* *
* Param: RESULT is the complex result of the subroutine. *
* MXSORD is the maximum order of s that can be stored in POLY. *
* W is the real coefficient of jw *
* *
* Calls: none *
*****

```

```

subroutine calcpw(result,poly,mxsord,w)
integer mxsord
real poly(*),w
complex result,jw
complex*16 sum

sum=cplx(poly(mxsord+1),0.)
jw=cplx(0.,w)
do 1 i=mxsord,1,-1
1 sum=sum*jw+cplx(poly(i),0.)
result=sum
return
end

```

\$include: 'add.blk'

```

*****
* CALCQI * CALCULTE INA MATRIX Q AT FREQUENCY WI *
*****
* Descr: This subroutine calculates the INA response for one frequency *
* interval. File 1= temp.gs 2= temp.ks 3=temp.ls 4=temp.fs *
* are read from and result is written to file 9= temp.plt. *
* *
* Param: ORDER order of matrices. *
* QW storage for resulting response. *
* CALCG,CALCK,CALCL,CALCF logical to signify if matrices exist *
* INVERSE logical set true for INVERSE Nyquist *
* ERROR = true if a file access error occurred. *
* DET is the determinant of the resulting mx. *
* *
* Call.by: PLTINA *
* Calls: none *
*****

```

```

subroutine calcqi(qw,calcg,calck,calcl,calcf,error,det)

```

APPENDIX D SOFTWARE REFERENCE

```

complex  qw(*),mxb(100),det
logical  calcg,calck,calcl,calcf,error
integer  i,j,offset

$include:'design.blk'

error=.false.
if (calcg) then
  do 1 i=1,order*order
1    read(1,err=99) qw(i)
  else
    do 2 i=1,order
      offset=(i-1)*order
      do 2 j=1,order
        if (i.eq.j) then
          qw(j+offset)=cmplx(1.0,0.0)
        else
          qw(j+offset)=cmplx(0.0,0.0)
        endif
      2
    continue
  endif
  if (calcl) then
    do 3 i=1,order*order
3    read(3,err=99) mxb(i)
    call matmlt(mxb,qw,qw,order)
  endif
  if (calck) then
    do 4 i=1,order*order
4    read(2,err=99) mxb(i)
    call matmlt(qw,mxb,qw,order)
  endif
  if (qinvrt) then
    call cominv(qw,order,det)
  else
    det=cmplx(1,0)
  endif
  do 6 i=1,order*order
6    write(9,err=99) qw(i)
  goto 7
99  error=.true.
7   return
end

$include:'add.blk'
*****
* CALCTF * CALCULATE TRANSFER FUNCTION RESPONSE *
*****
* Descr:  The transfer function as specified in KN,KD,KL is evaluated *
*         at the frequency samples as given by W. The resulting complex *
*         table is stored in the specified file. *
*
* Param:  MXSORD is the maximum order of s that can be handled by KN,etc. *
*         KN are the numerator coefficients *
*         KD are the denominator coefficients *
*         KL is the lag *
*         W frequency table *
*         ORDER is the order of the transfer function matrix nxn *
*         ERROR is set to true if division by zero occurs. *
*         NOOFW contains the number of frequency points. *

```

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```

*          TFDIR is the subdirectory to use for filename.
*          NAME is the name for the file to write to.
*          EXT is the file extension to use.
*          QEXIST flag to indicate if transfer function has been changed.
*
* Call.by: EDITTF
* Calls:  CALCPW,DIMTF,DISK,ERROR
*****

```

```

+ subroutine calctf(w,noofw,kn,kd,kl,mxsord,order,
+                 name,tfdir,ext,qexist)

character*8 name
character*20 tfdir
character*4 ext
character*32 filen
logical      qexist,err
integer      iocheck
integer      noofw,mxsord,order,wi,row,col
integer      ij,ijk,ijw,sorder
real         kd(*),kl(*),kn(*),w(*),pi
complex      kw,nw,dw,lw
integer      getch,key
external     getch
character*40 message

err=.false.
qexist=.false.
pi=3.1415926536
call wait
call dimtf(order,mxsord,sorder,kn,kd)
call disk(filen,tfdir,name,ext)
95  open(1,file=filen,form='binary',status='NEW',iostat=iocheck)
do 1 wi=1,noofw
  do 1 row=1,order
    do 1 col=1,order
      ij=col+order*(row-1)
      ijk=1+(mxsord+1)*(ij-1)
      call calcpw(nw,kn(ijk),sorder,w(wi))
      call calcpw(dw,kd(ijk),sorder,w(wi))
      if (cabs(dw).le.1.e-8) then
        err=.true.
        kw=(0,0)
      elseif (kl(ij).eq.0) then
        kw=nw/dw
      else
        lw=cmplx(0.,amod( kl(ij)*w(wi) , 2 * pi ))
        kw=nw/dw*cexp(lw)
      endif
      write(1,err=92)kw
1    continue
    if (err) then
      call error('Division by zero ignored!  ')
    endif
    close(1,iostat=iocheck)
    if (iocheck.ne.0) goto 92
    goto 93
92  message=name
    message(9:40)=' removed from design!'
    call clrbot
    write(*,'(2a\)\') name,' write error! Press key to continue or

```

APPENDIX D SOFTWARE REFERENCE

```

+ESC to abort'
  if (getch().ne.27) goto 95
  call error(message)
  name=' '
93  return
    end

$include:'add.blk'
*****
* CALCWF * CALCULATE FREQUENCY SAMPLES *
*****
* Descr: The frequency sample table is initialised to the desired values. *
*
* Param: STDEC start decade *
*        ENDDC end decade *
*
* Call.by: EDITWF,DSNRST *
* Calls: none *
*****

c SQRT-LOG

  subroutine calcwf(stdect,endect)
  integer stdec,enddec,i,stdect,endect

$include:'desdta.blk'

  stdec=2*stdect
  enddec=endect*2
  do 3 i=0,noofw-1
    x=(stdec+enddec)*i/(noofw-1.)+1.
    if ((x-aint(x)).lt..1) x=.1+aint(x)
    if (x.ge.stdec) then
      w(i+1)=(x-aint(x))*10**(aint(x)-stdec)
    else
      w(i+1)=(x-aint(x))/10**(stdec-aint(x))
    endif
  3  continue
  do 4 i=1,noofw
  4  w(i)=sqrt(w(i))
  return
  end

c SQRT-SQRT-LOG
  subroutine calc2wf(stdect,endect)

  integer stdec,enddec,i,stdect,endect

$include:'desdta.blk'

  stdec=4*stdect
  enddec=endect*4
  do 3 i=0,noofw-1
    x=(stdec+enddec)*i/(noofw-1.)+1.
    if ((x-aint(x)).lt..1) x=.1+aint(x)
    if (x.ge.stdec) then
      w(i+1)=(x-aint(x))*10**(aint(x)-stdec)
    else
      w(i+1)=(x-aint(x))/10**(stdec-aint(x))
    endif

```

APPENDIX D SOFTWARE REFERENCE

```
3      continue
      do 4 i=1,noofw
4         w(i)=sqrt(sqrt(w(i)))
      return
      end

c SPECIAL
      subroutine specwf(stdec,enddec)

      integer stdec,enddec,cnt
      real size(18),x,step

$include:'desdta.blk'

      size(1)=1.0
      size(2)=1.1
      size(3)=1.2
      size(4)=1.3
      size(5)=1.4
      size(6)=1.5
      size(7)=1.6
      size(8)=1.7
      size(9)=1.8
      size(10)=1.9
      size(11)=2.0
      size(12)=3.0
      size(13)=4.0
      size(14)=5.0
      size(15)=6.0
      size(16)=7.0
      size(17)=8.0
      size(18)=9.0
      cnt=0
      do 1 i=stdec,enddec-1
          x=10.0**i
          do 1 j=1,18
              cnt=cnt+1
              if (cnt.le.200) w(cnt)=x*size(j)
1          continue
          cnt=cnt+1
          if (cnt.le.200) w(cnt)=10.0**i
          if ((noofw.eq.1).or.(cnt.le.noofw)) then
              noofw=cnt
          else
              step=1.0/noofw*cnt
              do 2 i=1,noofw
                  j=step*i
                  w(i)=w(j)
2          continue
          endif
          return
      end

c LOG
      subroutine logwf(stdect,endeect)
      integer stdec,enddec,i,stdect,endeect

$include:'desdta.blk'

      stdec=stdect
```

APPENDIX D SOFTWARE REFERENCE

```

enddec=endect
do 3 i=0,noofw-1
  x=(stdec+enddec)*i/(noofw-1.)+1.
  if ((x-aint(x)).lt..1) x=.1+aint(x)
  if (x.ge.stdec) then
    w(i+1)=(x-aint(x))*10.0**(aint(x)-stdec)
  else
    w(i+1)=(x-aint(x))/10.0**(stdec-aint(x))
  endif
3 continue
return
end

c LN
subroutine lnwf(stdect,endect)
integer stdec,enddec,i,stdect,endect

$include:'desdta.blk'

stdec=nint(stdect*log(10.)/log(2.74))
enddec=nint(endect*log(10.)/log(2.74))
do 3 i=0,noofw-1
  x=(stdec+enddec)*i/(noofw-1.)+1.
  if ((x-aint(x)).lt..1) x=.1+aint(x)
  if (x.ge.stdec) then
    w(i+1)=(x-aint(x))*EXP(aint(x)-stdec)
  else
    w(i+1)=(x-aint(x))/EXP(stdec-aint(x))
  endif
3 continue
return
end

$include:'add.blk'
*****
* COMINV * COMPLEX MATRIX INVERSION *
*****
* Descr:   Inverts a complex matrix using the Gauss-Jordan *
*          ellimination with complete pivoting *
* *
* Param:   B = Complex matrix *
*          N = Dimension of A where A is nxn *
*          C = Determinant *
* *
* Call.by: EDITTF *
* Calls:   none *
*****

SUBROUTINE COMINV(B,N,c)
INTEGER IR(10),IC(10)
C IR,IC are the pivot point of the matrix
COMPLEX*16 a(100),D,TEMP,HOLD
C A(100) double precision
complex b(*),c
INTEGER I,N,J,K,L,II,JJ,III,M,IJ,IIJ,IT,KI,KJ,LP

do 101 i=1,n*n
101 a(i)=b(i)
DO 10 I=1,N
IR(I)=I

```

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```

10      IC(I)=I
      CONTINUE
      D=(1.,0.)
      M=-N
      DO 70 I=1,N
        M=M+N+1
        IF (I.EQ.N) GOTO 40
        BIG=CdABS(A(M))
        II=I
        JJ=I
        DO 20 K=I,N
          LP=(I-2)*N+K
          DO 20 L=I,N
            LP=LP+N
            IF (CdABS(A(LP)).LE.BIG) GOTO 20
            BIG=CdABS(A(LP))
            II=K
            JJ=L
20      CONTINUE
22      IF (II.EQ.I) GOTO 30
        IJ=I-N
        IIJ=II-N
        DO 25 J=1,N
          IJ=IJ+N
          IIJ=IIJ+N
          TEMP=A(IJ)
          A(IJ)=A(IIJ)
          A(IIJ)=TEMP
25      CONTINUE
        IT=IR(I)
        IR(I)=IR(II)
        IR(II)=IT
        D=-D
30      IF (JJ.EQ.I) GOTO 40
        IJ=(I-1)*N
        IIJ=(JJ-1)*N
        DO 35 J=1,N
          IJ=IJ+1
          IIJ=IIJ+1
          TEMP=A(IJ)
          A(IJ)=A(IIJ)
          A(IIJ)=TEMP
35      CONTINUE
        IT=IC(JJ)
        IC(JJ)=IC(I)
        IC(I)=IT
        D=-D
40      if (cdabs(d*a(m)).lt.1.d-150) then
        c=(0,0)
        return
      endif
      D=D*A(M)
      TEMP=A(M)
      A(M)=(1.,0.)
      IJ=I-N
      DO 50 J=1,N
        IJ=IJ+N
        A(IJ)=A(IJ)/TEMP
50      CONTINUE
      KI=(I-1)*N
      DO 70 K=1,N

```

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```

        KI=KI+1
        IF (K.EQ.I) GOTO 70
        TEMP=A(KI)
        A(KI)=(0.,0.)
        KJ=K-N
        IJ=I-N
        DO 60 J=1,N
            KJ=KJ+N
            IJ=IJ+N
            HOLD=-TEMP*A(IJ)
            A(KJ)=A(KJ)+HOLD
60      CONTINUE
70      CONTINUE
72      CONTINUE
        DO 80 I=1,N
            IF (IR(I).EQ.I) GOTO 80
            K=IR(I)
            JI=(I-1)*N
            JK=(K-1)*N
            DO 85 J=1,N
                JI=JI+1
                JK=JK+1
                TEMP=A(JI)
                A(JI)=A(JK)
                A(JK)=TEMP
85      CONTINUE
            IR(I)=IR(K)
            IR(K)=K
        GOTO 72
80      CONTINUE
82      CONTINUE
        DO 90 I=1,N
            IF (IC(I).EQ.I) GOTO 90
            K=IC(I)
            IJ=I-N
            KJ=K-N
            DO 75 J=1,N
                IJ=IJ+N
                KJ=KJ+N
                TEMP=A(IJ)
                A(IJ)=A(KJ)
                A(KJ)=TEMP
75      CONTINUE
            IC(I)=IC(K)
            IC(K)=K
        GOTO 82
90      CONTINUE
        do 100 i=1,n*n
100     b(i)=a(i)
        c=d
        RETURN
        END

```

\$include: 'add.blk'

```

*****
* COMM2 * SET UP COMMAND WINDOW *
*****
* Descr: The command window is set to the possible commands. *
*        It is used when entering a transfer function. *
* *

```

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```
* Call.by: INPUTTF *
* Calls:  ansisup  *
*****
```

```
subroutine comm2

call invers
call gotorc(5,62)
write(*,'(a,\)')'  COMMANDS  '
call gotorc(6,62)
write(*,'(a,\)')'-----'
call gotorc(7,62)
write(*,'(a,\)')' Select  '
call gotorc(8,62)
write(*,'(a,\)')'  '
call gotorc(9,62)
write(*,'(a,\)')' <N>umerator  '
call gotorc(10,62)
write(*,'(a,\)')'  '
call gotorc(11,62)
write(*,'(a,\)')' <D>enominator  '
call gotorc(12,62)
write(*,'(a,\)')'  '
call gotorc(13,62)
write(*,'(a,\)')' <L>ag  '
call gotorc(14,62)
write(*,'(a,\)')'  '
call gotorc(15,62)
write(*,'(a,\)')' <P>ower of s  '
call gotorc(16,62)
write(*,'(a,\)')'  '
call gotorc(17,62)
write(*,'(a,\)')' <ESC> to Exit  '
call gotorc(18,62)
write(*,'(a,\)')'-----'
call normal
return
end
```

```
$include:'add.blk'
*****
* COMMND * SET UP COMMAND WINDOW *
*****
* Descr:  The command window is set to the possible commands. *
*         It is used when entering a transfer function. *
* * * * *
* Call.by: INPUTTF *
* Calls:  ansisup  *
*****
```

```
subroutine commnd

call invers
call gotorc(5,62)
write(*,'(a,\)')'  COMMANDS  '
call gotorc(6,62)
write(*,'(a,\)')'-----'
call gotorc(7,62)
write(*,'(a,\)')' Select  '
call gotorc(8,62)
```

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```

write(*,'(a,\)')'
call gotorc(9,62)
write(*,'(a,\)')' <N>umerator
call gotorc(10,62)
write(*,'(a,\)')'
call gotorc(11,62)
write(*,'(a,\)')' <D>enominator
call gotorc(12,62)
write(*,'(a,\)')'
call gotorc(13,62)
write(*,'(a,\)')' <L>ag
call gotorc(14,62)
write(*,'(a,\)')'
call gotorc(15,62)
write(*,'(a,\)')' <P>ower of s
call gotorc(16,62)
write(*,'(a,\)')'
call gotorc(17,62)
write(*,'(a,\)')' <J>ump to R,C
call gotorc(18,62)
write(*,'(a,\)')'
call gotorc(19,62)
write(*,'(a,\)')' <RTN> to Skip
call gotorc(20,62)
write(*,'(a,\)')'
call gotorc(21,62)
write(*,'(a,\)')' <ESC> to Exit
call gotorc(22,62)
write(*,'(a,\)')'-----'
call normal
return
end

```

\$include:'add.blk'

```

*****
* DIAGON * DO DIAGONALISATION DESIGN *
*****
* Descr:   Calls various INA design aids. *
*          Displays the diagonalisation menu. *
* * * * *
* Call.by: INADSN *
* Calls:   GETCHC,PLTINA,ROWOPE,SWOP,RCMLT,UNDOCH,PRTNYQ *
*****

```

subroutine diagon

\$INCLUDE:'MENU.BLK'

```

1      menunb=4
      call getchc(menunb,escape)
      if (escape) goto 2
      if (chcdf1(menunb).eq.0) then
        call nyqstp
      elseif (chcdf1(menunb).eq.1) then
        call pltina
      elseif (chcdf1(menunb).eq.2) then
        call rowope
      elseif (chcdf1(menunb).eq.3) then
        call swop
      elseif (chcdf1(menunb).eq.4) then

```

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```

        call rcmlt
    elseif (chcdf1(menunb).eq.5) then
        call undoch
    elseif (chcdf1(menunb).eq.6) then
        call prtnyq
    endif
    goto 1
2    return
    end

```

```

$include:'add.blk'
*****
* DIMTF * FIND DIMENSIONS OF S IN TRANSFER FUNCTION *
*****
* Descr: This procedure searches through the transfer function *
*         coefficient array KN,KD to find the maximum power of s *
*         used in the numerator and denominator elements. *
*
*         ! Automatically sets denominator to 1 if all coefficients equal 0 *
*
* Param: ORDER order of transfer function matrix *
*         MXSORD maximum allowed order for s. *
*         SORDER returns the maximum order of s used. *
*
* Call.by: CALCPW, INPUTTF *
* Calls: none *
*****

```

```

subroutine dimtf(order,mxsord,sorder,kn,kd)

```

```

integer order,mxsord,m,n,sorder
integer row,col,ij,ijk,power
logical first
real kn(*),kd(*)

```

```

sorder=0
do 2 row=1,order
  do 2 col=1,order
    ij=(col-1)*order+row
    ijk=(ij-1)*(mxsord+1)+1
    power=mxsord
4    if (kn(ijk+power).ne.0) goto 3
    power=power-1
    if (power.gt.sorder) goto 4
3    if (power.gt.sorder) sorder=power
    power=mxsord
6    if (kd(ijk+power).ne.0) goto 5
    power=power-1
    if (power.gt.0) goto 6
    if(kd(ijk).eq.0) kd(ijk)=1.
5    if (power.gt.sorder) sorder=power
2  continue
  return
end

```

```

$include:'add.blk'
*****
* DISK * FORM DISK FILE NAME *
*****

```

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```
*****
* Descr: Here the name for a file on disk is concatenated from      *
*         the directory DIR ,NAME and EXTension into CONCAT.      *
*                                                                 *
* Calls: none                                                    *
*****
```

```
subroutine disk(concat,dir,name,ext)
```

```
character*32 concat
character*20 dir
character*8 name
character*4 ext
integer index,len
```

```

index=1
2  if (index.eq.20) goto 3
   if (dir(index+1:index+1).eq.' ') goto 3
   index=index+1
   goto 2
3  len=1
4  if (len.eq.8) goto 5
   if (name(len+1:len+1).eq.' ') goto 5
   len=len+1
   goto 4
5  if (dir.eq.' ') then
     concat(1:len)=name(1:len)
     concat(len+1:len+4)=ext(1:4)
     concat(len+5:32)=' '
   else
     concat(1:index)=dir(1:index)
     concat(index+1:index+len)=name(1:len)
     concat(1+index+len:index+len+4)=ext(1:4)
     concat(index+len+5:32)=' '
   endif
   return
end
```

```
$include:'add.blk'
```

```
*****
* DRAWC * DRAW COMPLEX VALUE                                     *
*****
* Descr: Plots a line between two given complex values at the cor- *
*         responding axis.                                       *
*                                                                 *
* Param: I,J index to axis.                                     *
*         QW(1) 1st complex point                               *
*         QW(OFFSET) 2nd complex point                         *
*         ORDER INA matrix order                              *
*         DIM dimension of axis                                *
*                                                                 *
* Call.by: PLOTPTS                                             *
* Calls: Hercules support DLINE.                               *
*****
```

```
subroutine drawc(i,j,qw,offset,order,dim)
```

```
integer i,j,offset,order
real x,y,x2,y2,dim,xdiv,ydiv,yp,xpl,ypl
```

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```

        complex    qw(*)

        x=real(qw(1))
        y=aimag(qw(1))
        x2=real(qw(1+offset))
        y2=aimag(qw(1+offset))
        if ((abs(x).le.dim).and.(abs(y).le.dim)
+         .and.(abs(x2).le.dim).and.(abs(y2).le.dim)) then
            xdiv=521./order/2.*(2*j-1)
            ydiv=347./order/2.*(2*i-1)
            xpl=xdiv+521.*x/order/2./dim
            ypl=ydiv-347.*y/order/2./dim
            call putpt(nint(xpl),nint(ypl))
            xp=xdiv+521.*x2/order/2./dim
            yp=ydiv-347.*y2/order/2./dim
            call dline(nint(xp),nint(yp))
c         if ((abs(nint(xp)-nint(xpl)).ge.12).or.
c         +     (abs(nint(yp)-nint(ypl)).ge.8))
c         +     call mark(nint(xp),nint(yp))
        endif
        return
        end

c Mark the position

        subroutine mark(i,j)
        integer i,j
        call putpt(i-3,j)
        call dline(i+3,j)
        call putpt(i,j-2)
        call dline(i,j+2)
        return
        end

$include:'add.blk'
*****
* DSNRST * DESIGN PARAMETERS RESET *
*****
* Descr:   Sets the design enviroment to default. *
* * * * *
* Call.by: INACAD *
* Calls:   none *
*****

        subroutine dsnrst
        integer iocheck,i,runid

$INCLUDE:'DESIGN.BLK'
$INCLUDE:'DESdta.BLK'

c Copy protection scheme

        open(1,file='\ina.cad',iostat=iocheck)
        read(1,22,err=1)runid
22      format(i3)
        runid=runid+1
        rewind 1
        if (runid.gt.30000) runid=0
        write(1,22,err=1)runid
        close(1)

```

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```

1      goto 2
      write(*,*)
      write(*,*)
      write(*,*) 'Unauthorised Duplicate.'
      stop

2      noofw=51
      call calcwf(3,3)
      order=1
      mxsord=20
      qexist=.false.
      wexist=.false.
      gexist=.false.
      kexist=.false.
      lexisit=.false.
      fexist=.false.
      gfilen='      '
      kfilen='      '
      lfilen='      '
      ffilen='      '
      wfilen='DEFAULT '
      dsnnme='      '
      gerint=0
      ostint=0
      qexist=.false.
      qinvrt=.true.
      single=.false.
      inadim=0.
      multdim=0.
      call gmode
      call clrscr
      call tmode
      return
      end

$include:'add.blk'
*****
*EDITMLT * EDIT MULTIPLYING FACTOR *
*****
* Descr:  The multiplication factor used for any row operation is *
*         displayed and can be edited here. *
* * * * *
* Param:  ORDER - Order of INA design. *
*         SORDER - Highest power of s used. *
*         KD - Denominator coefficients. *
*         KN - Numerator coefficients. *
*         KL - Lag *
*         MXSORD - Maximum order of s allowed *
*         CHANGE - Set TRUE if multiplier is altered *
* * * * *
* Call.by: ROWOP,RCMLT *
* Calls:   ansisup,COMM2 *
*****

      subroutine editmlt(order,sorder,kd,kn,kl,mxsord,change)

      character*20 input
      logical      escape,change
      integer      sorder,order,i,it,jt,j,k,ij,kij,mxsord
      real         kd(*),kn(*),kl

```

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```

real          num

integer      getch,key
external     getch

$include:'rowop.blk'

i=1
j=1
2  call cls
   call invers
   call gotorc(1,20)
   write(*,'(a\)\')' Editing Multiplication Factor '
   call gotorc(1,62)
   call invers
   if (ruse.ne.0) then
     write(*,'(a\)\')' Row used: '
     write(*,'(i2.2\)\')ruse
   else
     write(*,'(a\)\')' Column used:'
     write(*,'(i2.2\)\')cuse
   endif
   call gotorc(3,1)
   write(*,'(2a,2a1\)\')
+' Order of s Numerator      Denominator      L',
+'ag      ',13,10
   do 5 k=0,sorder
     write(*,'(i7,a,a1,a1\)\')k,'      ',13,10
5  continue
   call comm2
4  call invers
   call gotorc(1,1)
   call normal
   write(*,'(a,i2,a,i2,3a1\)\')'Reduce: (' ,ri',' ,rj,')',13,10
   ij=(j-1)*order+i
   kij=(ij-1)*(mxsord+1)
   do 25 k=1,sorder+1
     call gotorc(3+k,13)
     write(*,111)kn(kij+k)
     write(*,112)kd(kij+k)
     if (k.eq.1) write(*,113)k1
25  continue
   call normal
22  call gotorc(7,62+8)
   key=lowercase(getch())
   if ((key.ne.13).and.(key.ne.27).and.(key.ne.110).and.(key.ne.100
+).and.(key.ne.108).and.(key.ne.112)) goto 22
   if (key.eq.13)goto 7
   if (key.eq.27)goto 7
   if (key.eq.110) then
10  k=0
     k=k+1
     call invers
     call gotorc(3+k,13)
     write(*,111)kn(kij+k)
     call gotorc(3+k,13)
     call readln(input,14,escape)
     call normal
     if (escape) goto 11
     if (input.eq.'      ') goto 8
     read(input,110,err=9) num

```

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```

      kn(kij+k)=num
      change=.true.
8      call gotorc(3+k,13)
      write(*,111)kn(kij+k)
      goto 16
9      write(*,'(al\)' )7
      call gotorc(3+k,13)
      write(*,111)kn(kij+k)
      k=k-1
16     if (k.lt.sorder+1) goto 10
      key=100
11     call gotorc(3+k,13)
      write(*,111)kn(kij+k)
endif
if (key.eq.100) then
  k=0
12   k=k+1
      call invers
      call gotorc(3+k,13+18)
      write(*,111)kd(kij+k)
      call gotorc(3+k,13+18)
      call readln(input,14,escape)
      call normal
      if (escape) goto 14
      if (input.eq.'      ') goto 13
      read(input,110,err=15) num
      kd(kij+k)=num
      change=.true.
13   call gotorc(3+k,13+18)
      write(*,111)kd(kij+k)
      goto 17
15   write(*,'(al\)' )7
      call gotorc(3+k,13+18)
      write(*,111)kd(kij+k)
      k=k-1
17   if (k.lt.sorder+1) goto 12
      key=108
14   call gotorc(3+k,13+18)
      write(*,111)kd(kij+k)
endif
if (key.eq.108) then
18   call invers
      call gotorc(4,13+18+16)
      write(*,111)k1
      call gotorc*4,13+18+16)
      call readln(input,14,escape)
      call normal
      if (escape) goto 19
      if (input.eq.'      ') goto 21
      read(input,110,err=20) num
      k1=num
      change=.true.
21   call gotorc(4,13+18+16)
      write(*,111)k1
      goto 19
20   write(*,'(al\)' )7
      call gotorc(4,13+18+16)
      write(*,111)k1
      goto 18
19   call gotorc(4,13+18+16)
      write(*,111)k1

```

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```

endif
if (key.eq.112) then
1  call gotorc(25,1)
   write(*,'(15x,a,i1,a)\')' Change Power to (0-' ,mxsord,') : '
   call readln(input,2,escape)
   call normal
   call gotorc(25,1)
   call clreol
   if (.not.(escape.or.(input.eq.'          '))) then
       read(input,100,err=1) neworder
       if ((neworder.ge.0).and.(neworder.le.mxsord)) then
           sorder=neworder
       endif
   endif
endif
endif
if (key.eq.112) goto 2
goto 22
7  continue
do 77 i=sorder+2,mxsord+1
   kd(i)=0
77  kn(i)=0
return
100 format(bn,i2)
110 format(bn,e13.6)
111 format(lp,e14.7,\)
112 format(lp,e18.7,\)
113 format(lp,e16.7,\)
130 format(bn,2i2)
end

$include:'add.blk'
*****
* EDITTF * EDIT TRANSFER FUNCTION MATRIX *
*****
* Descr:  Allows the user to manipulate the process matrixes. *
* * *
* Param:  DIR,NAME,EXT name of file containing data. *
*         EXIST logical set to true if this file has been altered. *
*         ARRnd1 arrays containing coefficients *
* * *
* Call.by: PRCPAR *
* Calls:  ansisup,CALCTF,SAVCTF,LOADTF,DIMTF,INPUTTF,PRINTTF,GETCHC,RESETTF *
*****

subroutine edittf(name,ext,ext2,arrn,arrd,arr1,exist)

character*4  ext,ext2
character*8  name,oldname
character*32  filen
logical      exist,change,dexist,found
real         arrn(*),arrd(*),arr1(*)
integer      getch,sorder,key
external     getch

$INCLUDE:'DESDTA.BLK'
$INCLUDE:'DESIGN.BLK'
$INCLUDE:'MENU.BLK'

11  menunb=5

```

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```

call getchc(menunb,escape)
if (escape) goto l11
if (chcdf1(menunb).eq.0) then
  call getname(pfdir,name,ext,.true.,exist,escape)
  if (.not.escape) then
    call loadtf(pfdir,name,ext,arn,arrrd,arrrl,
+           order,mxsord,exist)
    if (name.ne.' ') then
      call calctf(w,noofw,arn,arrrd,arrrl,mxsord,order,
+           name,tfdir,ext2,qexist)
    endif
  endif
elseif (chcdf1(menunb).eq.1) then
  if (name.eq.' ') then
    call getname(pfdir,name,ext,.false.,exist,escape)
  endif
  if (.not.escape) then
    call dimtf(order,mxsord,sorder,arn,arrrd)
    if (sorder.eq.0) sorder=2
    call inputtf(name,ext,order,sorder,arrrd,arn,arrrl,
+           (ext.eq.'.FS '),change,mxsord)
    if (change) then
10      call clrbot
        write*,'(a\)' ' Press RETURN to calculate ...'
        if (getch().ne.13) then
          call inputtf(name,ext,order,sorder,arrrd,arn,arrrl,
+           (ext.eq.'.FS '),change,mxsord)
        goto 10
        endif
        exist=.true.
        call calctf(w,noofw,arn,arrrd,arrrl,mxsord,order,
+           name,tfdir,ext2,qexist)
    endif
  endif
elseif (chcdf1(menunb).eq.2) then
  oldname=name
  call getname(pfdir,name,ext,.false.,exist,escape)
  if (.not.escape) then
    call savetf(pfdir,name,ext,arn,arrrd,arrrl,
+           order,mxsord,exist)
    if (oldname.ne.name) then
      call calctf(w,noofw,arn,arrrd,arrrl,mxsord,order,
+           name,tfdir,ext2,qexist)
    endif
  endif
elseif (chcdf1(menunb).eq.3) then
  if (name.ne.' ') then
    call printtf(pfdir,name,ext,arn,arrrd,arrrl,order,mxsord)
  else
    call error('No matrix specified! ')
  endif
elseif (chcdf1(menunb).eq.4) then
  if (exist) then
    call clrbot
    write*,'(4a\)' ' Warning: Old ',name,ext,
+           ' will be LOST! Press <ESC> to abort...'
    if (getch().ne.27) exist=.false.
  endif
  if (.not.exist) then
    do 1 i=1,1000
      if (i.le.100) arrrl(i)=0.

```

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```

        arrn(i)=0.
        arrd(i)=0.
1      continue
        name=' '
        exist=.false.
        endif
    endif
    goto 11
111   return
    end

$include:'add.blk'
*****
* EDITWF * EDIT FREQUENCY TABLE *
*****
* Descr: The operator can specify the type of frequencies, the range *
*        and the number of frequency points. *
* * *
* Param: W - Frequency table *
*        NOOFW - Number of frequency points *
*        WEXIST - Set TRUE if it is altered. *
*        FILEN - Filename of frequency data *
* * *
* Calls: REDOWF,CALCWF. *
*****

        subroutine editwf(w,noofw,wexist,filen)
        logical      wexist,change,escape
        integer      noofw,type
        real         w(*)
        integer      stdec,enddec,newnb,oldnfw,getch,key
        character*20 input
        character*8  filen
        external     getch

        type=1
        call normal
        call gotorc(4,25)
        write(*,'(2a)')'Editing Frequency File : ',filen
        oldnfw=noofw

c      use W(2) rather than W(1) because W(1) may be equal to zero

        if (w(2).eq.0) then
            stdec=-9
        else
            stdec=nint(log10(w(2)))
        endif
        if (w(noofw).eq.0) then
            enddec=-9
        else
            enddec=nint(log10(w(noofw)))
        endif
        call gotorc(10,20)
        write(*,'(a)')'Start Frequency   : 10^'
        write(*,'(i3,a)')stdec,' Rad/s
        call gotorc(12,20)
        write(*,'(a)')'Final Frequency   : 10^'
        write(*,'(i3,a)')enddec,' Rad/s'
        call gotorc(14,20)

```

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```

write(*,'(a\)' )'Number of Samples : '
write(*,'(i3\)' )noofw
change=.false.
1 call gotorc(25,20)
  call invers
  write(*,'(a\)' )' Press <ESC> to leave unchanged.'
  call normal
4 call gotorc(8,20)
  write(*,'(a\)' )'Frequency Points : '
  if (type.eq.1) call invers
  write(*,'(a\)' )' SqrtLog '
  call normal
  if (type.eq.2) call invers
  write(*,'(a\)' )' Log '
  call normal
  if (type.eq.3) call invers
  write(*,'(a\)' )' Sqrt2Log '
  call normal
  if (type.eq.4) call invers
  write(*,'(a\)' )' Ln '
  call normal
  if (type.eq.5) call invers
  write(*,'(a\)' )' Special '
  call inverse
  call gotorc(9,22)
  write(*,'(a\)' )' Press <SPACE BAR> to change selection. '
  key=getch()
  call normal
  call gotorc(9,20)
  call clreol
  if (key.eq.27) goto 999
  if (key.eq.32) then
    type=type+1
    if (type.eq.6) type=1
    change=.true.
    goto 4
  endif
2 call gotorc(10,20)
  write(*,'(a\)' )'Start Frequency : 10^'
  call saverc
  write(*,'(i3,a\)' )stdec,' Rad/s'
  call invers
  call gotorc(11,22)
  write(*,'(a\)' )' Enter new decade. '
  call normal
  call loadrc
  call readln(input,3,escape)
  call gotorc(11,20)
  call clreol
  if (escape) goto 999
  if (input.eq.' ') goto 3
  read(input,100,err=92) newnb
  if (newnb.ne.stdec) then
    if (newnb.lt.enddec) then
      stdec=newnb
      change=.true.
    endif
  endif
  goto 2
3 call gotorc(12,20)
  write(*,'(a\)' )'Final Frequency : 10^'

```

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```

call saverc
write(*,'(i3,a\)' )enddec,' Rad/s'
call invers
call gotorc(13,22)
write(*,'(a\)' )' Enter new decade. '
call normal
call loadrc
call readln(input,3,escape)
call gotorc(13,20)
call clreol
if (escape) goto 999
if (input.eq.' ') goto 5
read(input,100,err=94) newnb
if (newnb.ne.enddec) then
    if (stdec.lt.newnb) then
        enddec=newnb
        change=.true.
    endif
endif
goto 3
5 call gotorc(14,20)
write(*,'(a\)' )'Number of Samples : '
call saverc
write(*,'(i3\)' )noofw
call invers
call gotorc(15,22)
write(*,'(a\)' )' Enter number from 2 to 200. '
call normal
call loadrc
call readln(input,3,escape)
call gotorc(15,20)
call clreol
if (escape) goto 999
if (input.eq.' ') goto 7
read(input,101,err=96) newnb
if (newnb.ne.noofw) then
    if ((newnb.gt.1).and.(newnb.le.200)) then
        noofw=newnb
        change=.true.
    endif
endif
goto 5
7 if (.not.change) goto 1
call invers
call gotorc(17,20)
write(*,'(a\)' )' Press ''Y'' to accept change...'
call normal
if (getch().ne.121) then
    call gotorc(17,20)
    call clreol
    goto 1
endif
if (type.eq.2) then
    call logwf(-stdec,enddec)
elseif (type.eq.3) then
    call calc2wf(-stdec,enddec)
elseif (type.eq.4) then
    call lnwf(-stdec,enddec)
elseif (type.eq.1) then
    call calcwf(-stdec,enddec)
else

```

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```

        call specwf(stdec,enddec)
    endif
    call redowf
    wexist=.true.
    goto 11

92     write(*,'(a1\)' )7
        goto 2
94     write(*,'(a1\)' )7
        goto 3
96     write(*,'(a1\)' )7
        goto 5

999    escape=.true.
        noofw=oldnfw
11     return
100    format(bn,i3)
101    format(bn,i3)
        end

$include:'add.blk'
*****
* ERROR * DISPLAY ERROR MESSAGE *
*****
* Descr:  Displays an error message on the bottom line and waits *
*         for a key to be pressed. *
* * *
* Param:  MESSAGE - Error message *
* * *
* Calls:  ansisup, *
*****

        subroutine error(message)

        character*30 message
        integer      key,getch
        external     getch

        call clrbot
        write(*,'(a1,3a\)' ) 7,'      ERROR: ',message,
+      ' Press any key to continue...'
        key=getch()
        call normal
        call gotorc(25,1)
        call clreol
        return
        end

$include:'add.blk'
*****
* FRANGE * SET FREQUENCY RANGE *
*****
* Descr:  Display menu to load, save or edit the frequency file. *
* * *
* Call.by:  PRCPAR *
* Calls:  ansisup,GETCHC,LOADWF,REDOWF,GETNAME,SAVEWF,EDITWF. *
*****

```

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```

subroutine frange
character*20 oldwname
integer      getch
external    getch

$include:'menu.blk'
$include:'design.blk'
$include:'desdta.blk'

11      menunb=6
        call getchc(menunb,escape)
        if (escape) goto 111
        if (chcdf1(menunb).eq.0) then
            oldwname=wfilen
            call getname(pfdir,wfilen,'.WS ',.true.,wexist,escape)
            if (.not.escape) then
                call loadwf(pfdir,wfilen,'.WS ',w,noofw,wexist)
                if (wfilen.eq.' ') then
                    wfilen=oldwname
                else
                    call redowf
                endif
            endif
        elseif (chcdf1(menunb).eq.2) then
            call getname(pfdir,wfilen,'.WS ',.false.,wexist,escape)
            if (.not.escape)
+         call savewf(pfdir,wfilen,'.WS ',w,noofw,wexist)
        elseif (chcdf1(menunb).eq.1) then
            call editwf(w,noofw,wexist,wfilen)
        endif
        goto 11
111     return
        end

```

\$include:'add.blk'

```

*****
* GETCHC * GET MENU CHOICE *
*****
* Descr:  This routine displays the menu as specified by MENUNB and *
*         returns the selected item in CHCDFL(MENUNB). If escape is *
*         pressed instead the logical ESCAPE becomes true. *
* * * * *
* Calls:  ansisup *
*****

```

```

subroutine getchc(mnunb,escape)

integer    i,ch,getch,readch
integer    msgrow,mnunb
logical    done
external   getch,readch

```

\$INCLUDE:'MENU.BLK'

```

menunb=mnunb
done=.false.
escape=.false.
ch=32

```

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```

if(oldmnu(depth).ne.menunb)depth=depth+1
call cls
if (menunb.eq.2) then
  call gotorc(1,1)
  write(*,'(3a\)' )'          INACAD Multi-Variable Control System',
+ ' Design Aid',
+ ' (c)RHE Venzke 1986,87,88'
  else
    call invers
    call gotorc(top(1),top(2)+4)
    write(*,'(a,\)' )choice(mnuinf(1,oldmnu(depth-1))
+   +chcdf1(oldmnu(depth-1)))
  endif
  call gotorc(1,1)
  call invers
  write(*,'(A,\)' )' Menu '
  do 3 i=2,depth
    write(*,'(I1,A,\)' )chcdf1(oldmnu(i-1))+1,'.'
3  continue
  write(*,'(A1,A4,\)' )27,'[ID '
  call invers
  call gotorc(2+top(1),top(2)-9)
  write(*,'(a,\)' )' Select:'
  call normal
  do 1 i=mnuinf(1,menunb),mnuinf(2,menunb)-1
    call gotorc(4+top(1)+2*(i-mnuinf(1,menunb)),top(2)-5)
    write(*,'(A,I1,A,A,\)' )'f',1+i-mnuinf(1,menunb)
+,' ',choice(i)
1  continue
  call gotorc(4+top(1)+2*(i-mnuinf(1,menunb)),top(2)-6)
  write(*,'(2a,\)' )'Esc ',choice(i)
  msgrow=6+top(1)+2*(i-mnuinf(1,menunb))
  call invers
  call gotorc(msgrow,top(2)-9)
  write(*,'(a,\)' )' Choice: '
2  continue
  call invers
  call gotorc(4+top(1)+2*chcdf1(menunb),top(2))
  write(*,'(a,\)' ) choice(chcdf1(menunb)+mnuinf(1,menunb))
  call normal
  call gotorc(msgrow,top(2))
  write(*,'(a,\)' ) message(chcdf1(menunb)+mnuinf(1,menunb))
  ch=getch()
  if (ch.eq.0) then
    ch=readch()
    if ((ch.eq.77).or.(ch.eq.80).or.(ch.eq.79).or.(ch.eq.81)) then
      call gotorc(3+top(1)+2*chcdf1(menunb),top(2))
      write(*,'(a,\)' )'
      call gotorc(4+top(1)+2*chcdf1(menunb),top(2))
      write(*,'(a,\)' ) choice(chcdf1(menunb)+mnuinf(1,menunb))
      chcdf1(menunb)=chcdf1(menunb)+1
      if ((ch.eq.79).or.(ch.eq.81))chcdf1(menunb)=mnuinf(2,menunb)
+ -mnuinf(1,menunb)
      if (chcdf1(menunb).gt.(mnuinf(2,menunb)
+ -mnuinf(1,menunb))) then
        chcdf1(menunb)=0
      endif
    elseif ((ch.eq.75).or.(ch.eq.72).or.(ch.eq.71).or.(ch.eq.73)) then
      call gotorc(3+top(1)+2*chcdf1(menunb),top(2))
      write(*,'(a,\)' )'
      call gotorc(4+top(1)+2*chcdf1(menunb),top(2))

```

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```

write(*,'(a,\)') choice(chcdf1(menunb)+mnuinf(1,menunb))
chcdf1(menunb)=chcdf1(menunb)-1
if ((ch.eq.71).or.(ch.eq.73)) chcdf1(menunb)=0
if (chcdf1(menunb).lt.0) then
  chcdf1(menunb)=mnuinf(2,menunb)-mnuinf(1,menunb)
endif
elseif ((ch.ge.59).and.((ch-59).lt.
+   (mnuinf(2,menunb)-mnuinf(1,menunb)))) then
  chcdf1(menunb)=ch-59
  done=.true.
endif
elseif (ch.eq.13) then
  done=.true.
elseif (ch.eq.27) then
  done=.true.
  escape=.true.
endif
if (.not.done) goto 2
if (escape.or.(chcdf1(menunb).eq.(mnuinf(2,menunb)-
+   mnuinf(1,menunb)))) then
  depth=depth-1
  escape=.true.
else
  oldmnu(depth)=menunb
  call cls
  call invers
  call gotorc(top(1),top(2)+4)
  write(*,'(a,\)')choice(mnuinf(1,oldmnu(depth))
+   +chcdf1(oldmnu(depth)))
  call gotorc(1,1)
  call invers
  write(*,'(A,\)')' Menu '
  do 4 i=2,depth+1
    write(*,'(I1,A,\)')chcdf1(oldmnu(i-1))+1,'.'
4   continue
    write(*,'(A1,A4,\)')27,'[1D '
    call normal
  endif
  return
end

$include:'add.blk'
*****
* GETNAME* GET FILENAME FROM USER *
*****
* Descr:   Here the user is prompted for a filename. This routine is used *
*          both for saving and loading. It checks whether the file exists. *
*          * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * *
* Param:   DIR,NAME,EXT Complete filename. *
*          LOAD Logical false if used for saving else for loading. *
*          NAME = ' ' if used for loading but file not found. *
*          ESCAPE logical true if escape was pressed. *
*          EXIST logical true if old file needs to be saved. *
*          * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * *
* Call.by: EDITTF,LOADTF,SAVTF *
* Calls:   ansisup,SYSCAL *
*****

subroutine getname(dir,name,ext,load,exist,escape)

```

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```

character*32 fname
character*20 dir
character*8  name,newname,oldname,tname
character*4  ext
character*40[c] command
logical      load,escape,found,exist
integer      i,getch,key
external     getch

oldname=name
1 call normal
call gotorc(4,20)
write(*,'(a\)' )'File directory= '
if (dir.eq.' ') then
  write(*,'(a\)' )'default'
else
  write(*,'(a\)' )dir
endif
call gotorc(6,20)
call clreol
call gotorc(6,20)
write(*,'(a\)' )'Enter filename: '
call saverc
write(*,'(4a\)' )name,['',ext,']
if (exist.and.load) then
  call clrbot
  + ' will be LOST!   Press <ESC> to abort.'
  call normal
endif
call inverse
call gotorc(8,20)
write(*,'(a\)' )' Press <Enter> for default filename.'
call normal
call loadrc
call readln(newname,8,escape)
if (escape) name=oldname
if (escape) goto 100
if (newname.ne.' ') name=newname
call disk(fname,dir,name,ext)
inquire(file=fname,err=99,exist=found)
call gotorc(6,51)
call inverse
if (found) then
  write(*,'(a\)' )' FOUND '
  if ((.not.load).and.(oldname.ne.name)) then
    call clrbot
    + '   Press <ESC> to abort...'
    if (getch().eq.27) then
      call normal
      call gotorc(25,1)
      call clreol
      goto 1
    endif
  endif
elseif (.not.load) then
  write(*,'(a\)' )' NEW FILE '
  do 2 i=1,2000
2  continue

```

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```

else
  write(*,'(a,a1\))' NOT FOUND ',7
  call normal
  write(tname,'(2a)') '**',ext
  call disk(fname,dir,tname,' /w ')
  call gotorc(10,1)
  write(command,'(2a)') 'dir ',fname
  call syscal(command)
  write(*,'(2a1\))'13,10
  write(*,'(a\))' 'Press any key to continue...'
  key=getch()
  call cls
endif
if (.not.found.and.load) goto 1
if (name.eq.' ') goto 1
goto 100

99   call error('Disk fault!          ')
      goto 1

100  return
      end

$include:'add.blk'
*****
* GETORD * GET MATRIX ORDER *
*****
* Descr:   Sets the order of the transfer matrices. *
*          Calculates MXSORD which contains the maximum order of s that *
*          can be stored in the available data space. *
*          * *
* Call.by: PRCPAR *
* Calls:   READLN,DSNRST,ansisup *
*****

      subroutine getord

      character*20 input
      logical      escape
      integer      num

$INCLUDE:'DESIGN.BLK'

1     call clrdsp
      call gotorc(4,10)
      write(*,'(A\))' 'Select transfer matrices order (NxN)'
      call gotorc(5,11)
      write(*,'(a\))' 'where N ranges from 1 to 10.'
      call gotorc(7,10)
      write(*,'(a\))' 'Enter order N: '
      call saverc
      write(*,'(i2.2\))' order
      call gotorc(9,10)
      write(*,'(a,i2\))' 'Maximum order of s of polynomials= ',mxsord
      call loadrc
      call readln(input,2,escape)
      if (escape) goto 10
      if (input.eq.' ') goto 10
      read(input,100,err=11)num
      if ((num.gt.10).or.(num.le.0)) goto 11

```

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```

        order=num
        mxsord=1000/order/order-1.5
        if (mxsord.gt.20) mxsord=20
        goto 1
11      write(*,'(a1\)' ) 7
        goto 1
10      return
100     format(bn,i2)
        end

$include:'add.blk'
*****
* GETQU2 * GET QUOTIENT *
*****
* Descr:   Get quotient from INA diagram. *
*         Used by row/ column multiplication routine. *
*         * *
* Param:   none *
*         * *
* Call.by: ROWMLT *
* Calls:   ansisup. *
*****

        subroutine getqu2

        character*32 filen
        integer      iocheck,ci,cj,wi,row,col
        complex      kw
        integer      getch,key
        external     getch

$include:'rowop.blk'
$include:'design.blk'
$include:'desdta.blk'

        if (.not.qexist) then
            call error('No Nyquist Diagram exists!  ')
            do 3 i=1,noofw
3          quotient(i)=(0,0)
            goto 10
        endif
        call wait
        if (ruse.ne.0) then
            ci=ruse
            cj=rj
        else
            ci=ri
            cj=cuse
        endif
        call disk(filen,tfdir,'nyquist ','~jw')
2      open(1,file=filen,form='binary',iostat=iocheck)
        do 1 wi=1,noofw
            do 1 row=1,order
                do 1 col=1,order
                    read(1,err=92)kw
                    if ((row.eq.ci).or.(col.eq.cj))
1          +      quotient(wi)=1/kw
                continue
            close(1)

```

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```

    goto 10
92    call error('INA diagram file corrupted!  ')
    close(1)
10    return
    end

$include:'add.blk'
*****
* GETQUOT* GET QUOTIENT *
*****
* Descr:  Gets the specified quotient from the INA diagram to be used *
*         by row or column operations. *
* *
* Param:  Given by ROWOP.BLK *
* *
* Call.by: ROWOP *
* Calls:  ansisup. *
*****

    subroutine getquot

    character*32 filen
    integer      ioccheck,ci,cj,wi,row,col
    complex      kw
    integer      getch,key
    external     getch

$include:'rowop.blk'
$include:'design.blk'
$include:'desdta.blk'

    if (.not.qexist) then
        call error('No Nyquist Diagram exists!  ')
        do 3 i=1,noofw
3         quotient(i)=(0,0)
        goto 10
    endif
    call wait
    if (ruse.ne.0) then
        ci=ruse
        cj=rj
    else
        ci=ri
        cj=cuse
    endif
    call disk(filen,tmdir,'nyquist ','~jw')
2    open(1,file=filen,form='binary',iostat=ioccheck)
    do 1 wi=1,noofw
        quotient(wi)=(-1,0)
        do 1 row=1,order
            do 1 col=1,order
                read(1,err=92)kw
                if ((row.eq.ci).and.(col.eq.cj)) then
                    if (cabs(kw).gt.1.e-38) then
                        quotient(wi)=quotient(wi)/kw
                    else
                        call clrbot
                        write(*,'(8x,a,lp,e13.7\)' )'WARNING: Division by zero at w= ',
+w(wi)
                        quotient(wi)=(0,0)

```

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```

                endif
            endif
            if ((row.eq.ri).and.(col.eq.rj))
+               quotient(wi)=quotient(wi)*kw
1          continue
            close(1)
            goto 10
92         call error('INA diagram file corrupted!  ')
            close(1)
10        return
            end

$include:'add.blk'
*****
*GETSCALE* GET SCALE
*****
* Descr:   The operator can enter scales to be used for the multiplier
*          diagram.
*
* Param:   Set by DIM.BLK
*
* Call.by: ROWOP,ROWMLT
* Calls:   ansisup,
*****

                subroutine getscale
                character*20 input
                logical      escape

$include:'dim.blk'

                call gotorc(4,20)
                write(*,'(a\)' )'Multiplier Diagram Options'
                call gotorc(6,15)
                write(*,'(a\)' )'Select real values for min. & maximum scale,'
                call gotorc(7,15)
                write(*,'(a\)' )'or enter zero for automatic scaling.'
                call gotorc(24,20)
                call invers
                write(*,'(a\)' )' Press <ESC> to exit options. '
                call normal
                call gotorc(11,20)
                write(*,'(a\)' )' Y-Axis Range: '
                write(*,'(1p,e10.3,a,1p,e10.3,\)' ) ylo,'>',yhi
1          call gotorc(9,20)
                write(*,'(a\)' )' X-Axis Range: '
                write(*,'(1p,e10.3,a,1p,e10.3,\)' ) xlo,'>',xhi
                call gotorc(9,35)
                call readln(input,10,escape)
                if (escape) goto 100
                if (input.ne.' ') then
                    read(input,333,err=1) xlo
                    goto 1
                endif
11         call gotorc(9,46)
                write(*,'(1p,e10.3\)' ) xhi
                call gotorc(9,46)
                call readln(input,10,escape)
                if (escape) goto 100
                if (input.ne.' ') then

```

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```

        read(input,333,err=11) xhi
        goto 11
    endif
2    call gotorc(11,20)
    write(*,'(a\)' )' Y-Axis Range: '
    write(*,'(lp,e10.3,a,lp,e10.3,\)' ) ylo,'>',yhi
    call gotorc(11,35)
    call readln(input,10,escape)
    if (.not.escape.and.input.ne.' ') then
        read(input,333,err=2) ylo
        goto 2
    endif
22   call gotorc(11,46)
    write(*,'(lp,e10.3\)' ) yhi
    call gotorc(11,46)
    call readln(input,10,escape)
    if (escape) goto 100
    if (input.ne.' ') then
        read(input,333,err=22) yhi
        goto 22
    endif
    goto 1
333  format(e10.3)
100  return
    end

```

\$include:'add.blk'

```

*****
* HELP * ONLINE HELP FASCILITY *
*****
* Descr: The file INACAD.HLP is displayed page by page on the screen. *
* * * * *
* Call.by: INADSN *
* Calls: ansisup. *
*****

```

subroutine help

```

    logical    dummy
    character*20 filen
    character  ch
    logical    kbhit
    integer    getch,ioccheck
    external   getch,kbhit

    call gotorc(7,1)
    filen='inacad.hlp'
    open(1,file=filen,form='binary',iostat=ioccheck)
    if (ioccheck.ne.0) then
        close(1)
        call error('Help file not found!      ')
        goto 99
    endif
1    read(1,err=99)ch
    if (kbhit()) then
        if (getch().eq.27) goto 99
    endif
    if (ch.eq.'{') then
        call invers
    elseif (ch.eq.'}') then

```

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```

        call normal
    elseif (ch.eq.'|') then
        if (getch().eq.27) goto 99
    elseif (ch.ne.10) then
        write(*,12,err=99)ch
    endif
    goto 1
12      format(al\ )
99      close(1)
100     return
end

$include:'add.blk'
*****
* INADSN * PERFORM INA DESIGN *
*****
* Descr:  Displays the top level menu and allows the user to jump to *
*         a specific part of the design. *
* * *
* Call.by: INACAD *
* Calls:  ansisup,GETCHC,DSNPAR,PRCPAR,NYQPAR,DIAGON *
*****

        subroutine inadsn

            integer  key,getch
            external getch
            logical  dsnc1r
            external dsnc1r

$INCLUDE:'MENU.BLK'
$include:'design.blk'

11      menunb=2
        call getchc(menunb,escape)
        if (escape) goto 10
        if (chcdf1(menunb).eq.5) then
            call shwpar(.false.)
            call clrbot
            write(*,'(8x,2a\ )')'WARNING: Old design parameters will ',
+           'be lost! Press <ESC> to abort...'
            if (getch().ne.27) then
                call gotorc(25,1)
                call clreol
                write(*,'(20x,a\ )')'Clearing Design...'
                call clrdsn
            endif
            goto 11
        elseif (chcdf1(menunb).eq.0) then
            call dos
        elseif (chcdf1(menunb).eq.1) then
            call help
        elseif (chcdf1(menunb).eq.2) then
            call shwpar(.true.)
        elseif (chcdf1(menunb).eq.3) then
            call prcpar
        elseif (chcdf1(menunb).eq.4) then
            call diagon
        endif
        goto 11

```

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```

10      if (gexist.or.kexist.or.lexist.or.fexist.or.wexist) then
          call gotorc(24,21)
          write(*,'(a1,a\)'')7,'Changes were made ! Quit anyway (y/n)?'
          if (getch().eq.121) goto 111
          depth=depth+1
          goto 11
        else
          call gotorc(24,21)
          write(*,'(a1,a\)'')7,'Quit INACAD (y/n)?'
          if (getch().eq.121) goto 111
          depth=depth+1
          goto 11
        endif
111     return
        end

        logical function dsnc1r()
        logical result

$include:'design.blk'

+      if ((gfilen.eq.' ').and.(kfilen.eq.' ').and.
          (lfilen.eq.' ').and.(ffilen.eq.' ')) then
          result=.true.
        else
          result=.false.
        endif
        dsnc1r=result
        return
        end

        subroutine clrdsn()
        integer i

$include:'design.blk'
$include:'rowop.blk'
$include:'desdta.blk'

        dsnnme=' '
        gfilen=' '
        gexist=.false.
        kfilen=' '
        kexist=.false.
        lfilen=' '
        lexist=.false.
        ffilen=' '
        fexist=.false.
        qexist=.false.
        ri=1
        rj=1
        ruse=1
        cuse=0
        rsord=1
        xdim=0
        ydim=0
        eps=1.e-8
        wint=10
        do 1 i=1,21
          rkd(i)=0.0
1         rkn(i)=0.0
        rkd(1)=1.

```

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```

    rkl=0.
    stp=10.
    do 3 i=1,1000
        gnum(i)=0.
        knum(i)=0.
        lnum(i)=0.
        fnum(i)=0.
        gden(i)=0.
        kden(i)=0.
        lden(i)=0.
3       fden(i)=0.
    do 4 i=1,100
        glag(i)=0.
        klag(i)=0.
        llag(i)=0.
4       flag(i)=0.
    ksaved=.false.
    lsaved=.false.
    return
end

$include:'add.blk'
*****
* INPUTTF* INPUT TRANSFER FUNCTION *
*****
* Descr:   The transfer function can be edited in this routine. *
* * * * *
* Param:   FNAME filename of definition. *
*          EXT filename extesion *
*          ORDER matrix order (nxn) *
*          SORDER maximum order of s used. *
*          MXSORD maximum allowed order of s. *
*          KNT,KDT,KLT contains matrix specifications. *
*          DIAGON logical true if only diagonal entries are allowed i.e. F(s)*
*          CHANGE logical true if changes were made to the data. *
* * * * *
* Call.by: EDITTF *
* Calls:   READLN,ansisup,COMMND,CLRCOM *
*****

    subroutine inputtf(fname,ext,order,sorder,kd,kl,
+diagon,change,mxsord)

    character*4 ext
    character*8 fname
    character*20 input
    character*32 filen
    logical      escape,change,diagon
    integer      sorder,order,i,it,jt,j,k,ij,kij,mxsord
    real         kd(*),kl(*),kn(*)
    real         num

    integer      getch,key
    external     getch

    i=1
    j=1
    change=.false.
2   call cls
    call invers

```

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```

    call gotorc(1,25)
    write(*,'(a,a,a\)' )' Editing: ',fname,ext
    call gotorc(1,67)
    call invers
    write(*,'(a\)' )' Mx Order:'
    write(*,'(i2.2\)' )order
    call gotorc(3,1)
    write(*,'(2a,2a1\)' )
+ ' Order of s      Numerator      Denominator      ',
+ 'Lag      ',13,10
    do 5 k=0,sorder
        write(*,'(i7,a,a1,a1\)' )k,'      ',13,10
5    continue
    call commnd
4    call invers
    call gotorc(1,1)
    if (diagon) then
        write(*,'(a,\)' )' Diag. Element:'
        i=j
    else
        write(*,'(a,\)' )' Element: '
    endif
    call normal
    write(*,'(a,i2,a,i2,3a1\)' )' (' ,i',' ',j,')',13,10
    ij=(i-1)*order+j
    kij=(ij-1)*(nxsord+1)
    do 25 k=1,sorder+1
        call gotorc(3+k,13)
        write(*,111)kn(kij+k)
        write(*,112)kd(kij+k)
        if (k.eq.1) write(*,113)kl(ij)
25    continue
22    call normal
    call gotorc(25,1)
    call clreol
    call gotorc(7,62+8)
    key=getch()
    if ((key.ne.13).and.(key.ne.27).and.(key.ne.110).and.(key.ne.100
+).and.(key.ne.108).and.(key.ne.112).and.(key.ne.106)) goto 22
    if (key.eq.13) then
        j=j+1
        if (j.gt.order) then
            j=1
            i=i+1
            if (i.gt.order) i=1
        endif
    endif
    if (key.eq.27)goto 7
    if (key.eq.110) then
        k=0
10    k=k+1
        call invers
        call gotorc(3+k,13)
        write(*,111)kn(kij+k)
        call gotorc(3+k,13)
        call readln(input,14,escape)
        call normal
        if (escape) goto 11
        if (input.eq.'      ') goto 8
        read(input,110,err=9) num
        kn(kij+k)=num

```

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```

      change=.true.
8      call gotorc(3+k,13)
      write(*,111)kn(kij+k)
      goto 16
9      write(*,'(a1\)' )7
      call gotorc(3+k,13)
      write(*,111)kn(kij+k)
      k=k-1
16     if (k.lt.sorder+1) goto 10
      key=100
11     call gotorc(3+k,13)
      write(*,111)kn(kij+k)
endif
if (key.eq.100) then
  k=0
12   k=k+1
      call invers
      call gotorc(3+k,13+18)
      write(*,111)kd(kij+k)
      call gotorc(3+k,13+18)
      call readln(input,14,escape)
      call normal
      if (escape) goto 14
      if (input.eq.'          ') goto 13
      read(input,110,err=15) num
      kd(kij+k)=num
      change=.true.
13   call gotorc(3+k,13+18)
      write(*,111)kd(kij+k)
      goto 17
15   write(*,'(a1\)' )7
      call gotorc(3+k,13+18)
      write(*,111)kd(kij+k)
      k=k-1
17   if (k.lt.sorder+1) goto 12
      key=108
14   call gotorc(3+k,13+18)
      write(*,111)kd(kij+k)
endif
if (key.eq.108) then
18   call invers
      call gotorc(4,13+18+16)
      write(*,111)kl(ij)
      call gotorc(4,13+18+16)
      call readln(input,14,escape)
      call normal
      if (escape) goto 19
      if (input.eq.'          ') goto 21
      read(input,110,err=20) num
      kl(ij)=num
      change=.true.
21   call gotorc(4,13+18+16)
      write(*,111)kl(ij)
      goto 19
20   write(*,'(a1\)' )7
      call gotorc(4,13+18+16)
      write(*,111)kl(ij)
      goto 18
19   call gotorc(4,13+18+16)
      write(*,111)kl(ij)
endif

```

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```

1      if (key.eq.112) then
        call clrbot
        write(*,'(15x,a,i2,a\)' )' Change Power to (0-',mxsord,') : '
        call readln(input,2,escape)
        call clrbot
        if (.not.(escape.or.(input.eq.'          '))) then
            read(input,100,err=1) neworder
            if ((neworder.ge.0).and.(neworder.le.mxsord)) then
                sorder=neworder
            endif
        endif
    endif
23     if (key.eq.106) then
        call clrbot
        write(*,'(20x,a,\)' )'JUMP to (row col):'
        call readln(input,5,escape)
        call normal
        if (escape.or.(input.eq.'          ')) goto 24
        call clrbot
        read(input,130,err=23)it,jt
        if((it.gt.order).or.(it.le.0).or.(jt.gt.order).or.(jt.le.0)
+ ) goto 23
            i=it
            j=jt
24     endif
        if (key.eq.106) goto 4
        if (key.eq.13) goto 4
        if (key.eq.112) goto 2
        goto 22
7      continue
        return
100     format(bn,i2)
110     format(bn,e13.6)
111     format(lp,e14.7,\)
112     format(lp,e18.7,\)
113     format(lp,e16.7,\)
130     format(bn,2i2)
        end

```

\$include:'add.blk'

```

*****
* KXCOL * MULTIPLY K(s) * COLUMN OF MATRIX *
* KXROW * MULTIPLY K(s) * ROW OF MATRIX *
*****
* Descr: Multiplies the specified row or column of a transfer matrix by a *
*         desired function. *
* * *
* Param: RKN,RKD,RKL - Function specifications *
*         KNUM,KDEN,KLAG - Matrix coefficients *
*         ORDER - Matrix order *
*         MXSORD - Highest power of s used. *
*         RUSE/CUSE - Row / column to be multiplied *
* * *
* Call.by: ROWOP *
* Calls: MLTROW,MLTCOL *
*****
+      subroutine kxrow(rkn,rkd,rkl,knum,
          kden,klag,order,mxsord,ruse)
          real rkn(*),rkd(*),rkl,knum(*)

```

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```

real      kden(*),klag(*),mltn(140),mltd(140),mlt1(10)
integer   i,j,order,mxsord,ruse

call mltrow(mltn,mltd,mlt1,rkn,rkd,rkl,knum,
+          kden,klag,order,mxsord,ruse)
do 1 i=1,order
  klag(i+order*(ruse-1))=mlt1(i)
  do 1 j=1,mxsord+1
    knum(j+(mxsord+1)*((i-1)+order*(ruse-1)))=
+    mltn(j+(mxsord+1)*(i-1))
    kden(j+(mxsord+1)*((i-1)+order*(ruse-1)))=
+    mltd(j+(mxsord+1)*(i-1))
1 continue
return
end

subroutine kxcol(rkn,rkd,rkl,lnum,
+             lden,llag,order,mxsord,cuse)
real      rkn(*),rkd(*),rkl,lnum(*)
real      lden(*),llag(*),mltn(140),mltd(140),mlt1(10)
integer   i,j,order,mxsord,cuse

call mltdcol(mltn,mltd,mlt1,rkn,rkd,rkl,lnum,
+           lden,llag,order,mxsord,cuse)
do 1 i=1,order
  llag(cuse+order*(i-1))=mlt1(i)
  do 1 j=1,mxsord+1
    lnum(j+(mxsord+1)*((cuse-1)+order*(i-1)))=
+    mltn(j+(mxsord+1)*(i-1))
    lden(j+(mxsord+1)*((cuse-1)+order*(i-1)))=
+    mltd(j+(mxsord+1)*(i-1))
1 continue
return
end

$include:'add.blk'
*****
* LOADTF * LOAD TRANSFER FUNCTION MATRIX *
*****
* Descr: Here the transfer function data is loaded from disk. *
*        NAME set to ' ' if file is in error. *
*        If the file was saved compacted, it is decompacted automatically. *
* *
* Param: DIR,NAME,EXT - filename specifications *
*        ARRn,d,l refers to parameter arrays *
*        ORDER is the matrix order (n*n) *
*        MXSORD is the maximum order of s of the saved file *
*        EXIST set false *
* *
* Call.by: EDITTF *
* Calls:  ansisup,DISK,READLN,(AUTOORD) *
*****

subroutine loadtf(dir,name,ext,arrn,arrrd,arrrl,
+             order,mxsord,exist)

character*4 ext
character*8 name
character*20 dir
character*32 filen

```

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```

character*30 message
real          arrn(*),arrd(*),arrl(*)
logical       exist
integer       key,order,mxtord,mxsord,tlorder,t2order,i,j
integer       getch,ioccheck
external      getch
logical       autoord
external      autoord

1      call disk(filn,dir,name,ext)
      open(1,file=file,iostat=ioccheck)
      read(1,'(3i2)',err=6)tlorder,t2order,mxtord
      mxtord=mxtord-1
      if (tlorder.ne.order) then
        if (autoord()) then
          order=tlorder
          mxsord=1000/order/order-1.5
          if (mxsord.gt.20) mxsord=20
        endif
      endif
      if((t2order.ne.order).or.(tlorder.ne.order).or.(mxsord.lt.
+      mxtord)) goto 10
      do 3 i=1,order
        do 3 j=1,order
          do 3 k=1,mxsord+1
            ijk=k+(mxsord+1)*((j-1)+order*(i-1))
            if (k.le.mxtord+1) then
              read(1,'(e13.7)',err=6)arrn(ijk)
            else
              arrn(ijk)=0.
            endif
3      continue
      do 4 i=1,order
        do 4 j=1,order
          do 4 k=1,mxsord+1
            ijk=k+(mxsord+1)*((j-1)+order*(i-1))
            if (k.le.mxtord+1) then
              read(1,'(e13.7)',err=6)arrd(ijk)
            else
              arrd(ijk)=0.
            endif
4      continue
      do 5 i=1,order*order
5      read(1,'(e13.7)',err=6)arrl(i)
      exist=.false.
      close(1,iostat=ioccheck)
      if (ioccheck.ne.0) goto 6
      goto 100

6      call error('File corrupted!          ')
      name=' '
      close(1)
      goto 100

10     write(message,'(a,i2.2)')'Order incorrect!  Set to : ',
+      tlorder
      call error(message)
      name=' '
100    return
      end

```

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```

c      Check if no parameters have been specified before
c      then update process order

      logical function autoord()
      logical result

$include:'design.blk'

      if ((kfilen.eq.' ').and.
+      (lfilen.eq.' ').and.(ffilen.eq.' ')) then
          result=.true.
      else
          result=.false.
      endif
      autoord=result
      return
      end

$include:'add.blk'
*****
* LOADWF * LOAD FRQUENCY SAMPLE POINTS *
*****
* Descr:  Here the frequency sample data is loaded from disk. *
* * * * *
* Param:  DIR,NAME,EXT - Filename specifications. *
*          EXIST - set to logical false *
*          ARR - refers to parameter array *
*          NOOFW - the number of samples *
* * * * *
* Call.by: EDITWF *
* Calls:  ERROR *
*****
      subroutine loadwf(dir,name,ext,arr,noofw,exist)

      character*8 name
      character*20 dir,input
      character*4 ext
      real arr(*)
      logical exist,found
      character*32 filen
      integer getch,key,noofw,ioccheck,i,j
      external getch

      call disk(filen,dir,name,ext)
1      open(1,file=filen,iostat=ioccheck)
      read(1,'(i3)',err=2)noofw
      do 3 i=1,noofw
3      read(1,'(e13.7)',err=2)arr(i)
      close(1)
      exist=.false.
      goto 100

2      call error('Frequency file corrupted! ')
      noofw=1
      arr(1)=1
      close(1)
100     return
      end

```

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```

$include: 'add.blk'
*****
* MATMLT * MATRIX MULTIPLICATION
*****
* Descr:   This routine multiplies two complex matrices.
*
* Param:   MXC = MXA x MXB
*          ORDER is the matrix order nxn.
*
* Call.by: CALCQI
* Calls:   none.
*****

      subroutine matmlt(mxa, mxb, mxc, order)

      integer    order, dx, ax, bx, offset
      complex    mxa(*), mxb(*), mxc(*)

c      use double precision in calculations
      complex*16 mxd(100)

      do 1 i=1, order
        offset=(i-1)*order
        do 1 j=1, order
          dx=j+offset
          mxd(dx)=(0,0)
          do 1 k=1, order
1            mxd(dx)=mxd(dx)+mxa(k+offset)*mxb(j+(k-1)*order)
          do 2 i=1, order*order
2            mxc(i)=mxd(i)
          return
        end

$include: 'add.blk'
*****
* MNURST * MENU RESET
*****
* Descr:   Initialises the menu data with the necessary data.
*
* Call.by: INACAD
* Calls:   ansisup
*****

      function ip(i)
c      Used as a counter to fill menu items
      integer i

      i=i+1
      ip=i
      return
      end

      subroutine mnurst

      integer i

$INCLUDE: 'MENU.BLK'

```

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```

i=0
top(1)=1
top(2)=20
oldmnu(1)=1
depth=1
mnuinf(1,1)=i+1
choice(ip(i))=' INA DESIGN PROGRAM '
messge(i)=' '
mnuinf(2,1)=i
chcdf1(1)=0
mnuinf(1,2)=i+1
choice(ip(i))=' DOS Command '
messge(i)=' Execute a DOS Command. '
choice(ip(i))=' Help '
messge(i)=' Get help on updated information. '
choice(ip(i))=' Design Status '
messge(i)=' Show design setup & enter design name. '
choice(ip(i))=' Process Parameters'
messge(i)=' Select process paramters. '
choice(ip(i))=' Diagonalisation '
messge(i)=' Diagonalise Process Response. '
choice(ip(i))=' Clear design '
messge(i)=' Clear design parameters. '
choice(ip(i))=' Quit Program '
messge(i)=' Return To DOS . '
mnuinf(2,2)=i
chcdf1(2)=3
mnuinf(1,3)=i+1
choice(ip(i))=' File Directories '
messge(i)=' Temporary & parameter file directories.'
choice(ip(i))=' Process Order '
messge(i)=' Change order of the process matrices. '
choice(ip(i))=' Frequency Range '
messge(i)=' Select frequency sample range. '
choice(ip(i))=' Plant Matrix G(s) '
messge(i)=' Edit/Load/Save/Print plant matrix G(s).'
choice(ip(i))=' Controller Mx K(s) '
messge(i)=' Edit/Load/Save/Print matrix K(s). '
choice(ip(i))=' Controller Mx L(s) '
messge(i)=' Edit/Load/Save/Print matrix L(s). '
choice(ip(i))=' Feedback Mx F(s) '
messge(i)=' Edit/Load/Save/Print feedback mx F(s). '
choice(ip(i))=' Return '
messge(i)=' Return To TOP LEVEL Menu.'
mnuinf(2,3)=i
chcdf1(3)=3
mnuinf(1,4)=i+1
choice(ip(i))=' Nyquist Setup '
messge(i)=' Select Nyquist Diagram options. '
choice(ip(i))=' Plot Nyquist '
messge(i)=' Show resulting Nyquist Diagram. '
choice(ip(i))=' Row/Col. operation '
messge(i)=' Perform a row or column operation. '
choice(ip(i))=' Swop Rows /Columns '
messge(i)=' Interchange rows/columns of Q(s). '
choice(ip(i))=' Multiply Row/Col. '
messge(i)=' Multiply a row or column with function.'
choice(ip(i))=' Undo Operation '
messge(i)=' Undo alteration of K(s) or L(s). '
choice(ip(i))=' Print Response '
messge(i)=' Print frequency response of process. '

```

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```

choice(ip(i))=' Return '
messge(i)=' Return To TOP LEVEL Menu. '
mnuinf(2,4)=i
chcdf1(4)=1
mnuinf(1,5)=i+1
choice(ip(i))=' Load Transfer Fn '
messge(i)=' Load transfer function file from disk. '
choice(ip(i))=' Edit Transfer Fn '
messge(i)=' Create or edit transfer function. '
choice(ip(i))=' Save Transfer Fn '
messge(i)=' Save transfer function file to disk. '
choice(ip(i))=' Print Transfer Fn '
messge(i)=' Print Coefficient Matrix.'
choice(ip(i))=' Remove Parameter '
messge(i)=' Delete parameter matrix from Design. '
choice(ip(i))=' Return '
messge(i)=' Return To PROCESS PARAMETERS Menu. '
mnuinf(2,5)=i
chcdf1(5)=0
mnuinf(1,6)=i+1
choice(ip(i))=' Load Frequency Data'
messge(i)=' Load frequency range from Disk. '
choice(ip(i))=' Edit Frequency Data'
messge(i)=' Create or change frequency range. '
choice(ip(i))=' Save Frequency Data'
messge(i)=' Save frequency range to Disk. '
choice(ip(i))=' Return '
messge(i)=' Return To PROCESS PARAMETERS Menu. '
mnuinf(2,6)=i
chcdf1(6)=0
mnuinf(1,7)=i+1
choice(ip(i))=' Operation Options '
messge(i)=' Select element to ellim. & row to use. '
choice(ip(i))=' Edit Multiplier '
messge(i)=' Enter multiplication factor. '
choice(ip(i))=' Optimise Multiplier'
messge(i)=' Do optimisation of multiplier function.'
choice(ip(i))=' Plot Multiplier '
messge(i)=' Plot multiplication factor & function. '
choice(ip(i))=' Adjust Scale '
messge(i)=' Select scale for plot of multiplier. '
choice(ip(i))=' Perform Operation '
messge(i)=' Update altered K(s) or L(s) matrix. '
choice(ip(i))=' Print Operation '
messge(i)=' Print operation performed on Printer. '
choice(ip(i))=' Print Plot '
messge(i)=' Print plotted points on Printer. '
choice(ip(i))=' Return '
messge(i)=' Return To PERFORM INA DESIGN Menu. '
mnuinf(2,7)=i
chcdf1(7)=0
mnuinf(1,8)=i+1
mnuinf(2,8)=i
chcdf1(8)=0
mnuinf(1,9)=i+1
choice(ip(i))=' Operation Options '
messge(i)=' Select Row or Column to multiply. '
choice(ip(i))=' Edit Multiplier '
messge(i)=' Edit multiplication funtion. '
choice(ip(i))=' Optimise Multiplier'
messge(i)=' Do optimisation of multiplier function.'

```

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```

choice(ip(i))=' Plot Multiplier      '
messge(i)=' Plot element inverse & multiplier.      '
choice(ip(i))=' Adjust Scale          '
messge(i)=' Select scale for plot of multiplier.      '
choice(ip(i))=' Perform Operation      '
messge(i)=' Update altered K(s) or L(s) matrix.      '
choice(ip(i))=' Print Operation        '
messge(i)=' Print operation on printer.      '
choice(ip(i))=' Print Plot            '
messge(i)=' Print plotted points on Printer.      '
choice(ip(i))=' Return                '
messge(i)=' Return To PERFORM INA DESIGN Menu.      '
mnuinf(2,9)=i
chcdf1(9)=0
mnuinf(1,10)=i+1
choice(ip(i))=' Swop Rows              '
messge(i)=' Select rows to interchange.      '
choice(ip(i))=' Swop Columns          '
messge(i)=' Select columns to interchange.      '
choice(ip(i))=' Perform Operation      '
messge(i)=' Update altered K(s) or L(s) matrix.      '
choice(ip(i))=' Print Operation        '
messge(i)=' Print operation on printer.      '
choice(ip(i))=' Return                '
messge(i)=' Return To PERFORM INA DESIGN Menu.      '
mnuinf(2,10)=i
chcdf1(10)=0
return
end

```

\$include:'add.blk'

```

*****
* NELM      * NONLINEAR PARAMETER ADJUSTMENT METHOD      *
*****
* Descr:    This routine performs a nonlinear parameter adjustment      *
*           of a function to reduce the sum of error^2.      *
*           *                                           *
*           *                                           *
* Param:    N - Number of parameters to adjust (max.21)      *
*           X(N) - Parameters to adjust.      *
*           F   - Sum of square of error      *
*           EPS - Convergence crriterion specifications:      *
*           end IF SQR((F(i)-F(lowest))/(N+1)) < EPS*N      *
*           P(N*(N+2)) - temporary storage      *
*           FP(N+1)  -      "      *
*           XS(N)    -      "      *
*           H(N)     - Step size corresponding to X(N)      *
*           IX      - set to 0 when routine first entered      *
*           *                                           *
* Call.by:   *                                           *
* Calls:     CALCF   - Function calculating Sum of error squared.      *
*****

```

```

subroutine nelm(ix,x,h,n,f,eps,err)

```

```

real      x(*),f,fs,eps,p(483),fp(22),xs(21),h(*)
integer   ix,i,j,k,kl,nn,n,n1,np,xn,ih,is,k0,il,key
logical   kbhit,err
integer   getch
external  kbhit,getch

```

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```

err=.false.
call saverc
n1=n+1
np=n*(n+2)
nn=n*(n+1)
call calcf(n,x,f)
fp(1)=f
if (ix.eq.0) then
  do 1 i=1,n
    k=i
    do 1 j=1,n1
      p(k)=x(i)
      if (i.eq.j-1) p(k)=x(i)+h(i)
1      k=k+n
    endif
2      k=1+n
    do 3 i=2,n1
      do 4 j=1,n
        x(j)=p(k)
        k=k+1
4      continue
      call calcf(n,x,f)
      fp(i)=f
3      continue
303      if (fp(1)-fp(2)) 303,303,5
      ih=2
      il=1
      go to 6
5      ih=1
      il=2
6      do 7 i=3,n1
      if (fp(i)-fp(ih)) 304,304,8
304      if (fp(i)-fp(il)) 305,7,7
305      il=i
      go to 7
8      ih=i
7      continue
      xn=n
50      k1=nn
      do 9 i=1,n
        k=i
        s=0.0
        do 10 j=1,n1
          if (j.ne.ih) s=s+p(k)
          k=k+n
10      continue
          k1=k1+1
          p(k1)=s/xn
9      continue
      k=nn+1
      do 11 i=1,n
        x(i)=p(k)
11      k=k+1
      call calcf(n,x,f0)
      s=0.0
      do 12 i=1,n1
12      s=s+(fp(1)-f0)**2
          s=s/xn
307      if (sqrt(s)-eps) 100,100,307
          if (kbhit()) goto 100

```

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```

call loadrc
write(*,'(1p,e14.6,a,1p,e14.6\)' ) fp(il),'      ',sqrt(s)
if (ih-1) 308,13,308
308  is=1
      go to 14
13   is=2
14   continue
      do 15 i=1,n1
          if (i.ne.ih) then
              if (fp(i).lt.fp(is)) is=i
          endif
15   continue
c    REFLECTION
      k=(ih-1)*n+1
      k0=nn+1
      do 16 i=1,n
          x(i)=2.*p(k0)-p(k)
          k=k+1
          k0=k0+1
16   continue
      k=k-n
      call calcf(n,x,f)
c    EXPANSION
      if (f-fp(il))311,20,20
311  k0=nn+1
      do 17 i=1,n
          xs(i)=2.*x(i)-p(k0)
17   k0=k0+1
      call calcf(n,xs,fs)
      if (fs-fp(il))312,18,18
312  do 19 i=1,n
          p(k)=xs(i)
19   k=k+1
      fp(ih)=fs
      il=ih
      ih=is
      go to 30
18   il=ih
      ih=is
      fp(il)=f
21   do 22 i=1,n
          p(k)=x(i)
22   k=k+1
      go to 30
20   if(f-fp(is))313,23,23
313  fp(ih)=f
      ih=is
      go to 21
23   if(f-fp(ih))314,25,25
314  do 24 i=1,n
          p(k)=x(i)
24   k=k+1
      fp(ih)=f
c    CONTRACT
      k=k-n
25   k0=nn+1
      do 26 i=1,n
          xs(i)=.5*(p(k)+p(k0))
          k=k+1
26   k0=k0+1
      k=k-n

```

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```

    call calcf(n,xs,fs)
    if (fs-fp(ih))315,40,40
315  do 27 i=1,n
        p(k)=xs(i)
27    k=k+1
        fp(ih)=fs
        if(fp(1)-fp(2)) 316,316,28
316  ih=2
        go to 29
28    ih=1
29    continue
        do 31 i=3,n1
            if (fp(i).gt.fp(ih)) ih=i
31    continue
30    go to 50
40    fp(1)=fp(i1)
        if (i1-1) 318,43,318
318  k=(i1-1)*n
        do 41 i=1,n
            k=k+1
            x(i)=p(k)
            p(k)=p(i)
41    p(i)=x(i)
        i1=1
43    k=n
        do 42 i=2,n1
            do 42 j=1,n
                k=k+1
42    p(k)=.5*(p(k)+p(j))
        go to 2
100  k=(i1-1)*n
        do 101 i=1,n
            k=k+1
101  x(i)=p(k)
        f=fp(i1)
222  if (kbhit()) then
            call error('Optimisation ABORTED! ' )
            err=.true.
        endif
        return
    end

c    Calculate resulting sum of error^2

    subroutine calcf(n,x,errsum)
    integer      n
    real         x(*),errsum
    complex      result
    integer      wi
    real         pi
    complex      kw,nw,dw,lw

$include:'desdta.blk'
$include:'rowop.blk'

    errsum=0.
    pi=3.1415926536
    do 67 wi=1,noofw,wint
        call calcpw(nw,x(1),rsord,w(wi))
        call calcpw(dw,x(rsord+2),rsord,w(wi))

```

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```

        if (cabs(dw).le.1.e-8) then
            result=(0,0)
        else
            if (mod(n,2).ne.0) then
                lw=cplx(0.,amod( x(n)*w(wi) , 2 * pi ))
                result=nw/dw*cexp(lw)
            else
                result=nw/dw
            endif
        endif
        errsum=errsum+cabs(quotient(wi)-result)**2
67      continue
69      return
      end

$include:'add.blk'
*****
* NYQSTP * NYQUIST DIAGRAM SETUP *
*****
* Descr:   In this subroutine the Nyquist Diagram Parameters can be changed. *
*
* Call.by: DIAGON *
* Calls:   ansisup, *
*****

      subroutine nyqstp

          logical      change,escape
          character*20 input
          integer      i,j,key,getch,pos
          external     getch

$include:'design.blk'
$include:'desdta.blk'

          pos=1
          call normal
          call gotorc(4,17)
          write(*,'(a\)' )'Press <RTN> to move cursor to desired option.'
          call gotorc(25,17)
          write(*,'(a,\)' )'Press <ESC> to exit Nyquist options menu.'
1      call normal
          call gotorc(6,20)
          if (single) then
              write(*,'(a\)' )'ELEMENT(s) to display on plot: '
              write(*,'(a,i2.2,a,i2.2,a,\)' )'(' ,si,',',sj,')'
          else
              write(*,'(a\)' )'ELEMENT(s) to display on plot: ( ALL )'
          endif
          call gotorc(9,20)
          write(*,'(a,a1\)' )'SCALE plot to axis range of :',241
          write(*,'(lp,e14.7\)' ) inadim
          call gotorc(12,20)
          write(*,'(a\)' )'TYPE of Nyquist Array Diagram '
          if (qinvrt) call invers
          write(*,'(a,\)' )' INVERSE '
          call normal
          write(*,'(a\)' )' or '
          if (.not.qinvrt) call invers
          write(*,'(a,\)' )' DIRECT '

```

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```

    call normal
    call gotorc(15,20)
write(*,'(a,i3\)' )'Number of Gershgorin circles :',abs(gerint)
    call gotorc(18,20)
write(*,'(a,i3\)' )'Number of Ostrowski circles :',abs(ostint)
    call gotorc(21,20)
    write(*,'(a\)' ) 'DOMINANCE use to plot circles '
    if (gerint+ostint.lt.0) call invers
    write(*,'(a,\)' )' COLUMN '
    call normal
    write(*,'(a\)' )' or '
    if (gerint+ostint.ge.0) call invers
    write(*,'(a,\)' )' ROW '
    call inverse
    if (pos.eq.1) then
        call gotorc(7,20)
        write(*,'(2a,\)' )' Select element as ''row,column'',
+         ' or enter 0 for ALL.'
2         call gotorc(6,52)
        call normal
        call readln(input,5,escape)
        if (escape) goto 100
        if (input.ne.' ') then
122         read(input,122,err=1) i,j
            format(bn,2i2)
+         if ((i.ge.0).and.(i.le.order).and.(j.ge.0).and.(j.le.order))
            then
                si=i
                sj=j
                if ((si.ne.0).and.(sj.ne.0)) then
                    single=.true.
                else
                    single=.false.
                endif
                qexist=.false.
            else
                write(*,'(al\)' )?
                goto 2
            endif
        endif
        pos=2
        call gotorc(7,20)
        call normal
        call clreol
        call inverse
    endif
    if (pos.eq.2) then
        call gotorc(10,20)
        write(*,'(2a,\)' )' Select maximum axis range value,',
+ 'or 0 for automatic scaling.'
3         call gotorc(9,51)
        call saverc
        call normal
        call readln(input,20,escape)
        if (escape) goto 100
        if (input.ne.' ') then
            read(input,222,err=3) inadim
            inadim=abs(inadim)
            call loadrc
            write(*,'(1p,e14.7\)' ) inadim
            qexist=.false.

```

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```

222         endif
           format(e13.7e2)
           pos=3
           call gotorc(10,20)
           call normal
           call clreol
           call inverse
         endif
         if (pos.eq.3) then
           call gotorc(13,23)
           write(*,'(a,\)')' Press <SPACE BAR> to change type.'
4           call gotorc(12,50)
           call saverc
           key=getch()
           if (key.eq.27) goto 100
           if (key.eq.32) then
             qinvrt=.not.qinvrt
             qexist=.false.
             call loadrc
             call normal
             if (qinvrt) call invers
             write(*,'(a,\)')' INVERSE '
             call normal
             write(*,'(a\)\)')' or '
             if (.not.qinvrt) call invers
             write(*,'(a,\)')' DIRECT '
             call normal
           endif
           if (key.ne.13) goto 4
           pos=4
           call gotorc(13,20)
           call normal
           call clreol
           call inverse
         endif
         if (pos.eq.4) then
           call gotorc(16,23)
           write(*,'(a,i3,a\)\)')' Select amount from 0 to ',noofw,'.'
5           call gotorc(15,50)
           call normal
           call readln(input,3,escape)
           if (escape) goto 100
           if (input.ne.' ') then
             read(input,444,err=5) i
444           format(bn,i3)
             if ((i.lt.0).or.(i.gt.noofw)) then
               write(*,'(a1\)\)')7
               goto 5
             endif
             if ((ostint.lt.0).or.(gerint.lt.0)) then
               gerint=-i
             else
               gerint=i
             endif
             qexist=.false.
           endif
           pos=5
           call gotorc(16,20)
           call normal
           call clreol
           call inverse

```

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```

endif
if (pos.eq.5) then
  call gotorc(19,23)
  write(*,'(a,i3,a)') ' Select amount from 0 to ',noofw,'.'
6   call gotorc(18,50)
  call normal
  call readln(input,3,escape)
  if (escape) goto 100
  if (input.ne.' ') then
    read(input,444,err=6) i
    if ((i.lt.0).or.(i.gt.noofw)) then
      write(*,'(a\)\')7
      goto 6
    endif
    if ((ostint.lt.0).or.(gerint.lt.0)) then
      ostint=-i
    else
      ostint=i
    endif
    qexist=.false.
  endif
  pos=6
  call gotorc(19,20)
  call normal
  call clreol
  call inverse
endif
if (pos.eq.6) then
  if (ostint+gerint.eq.0) then
    goto 8
  endif
  call gotorc(22,23)
  write(*,'(a,\)\') ' Press <SPACE BAR> to change dominance.'
7   call gotorc(21,50)
  call saverc
  key=getch()
  if (key.eq.27) goto 100
  if (key.eq.32) then
    ostint=-ostint
    gerint=-gerint
    qexist=.false.
    call loadrc
    call normal
    if (gerint+ostint.lt.0) call invers
    write(*,'(a,\)\') ' COLUMN '
    call normal
    write(*,'(a\)\') ' or '
    if (gerint+ostint.ge.0) call invers
    write(*,'(a,\)\') ' ROW '
    call normal
  endif
  if (key.ne.13) goto 7
8   pos=1
  call gotorc(22,20)
  call normal
  call clreol
endif
goto 1
100 return
end

```

APPENDIX D SOFTWARE REFERENCE

```

$include:'add.blk'
*****
* OPTIM * OPTIMISATION *
*****
* Descr: Here the options for the optimisation routine are selected. *
* * *
* Call.by: ROWOP *
* Calls: ansisup,PLTMLT,NELM *
*****

      subroutine optim

      real      rkd2(10),rkl2,rkn2(10)
      real      x(21),stpn(21),sumerr
      logical   escape,change,err
      integer   i,getch,key
      character*20 input
      external  getch

$include:'rowop.blk'
$include:'desdta.blk'

123      do 1 i=1,10
          rkd2(i)=rkd(i)
1          rkn2(i)=rkn(i)
          rkl2=rkl
          call gotorc(4,20)
          write(*,'(a)')'Nonlinear Parameter Adjustment Procedure'
          call gotorc(6,15)
          write(*,'(2a)')'This routine attempts to optimise ',
+ 'the entered function.'
          call gotorc(9,15)
          write(*,'(2a)')'Enter the starting stepsize ',
+ 'to optimise all coefficients'
          call gotorc(10,15)
          write(*,'(a)')'as a percentage of its initial value.'
          call gotorc(11,15)
          write(*,'(a)')' (N.B. Coefficients = 0 will remain 0.)'
          call gotorc(25,20)
          write(*,'(a)')'Press <ESC> to exit optimisation.'
39      call gotorc(13,15)
          write(*,'(a)')' Stepsize : '
          call saverc
          write(*,'(f6.2,a)')stp,'% '
          call loadrc
          call readln(input,6,escape)
          if (escape) goto 100
          if (input.eq.' ') goto 40
          read(input,331,err=39) stp
          if (stp.eq.0) then
              write(*,'(a1)')7
          endif
          goto 39
331      format(bn,e6.2)
40      call gotorc(15,15)
          write(*,'(a,i3,a)')'Select frequency sample interval from 1-',
+ noofw,','
          if (wint.gt.noofw) wint=noofw
          if (wint.eq.0) wint=1
          call gotorc(16,15)

```

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```

write(*,'(a\)' )' Interval: ',
call saverc
write(*,'(i3\)' )wint
call loadrc
call readln(input,3,escape)
if (escape) goto 100
if (input.eq.' ') goto 41
read(input,333,err=40) wint
if ((wint.le.0).or.(wint.gt.noofw)) then
  write(*,'(a1\)' )7
endif
goto 40
333  format(bn,i3)
41   call gotorc(18,15)
write(*,'(a\)' )'Enter Convergence Epsilon : '
call saverc
write(*,'(1p,e13.6\)' )eps
call loadrc
call readln(input,13,escape)
if (escape) goto 100
if (input.eq.' ') goto 441
read(input,332,err=40) eps
if (eps.lt.0) then
  write(*,'(a1,\)' )7
  eps=0.
endif
goto 41
332  format(bn,f13.6)
441  call gotorc(20,20)
write(*,'(2a1,3a\)' )' ',228,' Error**2  ', ' ',
+' Epsilon '
call gotorc(25,20)
call invers
write(*,'(a\)' )' Press key to START optimization. '
if (getch().eq.27) goto 100
call clrbot
write(*,'(2a\)' )' Press any ',
+' key to stop optimisation . . . '
call normal
33   do 3 i=1,rsord+1
      x(i)=rkn(i)
      x(i+rsord+1)=rkd(i)
      stpn(i)=stp*rkn(i)/100.
3     stpn(i+rsord+1)=stp*rkd(i)/100.
change=.true.
n=2*rsord+2
if (rkl.ne.0) then
  n=n+1
  x(n)=rkl
  stpn(n)=stp*rkl/100.
endif
ct=0
call gotorc(21,18)
call nelm(ct,x,stpn,n,sumerr,eps,err)
if (err) then
  call gotorc(20,1)
  call clreol
  call gotorc(21,1)
  call clreol
endif
do 4 i=1,rsord+1

```

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```

      rkn(i)=x(i)
4      rkd(i)=x(i+rsord+1)
      if (mod(n,2).ne.0) rkl=x(n)
      call invers
      call gotorc(23,20)
write(*,'(a1,a1p,e15.6,a\)' )7,' Sum of Errors**2 = ',sumerr,' '
      call normal
      call gotorc(25,1)
      call clreol
      call gotorc(25,20)
      call invers
      write(*,'(a\)' )' Press key for PLOT... '
      call normal
      if (getch().eq.27) goto 99
      call pltmlt
      call cls
      call invers
      call gotorc(15,15)
      write(*,'(a\)' )' Press key to accept ALTERED Function,'
      call gotorc(16,15)
      write(*,'(a\)' )' or press <ESC> to UNDO optimisation. '
      call normal
      if (getch().ne.27) goto 100
99      do 2 i=1,10
          rkn(i)=rkn2(i)
2          rkd(i)=rkd2(i)
          rkl=rkl2
100      return
      end

```

```

$include:'add.blk'
*****
* PLTAX2 * PLOT AXIS FOR MLT DIAGRAM *
*****
* Descr: Here the axis for the ina plot is drawn. *
* * *
* Call.by: PLTMLT *
* Calls: Hercules Support *
*****

```

```

      subroutine pltax2

```

```

      integer i,j,k,order,m
      real delatx,delay,x,y,dely,delx,mlt,xdim,ydim

```

```

$include:'dim.blk'

```

```

      order=1
      call clrscr
      call putpt(0,0)
      call dline(521,0)
      call dline(521,347)
      call dline(0,347)
      call dline(0,0)
      deltax=0.9*521./order/2.
      delx=521./order/20.
      delay=0.9*347./order/2.
      dely=347./order/20.
      ydiv=347./2.
      xdiv=521./2.

```

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```

xdim=xhi-xlo
ydim=yhi-ylo
x=-521.*xlo/xdim
y=347+347.*ylo/ydim
call circ(nint(x),nint(y),3)
if (x.gt.521) x=521
if (y.gt.347) y=347
if (x.lt.0) x=0
if (y.lt.0) y=0
call putpt(0,nint(y))
call dline(521,nint(y))
call putpt(nint(x),0)
call dline(nint(x),347)
do 1 k=1,20
  if (mod(k,5).eq.0) then
    mlt=2.
  else
    mlt=5.
  endif
  call putpt(nint(x+k*delx),nint(y+dely/mlt))
  call dline(nint(x+k*delx),nint(y-dely/mlt))
  call putpt(nint(x-k*delx),nint(y+dely/mlt))
  call dline(nint(x-k*delx),nint(y-dely/mlt))
  call putpt(nint(x+delx/mlt),nint(y+k*dely))
  call dline(nint(x-delx/mlt),nint(y+k*dely))
  call putpt(nint(x+delx/mlt),nint(y-k*dely))
  call dline(nint(x-delx/mlt),nint(y-k*dely))
1
return
end

$include:'add.blk'
*****
* PLTAXS * PLOT AXIS FOR INA DIAGRAM *
*****
* Descr: Here the axis for the ina plot is drawn. *
* * *
* Param. : ORDER - order of diagram i.e. nxn set of axis *
* * *
* Call.by: PLTINA *
* Calls: Hercules Support *
*****

subroutine pltaxs(order)

integer i,j,k,order
real delatx,deltay,x,y,dely,delx,mlt

call clrscr
call putpt(0,0)
call dline(521,0)
call dline(521,347)
call dline(0,347)
call dline(0,0)
deltax=0.9*521./order/2.
delx=521./order/20.
deltay=0.9*347./order/2.
dely=347./order/20.
do 1 i=1,order
  y=347.*(2*i-1)/order/2.
  do 1 j=1,order

```

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```

      x=521.*(2*j-1)/order/2.
c      call putpt(nint(x-deltax),nint(y))
c      call dline(nint(x+deltax),nint(y))
c      call putpt(nint(x),nint(y-deltay))
c      call dline(nint(x),nint(y+deltay))
      do 1 k=1,9
        if (k.eq.5) then
          mlt=2.
        else
          mlt=5.
        endif
        call putpt(nint(x+k*delx),nint(y+dely/mlt))
        call dline(nint(x+k*delx),nint(y-dely/mlt))
        call putpt(nint(x-k*delx),nint(y+dely/mlt))
        call dline(nint(x-k*delx),nint(y-dely/mlt))
        call putpt(nint(x+delx/mlt),nint(y+k*dely))
        call dline(nint(x-delx/mlt),nint(y+k*dely))
        call putpt(nint(x+delx/mlt),nint(y-k*dely))
        call dline(nint(x-delx/mlt),nint(y-k*dely))
1      return
      end

$include:'add.blk'
*****
* PLTGER * PLOT GERSHGORIN AND OSTROWSKI CIRCLES *
*****
* Descr:   The Gershgorin and Ostrowski circles are plotted *
*          at a single frequency point. *
* * * * *
* Param:   QW - Array containing response. *
*          SINGLE - Set true if only one set of axis is used. *
*          SI,SJ - Index of single element to plot. *
*          ORDER - INA diagram order. *
*          DIM - Extents of axis *
*          GERINT,OSTINT - Determine row or column dominance. *
*          FHANDLE - File handle of feedback matrix. *
*          ERROR - Flag indicating file access error. *
* * * * *
* Call.by: PLTINA.
*
* Calls:   ansisup,hercules support,DCIRC.
*****

      subroutine pltger(qw,single,si,sj,order,
+          dim,gerint,ostint,fhandle,error)

      complex qw(*),f(10),dummy
      real*8 div
      real dim
      integer si,sj,order,gerint,ostint,fhandle,i,j,dom,index,indexs
      logical error,single
      real*8 gerrad(10),ostrad(10),max

      indexs=sj+(si-1)*order
      dom=gerint
      if (dom.eq.0) dom=ostint
      do 1 i=1,order
        gerrad(i)=0.
        do 1 j=1,order

```

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```

        if (dom.gt.0) then
        if (j.ne.i) gerrad(i)=gerrad(i)+cabs(qw(j+(i-1)*order))
        else
        if (j.ne.i) gerrad(i)=gerrad(i)+cabs(qw(i+(j-1)*order))
        endif
1      continue
        if (ostint.ne.0) then
        if (fhandle.ne.0) then
        do 2 i=1,order
        do 2 j=1,order
        if (i.eq.j) then
        read(fhandle,err=99)f(i)
        else
        read(fhandle,err=99)dummy
        endif
2      continue
        else
        do 3 i=1,order
3      f(i)=(1,0)
        endif
        do 4 i=1,order
        max=0
        do 5 j=1,order
        if (i.ne.j) then
        div=gerrad(j)/cabs(f(j)+qw(j+(j-1)*order))
c      div=gerrad(j)/cabs(qw(j+(j-1)*order))
        if (max.lt.div) max=div
        endif
5      continue
4      ostrad(i)=gerrad(i)*max
        do 7 i=1,order
        index=i+(i-1)*order
        if (single) then
        if (index.eq.indexs)
+      call dcirc(ostrad(i),1,1,qw(index),1,dim)
        else
        call dcirc(ostrad(i),i,i,qw(index),order,dim)
        endif
7      continue
        endif
        if (gerint.ne.0) then
        do 6 i=1,order
        index=i+(i-1)*order
        if (single) then
        if (index.eq.indexs)
+      call dcirc(gerrad(i),1,1,qw(index),1,dim)
        else
        call dcirc(gerrad(i),i,i,qw(index),order,dim)
        endif
6      continue
        endif
        goto 100
99     error=.true.
100    return
        end

```

c Draw circle of radius RAD at I,J with center at QW
subroutine dcirc(rad,i,j,qw,order,dim)

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```

integer    i,j,order,radius
real       x,y,dim,xdiv,ydiv,yp,yp
real*8     rad
complex    qw

x=real(qw)
y=aimag(qw)
radius=nint(rad*521./order/dim/2.)
if ((abs(x).le.dim).and.(abs(y).le.dim)
+   .and.(radius.gt.1)) then
    xdiv=521./order/2.*(2*j-1)
    ydiv=347./order/2.*(2*i-1)
    xp=xdiv+521.*x/order/2./dim
    yp=ydiv-347.*y/order/2./dim
    if (rad.le.2.*dim) then
        call circ(nint(xp),nint(yp),radius)
    else
        call putpt(nint(xp-6),nint(yp))
        call dline(nint(xp+6),nint(yp))
        call putpt(nint(xp),nint(yp-4))
        call dline(nint(xp),nint(yp+4))
    endif
endif
return
end

$include:'add.blk'
*****
* PLTHE2 * PLOT HEADING FOR MULTIPLIER DIAGRAM *
*****
* Descr:  Adds information to the Multiplier plot. *
* * *
* Call.by: PLTMLT. *
* Calls:  Hercules Support *
*****

subroutine plthe2(start)

character*20 str
character*8 dfilen
logical start

$include:'design.blk'
$include:'desdta.blk'
$include:'rowop.blk'
$include:'dim.blk'

if (start) then
    call gmode
    call clrscr
    call level(1)
    call pltax2
else
    call level(0)
    call blkfil(522,346,197,346)
    call level(1)
    call putpt(522,0)
    call dline(719,0)
    call dline(719,347)
    call dline(522,347)

```

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```

call dline(522,0)
call putpt(1,1)
call dline(1,346)
call dline(718,346)
call dline(718,1)
call dline(1,1)
call textf(522+9,14,20,' MULTIPLIER DIAGRAM ')
call textf(522+9,14*2,20,'-----')
call textf(522+9,14*3,20,d$nnme)
call textf(522+9,14*4,20,' G(s) : ')
call textf(522+9*10,14*4,8,g$filen)
call textf(522+9,14*5,20,' K(s) : ')
call textf(522+9*10,14*5,8,k$filen)
call textf(522+9,14*6,20,' L(s) : ')
call textf(522+9*10,14*6,8,l$filen)
call textf(522+9,14*7,20,' F(s) : ')
call textf(522+9*10,14*7,8,f$filen)
call textf(522+9,14*8,20,' W(i) : ')
call textf(522+9*10,14*8,8,w$filen)
call textf(522+9,14*10,20,' Process order x ')
write(str,'(i2.2)')order
call textf(522+9*16,14*10,2,str)
call textf(522+9*19,14*10,2,str)
call textf(522+9,14*12,20,' Element :( , ) ')
write(str,'(i2.2)')ri
call textf(522+9*13,14*12,2,str)
write(str,'(i2.2)')rj
call textf(522+9*16,14*12,2,str)
if (cuse.ne.0) then
  write(str,'(a,i2.2,a)')' Use column:['',cuse,'']
  call textf(522+9,14*13,16,str)
else
  write(str,'(a,i2.2,a)')' Use row : ['',ruse,'']
  call textf(522+9,14*13,16,str)
endif
call textf(522+9,14*15,20,' Frequency Range: ')
call textf(522+9,14*16,4,' 1:')
write(str,'(lp,E10.3,a)') w(1),' Rad/s'
call textf(522+9*5,14*16,16,str)
write(str,'(i3,a,lp,E10.3,a)') noofw,':',w(noofw),' Rad/s'
call textf(522+9,14*17,20,str)
write(str,'(a,lp,E10.3)')' X min: ',xlo
call textf(522+9,14*19,20,str)
write(str,'(a,lp,E10.3)')' max: ',xhi
call textf(522+9,14*20,20,str)
write(str,'(a,lp,E10.3)')' Y min: ',ylo
call textf(522+9,14*21,20,str)
write(str,'(a,lp,E10.3)')' max: ',yhi
call textf(522+9,14*22,20,str)
if (qinvrt) then
  call textf(522+9,14*23,20,' Operating on 1/Q(s)')
else
  call textf(522+9,14*23,20,' Operating on Q(s) ')
endif
call textf(522+9,347-5,20,' INACAD (c)R.Venzke ')
endif
return
end

```

\$include:'add.blk'

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```
*****
* PLTHED * PLOT HEADING FOR INA DIAGRAM *
*****
* Descr:   Adds information to the INA plot. *
* * * * *
* Param. : CLS - Flag set if information window is to be cleared first. *
* * * * *
* Call.by: PLTINA. *
* Calls:   Hercules Support *
*****
```

```
subroutine plthed(cls)
```

```
logical      cls
character*20 str
character*8  dfilen
```

```
$include:'design.blk'
$include:'desdta.blk'
```

```
if (cls) then
  call level(0)
  call blkfil(522,346,197,346)
endif
call level(1)
call putpt(522,0)
call dline(719,0)
call dline(719,347)
call dline(522,347)
call dline(522,0)
call putpt(1,1)
call dline(1,346)
call dline(718,346)
call dline(718,1)
call dline(1,1)
if (qinvrt) then
  call textf(522+9,14,20,'  INVERSE NYQUIST  ')
else
  call textf(522+9,14,20,'  DIRECT  NYQUIST  ')
endif
call textf(522+9,14*2,20,'  -----  ')
call textf(522+9,14*3,20,dsnme)
call textf(522+9,14*5,20,' G(s) :           ')
call textf(522+9*10,14*5,8,gfilen)
call textf(522+9,14*6,20,' K(s) :           ')
call textf(522+9*10,14*6,8,kfilen)
call textf(522+9,14*7,20,' L(s) :           ')
call textf(522+9*10,14*7,8,lfilen)
if (qinvrt) then
  call textf(522+9,14*8,20,' F(s) :           ')
  call textf(522+9*10,14*8,8,ffilen)
endif
call textf(522+9,14*9,20,' W(i) :           ')
call textf(522+9*10,14*9,8,wfilen)
call textf(522+9,14*11,20,' Process order  x  ')
write(str,'(i2.2)')order
call textf(522+9*16,14*11,2,str)
call textf(522+9*19,14*11,2,str)
if (single) then
  call textf(522+9,14*13,20,' Element : ( , ) ')
  write(str,'(i2.2)')si
```

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```

        call textf(522+9*13,14*13,2,str)
        write(str,'(i2.2)')sj
        call textf(522+9*16,14*13,2,str)
    endif
    call textf(522+9,14*15,20,' Frequency Range:  ')
    call textf(522+9,14*16,4,' 1:')
    write(str,'(lp,E10.3,a)') w(1),' Rad/s'
    call textf(522+9*5,14*16,16,str)
    write(str,'(i3,a,lp,E10.3,a)') noofw,':',w(noofw),' Rad/s'
    call textf(522+9,14*17,20,str)
    write(str,'(a,al,lp,E10.3)')' Axis: ',241,inadim
    call textf(522+9,14*19,20,str)
    if (gerint.ne.0)
+       call textf(522+9,14*21,20,' Gershgorin Circles ')
    if (ostint.ne.0)
+       call textf(522+9,14*22,20,' Ostrowski Circles ')
    if ((gerint.gt.0).or.(ostint.gt.0)) then
        call textf(522+9,14*23,20,' Row Dominance ')
    elseif ((gerint.ne.0).or.(ostint.ne.0)) then
        call textf(522+9,14*23,20,' Column Dominance ')
    endif
    call textf(522+9,347-5,20,' INACAD(c)RHE Venzke ')
    return
end

$include:'add.blk'
*****
* PLTINA * PLOT INA DIAGRAM *
*****
* Descr: Here the inverse Nyquist diagram is calculated and then plotted. *
* *
* Call.by: DIAGON *
* Calls: ansisup,DISK,PLTAXS,CALCQI,PLTPTS,PLTGER,Hercules support *
*****

subroutine pltina

integer i,j,k,offset,iocheck,readch,getch,t,fhandle,key
integer gerstp
logical err,calcg,calck,calcl,calcf,deterr
logical abort,kbhit,escape,trace,autoscale
complex det,qw(200),qwi
character*32 filen
external kbhit,readch,getch
character*20 input

$include:'desdta.blk'

$include:'design.blk'

gerstp=0
if (ostint+gerint.ne.0) then
    if (abs(ostint).gt.abs(gerint)) then
        gerstp=abs(ostint)
    else
        gerstp=abs(gerint)
    endif
    gerstp=nint(1.0*noofw/gerstp)
endif
call gmode

```

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```

call clrscr
22 autoscale=.false.
c if (.not.qexist) then
  if (.true.) then
    if (inadim.eq.0) then
      autoscale=.true.
      inadim=2.
    endif
    deterr=.false.
    abort=.false.
    trace=.false.
    t=1
    offset=order*order
    err=.false.
    calcg=(gfilen.ne.' ')
    calck=(kfilen.ne.' ')
    calcl=(lfilen.ne.' ')
    calcf=(ffilen.ne.' ')
    if (calcg) then
      call disk(filn,tfdir,gfilen,'.~gw')
      open(1,file=filn,form='binary',iostat=ioccheck)
    endif
    if (calck) then
      call disk(filn,tfdir,kfilen,'.~kw')
      open(2,file=filn,form='binary',iostat=ioccheck)
    endif
    if (calcl) then
      call disk(filn,tfdir,lfilen,'.~lw')
      open(3,file=filn,form='binary',iostat=ioccheck)
    endif
    call disk(filn,tfdir,'nyquist ','~jw')
    open(9,file=filn,form='binary',status='NEW',
+                                     iostat=ioccheck)
    fhandle=0
    if (calcf) then
      call disk(filn,tfdir,ffilen,'.~fw')
      open(4,file=filn,form='binary',iostat=ioccheck)
      call disk(filn,tfdir,ffilen,'.~f2')
      open(5,file=filn,form='binary',status='NEW',
+                                     iostat=ioccheck)
    do 12 i=1,noofw*offset
12   read(4,err=999) qwi
      write(5,err=999) qwi
      rewind 5
      rewind 4
      fhandle=5
    endif
    if (single) then
      call pltaxs(nint(1.))
    else
      call pltaxs(order)
    endif
    call plthed(.false.)
    call level(0)
    call textf(522+9,14*23,20,' Press ESC to abort.')
    call level(1)
    call calcqi(qw,calcg,calck,calcl,calcf,err,det)
    if (cabs(det).lt.1.e-8) then
1   do 1 j=1,order*order
      qw(j)=(0,0)
      deterr=.true.

```

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```

endif
do 2 i=1,noofw-1
  if (trace) then
155    t=mod(t+1,2)
        call level(t)
        call textf(522+9,14*23,20,' Hit KEY to continue')
        call level(1)
        if (.not.kbhit()) goto 155
  endif
  if (kbhit()) then
    key=readch()
    if (key.eq.27) then
      abort=.true.
      goto 998
    endif
    if (lowercase(key).eq.116) then
      trace=.not.trace
      if (.not.trace) then
        call level(0)
        call textf(522+9,14*23,20,' Press ESC to abort.')
        call level(1)
      endif
    endif
  endif
  if (.not.(err.or.abort)) then
    call calcqi(qw(offset+1),calcg,calck,calc1,
+          calcf,err,det)
    if (cabs(det).lt.1.e-8) then
4      do 4 j=1,order*order
          qw(j+offset)=(0,0)
          call level(t)
          t=mod(t+1,2)
          call textf(522+9,14*19,20,' Determinant *ERROR*')
          call level(1)
          deterr=.true.
        endif
        call pltpts(qw,single,si,sj,order,inadim,w(i))
      if ((gerint+ostint.ne.0).and.(mod(i,abs(gerstp)).eq.0))then
+        call pltger(qw,single,si,sj,order,inadim,gerint,
          ostint,fhandle,err)
      endif
3      do 3 j=1,order*order
          qw(j)=qw(j+offset)
      endif
2      continue
      close(9,iostat=ioccheck)
      if (ioccheck.ne.0) goto 999
      if (.not.autoscale) then
        if (gerstp.ne.0) call plthed(.true.)
      else
        call level(0)
        call textf(522+9,14*23,20,'REPLOT -> Rescaling ')
        call level(1)
        call disk(filn,tfdir,'nyquist ','~jw')
        open(9,file=filn,form='binary',status='OLD',iostat=ioccheck)
        inadim=0.
        do 35 i=1,offset*noofw
          read(9,err=999) qwi
          qwi=cmplx(abs(real(qwi)),abs(aimag(qwi)))
          if (real(qwi).gt.inadim) inadim=real(qwi)
          if (aimag(qwi).gt.inadim) inadim=aimag(qwi)

```

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```

35         continue
           write(*,'(a1\)' )7
           close(9)
         endif
         call textf(522+9,14*23,20,'          ')
         goto 998
999     err=.true.
998     qexist=.true.
         if (err) then
             call tmode
             call error('File corrupted - Plot aborted!')
             qexist=.false.
         else if (abort) then
             write(*,'(a1\)' )7
             i=getch()
             call tmode
             call clrbot
             write(*,'(8x,a,a\)' )' USER INTERRUPT: Plot aborted!',
+             ' Press any key to continue...'
             qexist=.false.
         else if (dterr) then
             i=getch()
             call tmode
             call error('Determinant = zero !          ')
         else if (.not.autoscale) then
             i=getch()
             if (i.eq.109) call mcircle(single,si,sj,order,inadim)
             if (i.eq.109) i=getch()
         endif
         if (calcg) close(1)
         if (calck) close(2)
         if (calcl) close(3)
         if (calcf) then
             close(4)
             close(5)
         endif
         endif
         if (autoscale.and.qexist) then
             qexist=.false.
             goto 22
         endif
         call tmode
         return
         end

subroutine mcircle(single,si,sj,order,inadim)
integer si,sj,order
logical single
real    inadim,re,r,cx,m
complex circ(50)

m=1.3
r=abs(m/(1-m*m))
x=m*m/(1-m*m)
do 1 i=1,50
    re=r*sin(i/50.0*2*3.1416)+x
    cx=r*cos(i/50.0*2*3.1416)
1    circ(i)=cmplx(re,cx)
    if (single) then
        do 3 i=1,49
3            call drawc(nint(1.),nint(1.),circ(i),nint(1.)),

```

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```

+          nint(1.),inadim)
  else
    do 2 i=1,order
      do 2 j=1,49
        call drawc(i,i,circ(j),nint(1.),order,inadim)
2      continue
    endif
    do 4 i=1,50
      re=sin(i/50.0*2*3.1416)
      cx=cos(i/50.0*2*3.1416)
4      circ(i)=cmplx(re,cx)
      if (single) then
        do 5 i=1,49
5          call drawc(nint(1.),nint(1.),circ(i),nint(1.),
+            nint(1.),inadim)
        else
          do 6 i=1,order
            do 6 j=1,49
              call drawc(i,i,circ(j),nint(1.),order,inadim)
6          continue
        endif
      return
    end

```

\$include:'add.blk'

```

*****
* PLTMLT * PLOT MULTIPLIER FUNCTION AND QUOTIENT *
*****
* Descr:  This routine plots the multiplier function and *
*         the quotient on a set of axis. *
* * *
* Call.by: ROWOP *
* Calls:  PLTHE2,ansisup,hercules graphic support. *
*****

```

subroutine pltmlt

```

logical      error,autoscale,user
complex      result(100)
real         pi, xp, yp
real         x, y, x2, y2, temp
complex      nw, dw, lw
integer      i, getch, key, j, k
external     getch

```

\$include:'desdta.blk'

\$include:'rowop.blk'

\$include:'design.blk'

\$include:'dim.blk'

```

user=.false.
if ((xhi.eq.0).and.(yhi.eq.0).and.
+  (xlo.eq.0).and.(ylo.eq.0)) then
  autoscale=.true.
else
  autoscale=.false.
endif
pi=3.1415926536
do 1 i=1,noofw
  call calcpw(nw,rkn,rsord,w(i))

```

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```

call calcpw(dw,rkd,rsord,w(i))
lw=cmplx(0.,amod( rkl*w(i) , 2 * pi ))
if (cabs(dw).le.1.e-8) then
  result(i)=(0,0)
else
  result(i)=nw/dw*cexp(lw)
endif
if (cabs(result(i)).ne.0.) user=.true.
1 continue
if (autoscale) then
  xlo=real(quotient(1))
  ylo=aimag(quotient(1))
  xhi=real(quotient(1))
  yhi=aimag(quotient(1))
  do 3 i=2,noofw
if (real(quotient(i)).gt.xhi) xhi=real(quotient(i))
if (aimag(quotient(i)).gt.yhi) yhi=aimag(quotient(i))
if (real(quotient(i)).lt.xlo) xlo=real(quotient(i))
if (aimag(quotient(i)).lt.ylo) ylo=aimag(quotient(i))
  if (user) then
if (real(result(i)).lt.xlo) xlo=real(result(i))
if (aimag(result(i)).lt.ylo) ylo=aimag(result(i))
if (real(result(i)).gt.xhi) xhi=real(result(i))
if (aimag(result(i)).gt.yhi) yhi=aimag(result(i))
  endif
3 continue
endif
xdim=xhi-xlo
ydim=yhi-ylo
if (xdim.lt.0) then
  temp=xhi
  xhi=xlo
  xlo=temp
  xdim=-xdim
endif
if (ydim.lt.0) then
  temp=yhi
  yhi=ylo
  ylo=temp
  ydim=-ydim
endif
if (xdim.lt.1.e-4) then
  xlo=xlo-0.5
  xhi=xhi+0.5
  xdim=xhi-xlo
endif
if (ydim.lt.1.e-4) then
  ylo=ylo-0.5
  yhi=yhi+0.5
  ydim=yhi-ylo
endif
call plthe2(.true.)
do 2 i=1,noofw-1
  x=real(quotient(i))
  y=aimag(quotient(i))
  x2=real(quotient(i+1))
  y2=aimag(quotient(i+1))
  xp=521.*(x-xlo)/xdim
  yp=347.-347.*(y-ylo)/ydim
  call putpt(nint(xp),nint(yp))
  call circ(nint(xp),nint(yp),3)
2

```

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```

xp=521.*(x2-xlo)/xdim
yp=347.-347.*(y2-ylo)/ydim
call dline(nint(xp),nint(yp))
x=real(result(i))
y=aimag(result(i))
x2=real(result(i+1))
y2=aimag(result(i+1))
xp=521.*(x-xlo)/xdim
yp=347.-347.*(y-ylo)/ydim
call putpt(nint(xp+4),nint(yp+3))
call dline(nint(xp-4),nint(yp-3))
call putpt(nint(xp-4),nint(yp+3))
call dline(nint(xp+4),nint(yp-3))
call putpt(nint(xp),nint(yp))
xp=521.*(x2-xlo)/xdim
yp=347.-347.*(y2-ylo)/ydim
call dline(nint(xp),nint(yp))
2   continue
call plthe2(.false.)
key=getch()
if (key.eq.32) then
  do 4 i=1,noofw
    x=real(quotient(i))
    y=aimag(quotient(i))
    x2=real(result(i))
    y2=aimag(result(i))
    xp=521.*(x-xlo)/xdim
    yp=347.-347.*(y-ylo)/ydim
    call putpt(nint(xp),nint(yp))
    xp=521.*(x2-xlo)/xdim
    yp=347.-347.*(y2-ylo)/ydim
    call dline(nint(xp),nint(yp))
4   continue
call plthe2(.false.)
key=getch()
endif
call tmode
100 return
end

$include:'add.blk'
*****
* PLTPTS * PLOT FREQUENCY POINTS FOR INA *
*****
* Descr:  The data for the INA is plotted for one frequency sample. *
* * * * *
* Param:  QW array containing ORDER*ORDER*2 frequency responses. *
*         *2 because lines are plotted to next value *
* * * * *
* Call.by: PLTINA *
* Calls:  DRAWC. *
*****

subroutine pltpts(qw,single,si,sj,order,dim,w)

complex      qw(*)
real         dim,w(*)
integer      i,j,index,indexs,offset,si,sj,order,readch
logical      single
character*20 str

```

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```

offset=order*order
index=sj+(si-1)*order
do 1 i=1,order
  do 1 j=1,order
    index=j+(i-1)*order
    if (single) then
      if (index.eq.indexs)
+       call drawc(nint(1.),nint(1.),qw(index),offset,
+       nint(1.),dim)
    else
      call drawc(i,j,qw(index),offset,order,dim)
    endif
1    continue

c    display current frequency

write(str,'(1p,E10.3)') w(2)
call textf(522+9*5,14*18,10,str)
return
end

$include:'add.blk'
*****
* PRCPAR * PROCESS PARAMETERS *
*****
* Descr:  Shows menu to view and edit process matrices. *
* * *
* Call.by: INADSN *
* Calls:  ansisup,GETORD,FRANGE,EDITTF,GETCHC *
*****

subroutine prcpar

integer  getch,key
logical  dsncrlr
external dsncrlr,getch

$INCLUDE:'MENU.BLK'
$INCLUDE:'DESIGN.BLK'
$INCLUDE:'DESDTA.BLK'

11  menunb=3
call getchc(menunb,escape)
if (escape) goto 111
if (chcdf1(menunb).eq.0) then
  if (dsncrlr()) then
    call setpfd
  else
    call error('Design must be cleared first!')
  endif
elseif (chcdf1(menunb).eq.1) then
  if (dsncrlr()) then
    call getord
  else
    call error('Design must be cleared first!')
  endif
elseif (chcdf1(menunb).eq.2) then
  call frange

```

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```

elseif (chcdf1(menunb).eq.3) then
  call edittf(gfilen,'.GS ','~gw',gnum,gden,glag,gexist)
elseif (chcdf1(menunb).eq.4) then
  call edittf(kfilen,'.KS ','~kw',knum,kden,klag,kexist)
elseif (chcdf1(menunb).eq.5) then
  call edittf(lfilen,'.LS ','~lw',lnum,lden,llag,lexist)
elseif (chcdf1(menunb).eq.6) then
  call edittf(ffilen,'.FS ','~fw',fnum,fden,flag,fexist)
endif
goto 11
111 return
end

$include:'add.blk'
*****
* PRINTF* PRINT TRANSFER FUNCTION
*****
* Descr: Prints selected transfer function matrix specification
*         on a printer or to the screen.
*
*
* Param: PFDIR,NAME,EXT - Filename specifications.
*         ARR,ARRD,ARRL - matrix coefficients.
*         ORDER - process order.
*         MXSORD - maximum power of s used.
*
* Call.by: PRCPAR
* Calls:  ansisup.
*****

subroutine printtf(pfdir,name,ext,arn,arrrd,arrrl,order,mxsord)

character*20 pfdir
character*8  name
character*4  ext
character*32 filen
real        arn(*),arrrd(*),arrrl(*)
integer     order,mxsord,i,k,j,sorder,ijk
integer     getch,key
external    getch

call clrbot
write(*,'(20x,a\)' )' Printer READY (y/n) ?'
key=getch()
if (key.eq.27) goto 100
if (lowercase(key).eq.121) then
  call clrbot
  write(*,'(a\)' )' Printing . . .'
  open(2,file='lpt1:')
else
  call cls
  open(2,file='con:')
endif
call dimtf(order,mxsord,sorder,arn,arrrd)
call disk(filen,pfdir,name,ext)
write(2,'(1h ,a)' )' '
write(2,'(1h ,2a)' )' Process Matrix: ',filen
write(2,'(1h ,a)' )' ===== '
write(2,'(1h ,a)' )' '
write(2,'(1h ,a)' )'

```

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```

+' Element      Order      Numerator      Denominator      Lag      '
  write(2,'(lh ,a)')
+'-----'-----'-----'-----'-----'
  do 3 i=1,order
    do 3 j=1,order
      write(2,'(lh ,a)')' '
      write(2,'(lh ,a,i2.2,a,i2.2,a)')' (' ,i',' ,j,') '
      do 3 k=1,sorder+1
        write(2,'(a,i2.2,a)')' s^ ,k-1, ' '
        ijk=k+(mxsord+1)*((j-1)+order*(i-1))
        write(2,'(a,lp,e13.6,a)')' ',arrn(ijk),' '
        write(2,'(a,lp,e13.6,a)')' ',arrd(ijk),' '
      if (k.eq.1) write(2,'(a,lp,e13.6,a)')' ',arrl(j+(i-1)*order),' '
      write(2,'(a)')' '
      write(2,'(lh ,a)')' '
3    continue
      write(2,'(lh )')
      write(2,'(lh \)')
      call clrbot
      write(*,'(a)')' Press <key> to continue . . .'
      key=getch()
      close(2)
100   return
      end

```

\$include:'add.blk'

```

*****
* PRTMLT * PRINT MULTIPLIER AND ROW OPERATION DATA *
*****
* Descr:  Print selected or last row or column operation *
*         specifications. It displays the selected multiplier *
*         too. *
* * *
* Call.by: ROWOP *
* Calls:  ansisup. *
*****

```

subroutine prtmlt

```

integer      i,getch,key
external     getch

```

\$include:'rowop.blk'

\$include:'design.blk'

```

call clrbot
write(*,'(20x,a)')' Printer READY (y/n) ?'
key=getch()
if (key.eq.27) goto 100
if (lowercase(key).eq.121) then
  call clrbot
  write(*,'(a)')' Printing operation . . .'
  open(2,file='lpt1:')
else
  call cls
  open(2,file='con:')
endif
write(2,'(lh ,a)')' '
write(2,'(lh ,a)')'*****'

```


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```

        write(*,'(a\)')' Printing operation . . .'
        open(2,file='lpt1:')
    else
        call cls
        open(2,file='con:')
    endif
    write(2,'(1h ,a)')' '
    write(2,'(1h ,a)')'*****'
    if (qinvrt) then
        if (cuse.eq.0) then
            write(2,'(1h ,a)')' Row Operation on 1/[Q(s)] -> [K(s)]'
        else
            write(2,'(1h ,a)')' Column Operation on 1/[Q(s)] -> [L(s)]'
        endif
    else
        if (cuse.eq.0) then
            write(2,'(1h ,a)')' Row Operation on [Q(s)] -> [L(s)]'
        else
            write(2,'(1h ,a)')' Column Operation on [Q(s)] -> [K(s)]'
        endif
    endif
    write(2,'(1h ,a)')'*****'
    write(2,'(1h ,a)')' '
    if (cuse.eq.0) then
        write(2,'(1h ,a,i2.2,a)')
+   ' Multiply Row [',ruse,'] by Function'
    else
        write(2,'(1h ,a,i2.2,a,a)')
+   ' Multiply Column [',cuse,'] by Function'
    endif
    write(2,'(1h ,a)')' '
    write(2,'(1h ,a)')
+   ' Multiplier:      Numerator      Denominator      Lag      '
    write(2,'(1h ,a)')
+   ' =====      -----      -----      ----      '
    do 1 i=1,rsord+1
        write(2,'(1h ,a,i2.2\)')' s^',i-1
        write(2,'(6x,e13.7,\)')rkn(i)
        write(2,'(3x,e13.7,\)')rkd(i)
        if (i.eq.1) then
            write(2,'(2x,e13.7)')rkl
        else
            write(2,'(1h )')
        endif
    1   continue
        write(2,'(1h0)')
        write(2,'(1h \)')
    100  call clrbot
        write(*,'(a\)')' Press <key> to continue . . . '
        key=getch()
        return
    end

```

\$include:'add.blk'

```

*****
* PRTNYQ * PRINT PROCESS FREQUENCY RESPONSE *
*****
* Descr:  Loads the process (INA Plot)response given by INA.PLT in *
*         the TFDIR, temporary file directory. The expected number *
*         of samples is given by NOOFW. The ORDER specifies the order *

```

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```

*          nxn of the matrix. The response is then printed.          *
*                                                                 *
* Call.by:  DIAGON          *
* Calls:   ansisup,ERROR.  *
*****
subroutine prtnyq

integer      iocheck
complex      kw
character*32 filen,user
character*8  name
integer      i,getch,key,j,k,l,m,readch
logical      kbhit,escape
external     getch,kbhit,readch

$include:'design.blk'
$include:'desdta.blk'

if (.not.qexist) then
  call error('No Nyquist Diagram exists !  ')
  return
endif
write(*,'(20x,a\)' )' Printer READY (y/n) ?'
key=getch()
if (key.eq.27) goto 100
call disk(filen,tfdir,'NYQUIST ','~JW')
open(1,file=filen,form='binary',iostat=iocheck)
if (lowcase(key).eq.121) then
  call clrbot
  write(*,'(8x,2a\)' )'Printing Frequency Response...',
+   ' Press <ESC> to abort.'
  open(2,file='lpt1:')
else
  call gotorc(10,10)
  write(*,'(a\)' )' (Use CON: for screen output) '
  call gotorc(11,10)
  write(*,'(a\)' )' Enter filename [.PRN]: '
  call readln(input,8,escape)
  if (escape) goto 199
  call disk(user,pfdir,input,'.prn')
  if ((input.eq.'con:  ') .or. (input.eq.'CON:  ')) then
    open(2,file='con:')
    call cls
  else
    open(2,file=user,status='new')
  endif
endif
write(2,'(1h ,a)' )' '
if (qinvrt) then
  write(2,'(1h ,a)' )'   Process Response: INVERSE '
else
  write(2,'(1h ,a)' )'   Process Response: DIRECT '
endif
write(2,'(1h ,a)' )' =====
write(2,'(1h ,a)' )' '
write(2,'(1h ,2a)' )'   Design : ',dsnnme
if (gfilen.ne.' ')
+ write(2,'(1h ,2a)' )'   [G(s)] : ',gfilen

```

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```

+   if (kfilen.ne.' ')
+     write(2,'(1h ,2a)')' [K(s)] : ',kfilen
+   if (lfilen.ne.' ')
+     write(2,'(1h ,2a)')' [L(s)] : ',lfilen
+   if (ffilen.ne.' ')
+     write(2,'(1h ,2a)')' [F(s)] : ',ffilen
+     write(2,'(1h ,2a)')' W(i) : ',wfilen
+     write(2,'(1h ,a)')' '
+     write(2,'(1h ,a)')
+     ' ELEMENT          FREQUENCY          REAL          IMAGINARY'
+     write(2,'(1h ,a)')
+     ' -----          -----          -----          -----'
+     write(2,'(1h ,a)')' '
+     do 1 i=1,order
+       do 1 j=1,order
+         write(2,'(1h )')
+         write(2,'(1h \)')
+         close(1)
+         open(1,file=filen,form='binary',iostat=ioccheck)
+         do 1 k=1,noofw
+           if (k.eq.1) then
+             write(2,'(a,i2.2,a,i2.2,a\)')' (' ,i',' ,j,') '
+           else
+             write(2,'(13x\)')
+           endif
+           write(2,'(1h ,1p,e13.6,a\)')w(k),' '
+           do 2 l=1,order
+             do 2 m=1,order
+               if (kbhit()) then
+                 if (readch().eq.27) goto 199
+               endif
+               read(1,err=99)kw
+               if ((l.eq.i).and.(m.eq.j)) then
+                 write(2,'(1p,e13.6,a\)') real(kw),' '
+                 write(2,'(1p,e13.6)') aimag(kw)
+               endif
+             continue
+           continue
+         write(2,'(1h )')
+         write(2,'(1h \)')
+         call clrbot
+         write(*,'(25x,a\)')' Press any key to continue...'
+         goto 100

99    call clrbot
+     write(*,'(2a\)')' *FILE ERROR*',filen
+     goto 100

199   call clrbot
+     write(*,'(8x,a\)')'USER INTERRUPT: Printout aborted. '

100   key=getch()
+     write(2,'(1h )')
+     close(1)
+     close(2)
+     return
+     end

$include:'add.blk'
*****

```

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```

* PRTPLT * PRINT PLOT
*****
* Descr: Prints the multiplier and quotient data on a printer.
*       If no printer is used displays output on screen.
*
* Calls: ansisup.
*****

      subroutine prtplt

      complex      result
      real         pi
      complex      nw,dw,lw
      logical      kbhit
      integer      i,getch,key,j,k,readch
      external     getch,readch,kbhit

$include:'desdta.blk'
$include:'rowop.blk'

      call clrbot
      write(*,'(20x,a\)' )' Printer READY (y/n) ?'
      key=getch()
      if (key.eq.27) goto 100
      if (lowercase(key).eq.121) then
        call clrbot
        write(*,'(8x,2a\)' )'Printing multiplier response. ',
+         'Press <ESC> to abort.'
        open(2,file='lpt1:')
      else
        call cls
        write(*,'(a,3a1\)' )'Press <ESC> to abort.',13,10,10
        open(2,file='con:')
      endif
      write(2,'(1h )')
      write(2,'(1h ,2a)' )
+ '          APPROXIMATION
+ 'DATA TO BE FITTED'
      write(2,'(1h ,2a)' )
+ ' FREQUENCY      real      imaginary ',
+ '      real      imaginary'
      write(2,'(1h ,2a)' )
+ ' -----'
+ ' -----'
      write(2,'(1h )')
      do 1 i=1,noofw
        if (kbhit()) then
          if (readch().eq.27) goto 199
        endif
        write(2,'(1h ,e13.7,\)' )w(i)
        call calcpw(nw,rkn,rsord,w(i))
        call calcpw(dw,rkd,rsord,w(i))
        if (cabs(dw).le.1.e-8) then
          result=(0,0)
          write(2,'(a30\)' ) ' *** Division by zero *** '
        else
          if (lw.ne.0) then
            lw=cmplx(0.,amod( rkl*w(i) , 2 * pi ))
            result=nw/dw*cexp(lw)
          else
            result=nw/dw
          endif
        endif
      enddo

```

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```

        endif
        write(2,'(2x,lp,e13.6,\)') real(result)
        write(2,'(2x,lp,e13.6,\)') aimag(result)
        endif
        write(2,'(4x,lp,e13.6,\)') real(quotient(i))
        write(2,'(2x,lp,e13.6)') aimag(quotient(i))
1      continue
        write(*,'(1h )')
        write(*,'(1h \)')
        call clrbot
        write(*,'(25x,a\)' )'Press any key to continue...'
        goto 100

199     call clrbot
        write(*,'(8x,a\)' )'USER INTERRUPT: Printout aborted.'
100     key=getch()
        close(2)
        return
        end

$include:'add.blk'
*****
* PSEUDO * PSEUDO-DIAGONALISATION *
*****
* Descr: This program calculates a K matrix to pseudo diagonalize *
* the frequency response of a transfer function matrix. *
* *
* This program is designed to be used in conjunction with *
* INACAD. *
* *
* Operating Instructions *
* ----- *
* *
* Use INACAD to plot the Inverse Nyquist Diagram of the *
* process. This will result in a temporary file being written *
* to disk : NYQUIST.JW. *
* *
* This file in addition to the following information entered *
* at run time will result in a parameter file : PSEUDO.KS *
* which can directly be used by INACAD. *
* *
* Additional input: *
* *
* Process order. & *
* Number of frequency points to use. *
* *
*****
* Support routines *
* *
* SREVAL - Calculate eigenvalues and eigenvectors. *
* *
* COMINV - Matrix inversion routine. *
* *
*****

program pseudo
integer n,ierr
complex gw1(100),u(100),d
real a(100),eval(10),evctr(100),aik(100)

```

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```

900  format(a\ )
      open(1,file='nyquist.jw',form='binary')
      open(2,file='pseudo.ks',status='new')
      write(*,900) ' Enter order:'
      read(*,'(i3)') n
      write(*,900) ' Enter no of frequency points:'
      read(*,'(i3)') nw

      do 7 jr=1,n
        do 8 ij=1,n*n
          8      a(ij)=0.0
          do 9 iw=1,nw
            do 10 i=1,n
              do 10 j=1,n
                ij=i+(j-1)*n
                10      read(1,err=99) gw1(ij)
                do 11 i=1,n
                  do 11 l=i,n
                    il=i+(l-1)*n
                    do 12 k=1,n
                      if (k.eq.jr) goto 12
                      ik=i+(k-1)*n
                      lk=l+(k-1)*n
                      a(il)=a(il)+real(gw1(ik))*real(gw1(lk))+
                +      aimag(gw1(ik))*aimag(gw1(lk))
                12      continue
                  li=l+(i-1)*n
                11      a(li)=a(il)
                9      continue
                rewind(1)
                call sreval(a,n,eval,evctr,aik,ierr)
                if (ierr.ne.0) then
                  write(*,*) 'Eval routine error'
                  stop
                endif
                emn=1.e30
                do 13 i=1,n
                  if (eval(i).gt.emn) goto 13
                  emn=eval(i)
                  imn=i
                13      continue
                sum=0.0
                do 14 j=1,n
                  jrj=jr+(j-1)*n
                  jimn=j+(imn-1)*n
                  u(jrj)=cmplx(evctr(jimn),0.0)
                14      sum=sum+real(u(jrj))
                  if (sum.gt.0) goto 7
                  do 19 j=1,n
                    jrj=jr+(j-1)*n
                19      u(jrj)=-u(jrj)
                7      continue
                close(1)
                call cominv(u,n,d)
                write(2,'(3i2)') n,n,1
                do 15 i=1,n
                  do 15 j=1,n
                15      write(2,'(e13.7)') real(u(i+(j-1)*n))
                do 16 i=1,n*n
                16      write(2,'(e13.7)') 1.0
                do 17 i=1,n*n

```

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```

17   write(2,'(e13.7)') 0.0
      close(2)
      goto 100
99   write(*,*) 'File access error'
100  continue
      stop
      end

```

```
$include:'add.blk'
```

```

*****
* READLN * READ LINE INPUT *
*****
* Descr:  Read a string input of specified length MAX. *
* * * * *
* Param:  INPUT returned string. *
*         ESCAPE logical true if the escape key was pressed. *
* * * * *
* Calls:  ansisup. *
*****

```

```
subroutine readln(input,max,escape)
```

```

character*20 input
character*2  keych
integer     readch,key,count
integer     max
external    readch
logical     escape,start
integer     line(20),i

```

```
escape=.false.
```

```
start=.true.
```

```
call saverc
```

```
count=0
```

```
input='
```

```

1   key=readch()
    if (key.eq.27) escape=.true.
    if (key.eq.27) goto 5
    if (key.eq.13) goto 5
    if (key.ge.32) then
      if (start) then
        do 4 k=1,max
4       write(*,'(a\)' ) '
          start=.false.
          call loadrc
        endif
        if (count.le.max-1) then
          count=count+1
          keych=char(key)
          write(*,'(a1,\)' ) keych
          line(count)=key
        else
          write(*,'(a1,\)' )7
        endif
      endif
    if ((count.ne.0).and.(key.eq.8)) then
      count=count-1
      call loadrc
      do 2 k=1,max

```

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```

2      write(*,'(a\)' )' '
      call loadrc
      do 2l k=1,count
21     write(*,'(a\)' )char(line(k))
      endif
      goto 1
5      continue
      do 21l k=1,count
211    input(k:k)=char(line(k))
      return
      end

$include:'add.blk'
*****
* REODKL * RECALCULATE K AND L MATRIX *
*****
* Descr:  The specified row or column operation is performed on *
*         the required row or column of the K or L matrix. The *
*         frequency response of the matrix is recalculated and *
*         written to disk. *
* * * * *
* Call.by: ROWOP *
* Calls:  ansisup.(DOCOL),(DOROW) *
*****

      subroutine redokl

      logical   exist
      integer   getch,key,i
      external  getch

$include:'rowop.blk'
$include:'design.blk'
$include:'desdta.blk'

      if (qinvrt) then
      if (((kfilen.eq.' ').and.(ruse.ne.0)).or.
+      ((lfilen.eq.' ').and.(ruse.eq.0))) then
          call error(' No K(s) or L(s) file exists !      ')
          goto 100
      endif
      else
+      if (((kfilen.eq.' ').and.(ruse.eq.0)).or.
          ((lfilen.eq.' ').and.(ruse.ne.0))) then
          call error(' No K(s) or L(s) file exists !      ')
          goto 100
      endif
      endif
      exist=.true.
      call savetf(tfdir,'backup ','.~ks',knum,kden,klag,
+      order,mxsord,exist)
      if (exist) goto 100
      exist=.true.
      call savetf(tfdir,'backup ','.~ls',lnum,lden,llag,
+      order,mxsord,exist)
      if (exist) goto 100
      qexist=.false.
      ksaved=.false.
      lsaved=.false.
      call clrtop

```

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```

if (qinvrt) then
  do 1 i=1,rsord+1
1    rkn(i)=-rkn(i)
    if (ruse.ne.0) then
      write(*,'(30x,a\)' )' Updating K(s). . .'
      call docol(rkn,rkd,rkl,knum,kden,klag,
+         order,mxsord,ruse,ri)
      call calctf(w,noofw,knum,kden,klag,mxsord,order,
+         kfilen,tfdir,'.~kw',qexist)
      kexist=.true.
      ksaved=.true.
    else
      write(*,'(30x,a\)' )' Updating L(s). . .'
      call dorow(rkn,rkd,rkl,lnum,lden,llag,
+         order,mxsord,cuse,rj)
      call calctf(w,noofw,lnum,lden,llag,mxsord,order,
+         lfilen,tfdir,'.~lw',qexist)
      lexist=.true.
      lsaved=.true.
    endif
  do 2 i=1,rsord+1
2    rkn(i)=-rkn(i)
  else
    write(*,'(8x,a\)' )'WARNING: operating on DIRECT Nyquist!'
    if (ruse.ne.0) then
      write(*,'(a\)' )' Updating L(s). . .'
      call dorow(rkn,rkd,rkl,lnum,lden,llag,
+         order,mxsord,ri,ruse)
      call calctf(w,noofw,lnum,lden,llag,mxsord,order,
+         lfilen,tfdir,'.~lw',qexist)
      lexist=.true.
      lsaved=.true.
    else
      write(*,'(a\)' )' Updating K(s). . .'
      call docol(rkn,rkd,rkl,knum,kden,klag,
+         order,mxsord,rj,cuse)
      call calctf(w,noofw,knum,kden,klag,mxsord,order,
+         kfilen,tfdir,'.~kw',qexist)
      ksaved=.true.
      kexist=.true.
    endif
  endif
100 return
end

c    Perform column operation on matrix

subroutine docol(rkn,rkd,rkl,knum,kden,klag,
+         order,mxsord,cchange,cuse)
real      rkn(*),rkd(*),rkl,knum(*),kden(*),klag(*)
real      mltn(140),mltd(140),mltl(10)
integer   order,mxsord,cchange,cuse,i,offst1,offst2

call mltncol(mltn,mltd,mltl,rkn,rkd,rkl,knum,
+         kden,klag,order,mxsord,cuse)
do 1 i=1,order
  offst1=1+(mxsord+1)*((cchange-1)+order*(i-1))
  offst2=1+(mxsord+1)*(i-1)
  call addelm(knum(offst1),kden(offst1),
+         klag(cchange+(i-1)*order),
+         mltn(offst2),mltd(offst2),mltl(i),

```

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```

+          knum(offst1),kden(offst1),
+          klag(cchange+(i-1)*order),mxsord)
1      continue
      return
      end

c      Perform row operation on matrix

      subroutine dorow(rkn,rkd,rkl,knum,kden,klag,
+          order,mxsord,rchange,ruse)
      real    rkn(*),rkd(*),rkl,knum(*),kden(*),klag(*)
      real    mltn(140),mltd(140),mltl(10)
      integer order,mxsord,rchange,ruse,i,offst1,offst2

      call mltrw(mltn,mltd,mltl,rkn,rkd,rkl,knum,
+          kden,klag,order,mxsord,ruse)
      do 1 i=1,order
        offst1=1+(mxsord+1)*((i-1)+order*(rchange-1))
        offst2=1+(mxsord+1)*(i-1)
        call addelm(knum(offst1),kden(offst1),
+          klag(i+(rchange-1)*order),
+          mltn(offst2),mltd(offst2),mltl(i),
+          knum(offst1),kden(offst1),
+          klag(i+(rchange-1)*order),mxsord)
1      continue
      return
      end

c      Add two elements.

      subroutine addelm(mltn,mltd,mltl,poly1n,poly1d,poly1l,
+          poly2n,poly2d,poly2l,mxsord)
      real    mltn(*),mltd(*),mltl,poly1n(*),poly1d(*)
      real    poly1l,poly2n(*),poly2d(*),poly2l,t,temp1(21)
      real    temp2(21)
      integer mxsord,i

      if ((poly1l.ne.0).or.(poly2l.ne.0)) then
        if (poly1l.ge.poly2l) then
          mltl=poly1l
          call polyxe(temp1,poly2n,poly2l-poly1l,mxsord)
          call multpoly(temp1,temp1,poly1d,mxsord)
          call multpoly(temp2,poly1n,poly2d,mxsord)
        else
          mltl=poly2l
          call polyxe(temp1,poly1n,poly1l-poly2l,mxsord)
          call multpoly(temp1,temp1,poly2d,mxsord)
          call multpoly(temp2,poly2n,poly1d,mxsord)
        endif
      else
        mltl=0.
        call multpoly(temp1,poly1n,poly2d,mxsord)
        call multpoly(temp2,poly2n,poly1d,mxsord)
      endif
      call addpoly(mltn,temp1,temp2,mxsord)
      call multpoly(mltd,poly1d,poly2d,mxsord)
      return
      end

c      Multiply row by function

      subroutine mltrw(mltn,mltd,mltl,rkn,rkd,rkl,knum,

```

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```

+           kden, klag, order, mxsord, rchange)

real       mlt1(*), mltd(*), mltl(*), rkn(*), rkd(*), rkl
real       knum(*), kden(*), klag(*)
integer    order, mxsord, rchange, i

do 1 i=1, order
1   mlt1(i)=rkl+klag(i+order*(rchange-1))
do 2 i=1, order
2   call multpoly(mltn(1+(mxsord+1)*(i-1)), rkn,
+     knum(1+(mxsord+1)*((i-1)+order*(rchange-1))), mxsord)
do 3 i=1, order
3   call multpoly(mltd(1+(mxsord+1)*(i-1)), rkd,
+     kden(1+(mxsord+1)*((i-1)+order*(rchange-1))), mxsord)
return
end

c   Multiply column by function

subroutine mltpol(mltn, mltd, mlt1, rkn, rkd, rkl, knum,
+     kden, klag, order, mxsord, cchange)

real       mlt1(*), mltd(*), mltl(*), rkn(*), rkd(*), rkl
real       knum(*), kden(*), klag(*)
integer    order, mxsord, cchange, i

do 1 i=1, order
1   mlt1(i)=klag(cchange+order*(i-1))+rkl
do 2 i=1, order
2   call multpoly(mltn(1+(mxsord+1)*(i-1)), rkn,
+     knum(1+(mxsord+1)*((cchange-1)+order*(i-1))), mxsord)
do 3 i=1, order
3   call multpoly(mltd(1+(mxsord+1)*(i-1)), rkd,
+     kden(1+(mxsord+1)*((cchange-1)+order*(i-1))), mxsord)
return
end

c   Multiply two polynomials

subroutine multpoly(result, poly1, poly2, mxsord)

real       result(*), poly1(*), poly2(*), sum
integer    mxsord, i, j

do 1 i=mxsord+1, 1, -1
    sum=0.
    do 2 j=1, i
2     sum=sum+poly1(j)*poly2(i-j+1)
1   result(i)=sum
return
end

c   Add two polynomials

subroutine addpoly(result, poly1, poly2, mxsord)

real       result(*), poly1(*), poly2(*)
integer    mxsord, i, j

do 1 i=1, mxsord+1
1   result(i)=poly1(i)+poly2(i)

```

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```

        return
        end

c      Construct series of ets

        subroutine polyxe(result,poly,t,mxsord)
        real    result(*),poly(*),coeff(21),fact,t
        integer mxsord,i
        external fact

        do 1 i=1,mxsord+1
1       coeff(i)=t/fact(i)
        call multpoly(result,poly,coeff,mxsord)
        return
        end

c      Calculate Factorial

        real function fact(x)
        integer x,i
        real product

        product=1.
        if (x.gt.1) then
1       do 1 i=2,x
            product=product*i
        endif
        fact=product
        return
        end

$include:'add.blk'
*****
* REDOWF * RE-CALCULATE TRANSFER MATRICES *
*****
* Descr:  This subroutine is called is the frequency range *
*         was altered. The transfer matrices are re-calculated. *
*         *
* Call.by: EDITWF *
* Calls:  CALCTF. *
*****

        subroutine redowf

$include:'design.blk'
$include:'desdta.blk'

        if (gfilen.ne.' ')
+       call calctf(w,noofw,gnum,gden,glag,mxsord,order,
+                 gfilen,tfdir,'.~gw',qexist)
        if (kfilen.ne.' ')
+       call calctf(w,noofw,knum,kden,klag,mxsord,order,
+                 kfilen,tfdir,'.~kw',qexist)
        if (lfilen.ne.' ')
+       call calctf(w,noofw,lnum,lden,llag,mxsord,order,
+                 lfilen,tfdir,'.~lw',qexist)
        if (ffilen.ne.' ')
+       call calctf(w,noofw,fnum,fden,flag,mxsord,order,
+                 ffilen,tfdir,'.~fw',qexist)
        return

```

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end

```

$include:'add.blk'
*****
* RCMLT * ROW/COLUMN MULTIPLICATION BY A FACTOR *
*****
* Descr: Multiply a row or column by a function. *
* * *
* Call.by: DIAGON *
* Calls: ansisup,SAVETF,CALCTF,KXROW,KXCOL,EDITMLT *
*****
      subroutine rcmlt

            integer      i,ruset,cuset,key,j,rit,rjt
            real         mltn(140),mltd(140),mltl(10)
            character*20 input
            integer      getch
            external     getch
            logical      change,exist

$INCLUDE:'MENU.BLK'
$include:'rowop.blk'
$include:'design.blk'
$include:'desdta.blk'

      change=.true.
11      menunb=9
         call getchc(menunb,escape)
         if (escape) goto 111
         if (chcdf1(menunb).eq.0) then
1        call gotorc(4,20)
           write(*,'(a\)' )'Select an array element that is to be '
           call gotorc(5,20)
           write(*,'(a\)' )'multiplied by the multiplier function.'
           call gotorc(8,20)
           write(*,'(a\)' )' Element: ('
           call saverc
           write(*,'(i2.2,a,i2.2,a\)' ) ri,',',rj,')'
           call loadrc
           call readln(input,5,escape)
           if (input.eq.' ') goto 12
           if (escape) goto 12
           read(input,222,err=199) rit,rjt
           if ((rit.gt.order).or.(rit.le.0)) goto 199
           if ((rjt.gt.order).or.(rjt.le.0)) goto 199
           change=.true.
           ri=rit
           rj=rjt
           goto 1
222      format(bn,2i2)
199      write(*,'(a\)' ) 7
           goto 1
12      ruse=ri
           cuse=0
2        call gotorc(10,20)
           write(*,'(a\)' )'Select row or column multiplication.'
           call gotorc(14,20)
           write(*,'(a\)' )'Press key to change and <ESC> to exit.'
           call gotorc(12,20)
           write(*,'(a\)' )'Multiply '

```

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```

if (cuse.eq.0) call invers
write(*,'(a\)' )' Row ['
write(*,'(i2.2,a\)' )ruse,' ] '
call normal
if (ruse.eq.0) call invers
write(*,'(a\)' )' Column ['
write(*,'(i2.2,a\)' )cuse,' ] '
call normal
if (getch().eq.27) goto 11
if (ruse.eq.0) then
  ruse=ri
  cuse=0
else
  cuse=rj
  ruse=0
endif
change=.true.
goto 2
elseif (chcdf1(menunb).eq.1) then
  call editmlt(1,rsord,rkd,rkn,rkl,9,change)
elseif (chcdf1(menunb).eq.2) then
  if (change) call getqu2
  change=.false.
  call optim
elseif (chcdf1(menunb).eq.3) then
  if (change) call getqu2
  change=.false.
  call pltmlt
elseif (chcdf1(menunb).eq.4) then
  call getscale
elseif (chcdf1(menunb).eq.5) then
  goto 113
elseif (chcdf1(menunb).eq.6) then
  call prtml2
elseif (chcdf1(menunb).eq.7) then
  if (change) call getqu2
  change=.false.
  call prtplt
endif
goto 11
113 call gotorc(4,15)
write(*,'(a\)' )' Perform Operation (y/n)?'
if (getch().ne.121) goto 100
write(*,'(a\)' )' YES'
if (qinvrt) then
  if (((kfilen.eq.' ').and.(ruse.ne.0)).or.
+    ((lfilen.eq.' ').and.(ruse.eq.0))) then
    call error(' No K(s) or L(s) file exists !      ')
    goto 100
  endif
  else
+    if (((kfilen.eq.' ').and.(ruse.eq.0)).or.
+      ((lfilen.eq.' ').and.(ruse.ne.0))) then
      call error(' No K(s) or L(s) file exists !      ')
      goto 100
    endif
  endif
  exist=.true.
+  call savetf(tfdir,'backup ','.~ks',knum,kden,klag,
+    order,mxsord,exist)
  if (exist) goto 100

```

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```

exist=.true.
call savetf(tfdir,'Backup ','.~ls',lnum,lden,llag,
+         order,mxsord,exist)
if (exist) goto 100
call clrtop
ksaved=.false.
lsaved=.false.
if (qinvrt) then
  if (ruse.ne.0) then
    write(*,'(30x,a\)' )' Updating K(s). . .'
    call kxcol(rkd,rkn,-rkl,knum,kden,klag,
+         order,mxsord,ruse)
    call calctf(w,noofw,knum,kden,klag,mxsord,order,
+         kfilen,tfdir,'.~kw',qexist)
    kexist=.true.
    ksaved=.true.
  else
    write(*,'(30x,a\)' )' Updating L(s). . .'
    call kxrow(rkd,rkn,-rkl,lnum,lden,llag,
+         order,mxsord,cuse)
    call calctf(w,noofw,lnum,lden,llag,mxsord,order,
+         lfilen,tfdir,'.~lw',qexist)
    lexist=.true.
    lsaved=.true.
  endif
else
write(*,'(8x,a\)' )'WARNING: operating on DIRECT Nyquist!'
if (ruse.ne.0) then
  write(*,'(a\)' )' Updating L(s). . .'
  call kxrow(rkn,rkd,rkl,lnum,lden,llag,
+         order,mxsord,ruse)
  call calctf(w,noofw,lnum,lden,llag,mxsord,order,
+         lfilen,tfdir,'.~lw',qexist)
  lexist=.true.
  lsaved=.true.
else
  write(*,'(a\)' )' Updating K(s). . .'
  call kxcol(rkn,rkd,rkl,knum,kden,klag,
+         order,mxsord,cuse)
  call calctf(w,noofw,knum,kden,klag,mxsord,order,
+         kfilen,tfdir,'.~kw',qexist)
  kexist=.true.
  ksaved=.true.
endif
endif
100  goto 11
111  return
end

```

\$include:'add.blk'

```

*****
* ROWOPE * ROW/COLUMN OPERATION *
*****
* Descr: Here the options for a row/column operation are selected. *
* * *
* Call.by: DIAGON *
* Calls: ansisup,GETCHC,READLN,EDITMLT,PRTMLT,OPTIM,REDOKL. *
*****

```

subroutine rowope

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```

integer      i,rit,rjt,ruset,cuset
character*20 input
integer      getch
external     getch
logical      change

$INCLUDE:'MENU.BLK'
$include:'rowop.blk'
$include:'design.blk'
$include:'dim.blk'

change=.true.
xlo=0
xhi=0
ylo=0
yhi=0
11  menunb=7
    call getchc(menunb,escape)
    if (escape) goto 111
    if (chcdf1(menunb).eq.0) then
1   call gotorc(4,15)
    write(*,'(a\)' )'Select an array element to reduce to zero.'
    call gotorc(6,15)
    write(*,'(a\)' )'          Element: ('
    call saverc
    write(*,'(i2.2,a,i2.2,a\)' )ri,',',rj,')'
    call loadrc
    call readln(input,5,escape)
    if (input.eq.' ') goto 12
    if (escape) goto 12
    read(input,222,err=99) rit,rjt
    if ((rit.gt.order).or.(rit.le.0)) goto 99
    if ((rjt.gt.order).or.(rjt.le.0)) goto 99
    change=.true.
    ri=rit
    rj=rjt
    cuse=0
    ruse=1
    goto 1
222  format(bn,2i2)
99   write(*,'(a\)' ) 7
    goto 1
12   call gotorc(8,15)
    write(*,'(a\)' )'Select a row or column to use in reduction.'
    call gotorc(12,20)
    write(*,'(a\)' )'Press <RTN> to change Row with Column.'
    call gotorc(13,20)
    write(*,'(a\)' )'or press <ESC> to exit.'
2   call gotorc(10,25)
    if (cuse.eq.0) then
        write(*,'(a\)' )'Use Row  ['
        call saverc
        write(*,'(i2.2,a\)' )ruse,']'
    else
        write(*,'(a\)' )'Use Column ['
        call saverc
        write(*,'(i2.2,a\)' )cuse,']'
    endif
    call loadrc
    call readln(input,2,escape)

```

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```

if (escape) goto 11
if (input.eq.' ') then
  if (cuse.eq.0) then
    cuse=ruse
    ruse=0
  else
    ruse=cuse
    cuse=0
  endif
  goto 2
endif
read(input,2222,err=999) ruset
if ((ruset.gt.order).or.(ruset.le.0)) goto 999
if ((ruset.eq.rj).and.(ruse.eq.0)) goto 999
if ((ruset.eq.ri).and.(cuse.eq.0)) goto 999
if (cuse.eq.0) then
  ruse=ruset
else
  cuse=ruset
  ruse=0
endif
change=.true.
goto 2
999  write(*,'(a\)' ) 7
      goto 2
2222 format(bn,i2)
      elseif (chcdf1(menunb).eq.1) then
        call editmlt(1,rsord,rkd,rkn,rkl,9,change)
      elseif (chcdf1(menunb).eq.2) then
        if (change) call getquot
        change=.false.
        call optim
      elseif (chcdf1(menunb).eq.3) then
        if (change) call getquot
        change=.false.
        call pltmlt
      elseif (chcdf1(menunb).eq.4) then
        call getscale
      elseif (chcdf1(menunb).eq.5) then
        call gotorc(4,20)
        write(*,'(a\)' )'Perform Operation (y/n)?'
        if (getch().eq.121) then
          write(*,'(a\)' )' YES'
          call redokl
        endif
      elseif (chcdf1(menunb).eq.6) then
        call prtmlt
      elseif (chcdf1(menunb).eq.7) then
        if (change) call getquot
        change=.false.
        call prtplt
      endif
      goto 11
111  return
      end

```

\$include:'add.blk'

```

*****
* SAVETF * SAVE TRANSFER FUNCTION MATRIX *
*****

```

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```

* Descr:   The transfer function as specified in arrd,arrr,arrrl with dimen- *
*          sion given by order and mxsord (maximum order of s possible) is *
*          saved. *
*          *
* Param:   ASK tells it whether to prompt the user for the save name. *
*          EXIST is an indication if the data was altered from last save *
*          if SAVETF was successful EXIST is set to FALSE *
*          *
* Call.by: EDITTF *
* Calls:   READLN,DISK *
*****

```

```

subroutine savetf(dir,name,ext,arn,arrr,arrrl,
+               order,mxsord,exist)

character*8 name
character*20 dir,input
character*4 ext
real arn(*),arrr(*),arrrl(*)
logical exist,escape,found
character*32 filen
integer getch,key,order,mxsord,sorder,ioccheck
external getch

1 call disk(filen,dir,name,ext)
open(1,file=filen,status='new')
call dimtf(order,mxsord,sorder,arn,arrr)
write(1,'(3i2)',err=2)order,order,sorder+1
do 3 i=1,order
  do 3 j=1,order
    do 3 k=1,sorder+1
      ijk=k+(mxsord+1)*((j-1)+order*(i-1))
3 write(1,'(e13.7)',err=2)arn(ijk)
do 4 i=1,order
  do 4 j=1,order
    do 4 k=1,sorder+1
      ijk=k+(mxsord+1)*((j-1)+order*(i-1))
4 write(1,'(e13.7)',err=2)arrr(ijk)
do 5 i=1,order*order
5 write(1,'(e13.7)',err=2)arrrl(i)
close(1,iostat=ioccheck)
if (ioccheck.ne.0) goto 2
exist=.false.
goto 100
2 call error('Disk write error! ')
100 return
end

```

```
$include:'add.blk'
```

```

*****
* SAVEWF * SAVE FREQUENCY FILE *
*****
* Descr:   Save frequency sample table with specified name. *
*          *
* Param:   DIR,NAME,EXT - filename specifications. *
*          ARR - array containg frequency points. *
*          NOOFW - number of points used. *
*          EXIST - Set false if successfully saved. *
*          *
* Call.by: EDITWF *

```

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```

* Calls:   DISK,ERROR
*****

      subroutine savewf(dir,name,ext,arr,noofw,exist)

      logical      exist
      character*8  name
      character*20 dir,input
      character*4  ext
      real         arr(*)
      character*32 filen
      integer      getch,key,noofw,ioccheck
      external    getch

1      call disk(filen,dir,name,ext)
      open(1,file=filen,status='new',iostat=ioccheck)
      write(1,'(i3)',err=2)noofw
      do 3 i=1,noofw
3         write(1,'(e13.7)',err=2)arr(i)
      close(1,iostat=ioccheck)
      if (ioccheck.ne.0) goto 2
      exist=.false.
      goto 100
2      call error('Disk write error!          ')
100     return
      end

$include:'add.blk'
*****
* SETPFD * SET PARAMETER FILE DIRECTORY
*****
* Descr:   Change the parameter and temporary file directories.
*
* Calls:   ansisup.
*****

      subroutine setpfd

      character*20 input
      logical      escape

$INCLUDE:'DESIGN.BLK'

      call gotorc(4,20)
      write(*,'(a,\)')'Select data file directories, '
      call gotorc(5,20)
      write(*,'(a,\)')'or enter ':' for none.'
      call gotorc(15,20)
      write(*,'(a,\)')'Press <ESC> to exit.'
      call gotorc(7,20)
      write(*,'(2a,\)')'Parameter file directory: ',pfdir
      call gotorc(9,20)
      write(*,'(2a,\)')'Temporary file directory: ',tfdir
      call gotorc(7,20)
      write(*,'(a,\)')'Parameter file directory: '
      call readln(input,20,escape)
      if(escape) goto 100
      if(input.ne.' ') pfdir=input
      if(input.eq.':') pfdir=' '
      call gotorc(9,20)

```

APPENDIX D SOFTWARE REFERENCE

```

write(*,'(a,\)')'Temporary file directory: '
call readln(input,20,escape)
if(escape) goto 100
if(input.ne.' ') tfdir=input
if (input.eq.':') tfdir=' '
100  return
end

```

```
$include:'add.blk'
```

```

*****
* SHWPAR * SHOW DESIGN PARAMETERS *
*****
* Descr:   Displays current design parameter settings. *
*          Also displays if parameters have not yet been updated. *
*          * *
* Param:   WAIT logical true if key must be pressed to continue. *
*          * *
* Calls:   ansisup. *
*****

```

```
subroutine shwpar(wait)
```

```

character*20 input
logical        wait
integer        key,readch
external       readch

```

```
$INCLUDE:'DESIGN.BLK'
```

```

call gotorc(3,20)
write(*,'(a,\)')' DESIGN PROGRAM STATUS '
call gotorc(5,15)
call normal
write(*,'(a\)' )' Current Design Name      : '
write(*,'(2a,\)')' ',dsnnme
call gotorc(7,15)
write(*,'(a,\)')' Process Matrix Order    : '
write(*,'(I3,\)')'order
call gotorc(9,15)
write(*,'(a,\)')' Frequency Range File    : '
write(*,'(3a,\)')' ',wfilen,['.WS ]'
if (wexist) write(*,'(a\)' )' SAVE!'
call gotorc(11,15)
write(*,'(a,\)')' Plant Matrix G(s)       : '
write(*,'(3a,\)')' ',gfilen,['.GS ]'
if (gexist) write(*,'(a\)' )' SAVE!'
call gotorc(13,15)
write(*,'(a,\)')' Controller Matrix K(s)  : '
write(*,'(3a,\)')' ',kfilen,['.KS ]'
if (kexist) write(*,'(a\)' )' SAVE!'
call gotorc(15,15)
write(*,'(a,\)')' Controller Matrix L(s)  : '
write(*,'(3a,\)')' ',lfilen,['.LS ]'
if (lexist) write(*,'(a\)' )' SAVE!'
call gotorc(17,15)
write(*,'(a,\)')' Feedback Matrix F(s)    : '
write(*,'(3a,\)')' ',ffilen,['.FS ]'
if (fexist) write(*,'(a\)' )' SAVE!'
call gotorc(19,15)
write(*,'(a,\)')' Parameter File Directory : '

```

APPENDIX D SOFTWARE REFERENCE

```

write(*,'(2a,\)')' ',pfdir
call gotorc(21,15)
write(*,'(a,\)')' Temporary File Directory : '
write(*,'(2a,\)')' ',tfdir
if (wait) then
  call clrtop
write(*,'(15x,a\)' )' Enter New Design Name : '
  call readln(input,19,escape)
  if (input.ne.' ') dsnme=input
endif
return
end

$include:'add.blk'
*****
* SWOP * SWOP ROW OR COLUMNS OF INA *
*****
* Descr: Here the rows or columns of the INA can be swopped. *
* Swopping rows of the INA changes rows of K *
* Swopping columns of the INA changes columns of L *
* *
* Call.by: DIAGON. *
* Calls: ansisup,SAVETF,CALCTF,(SWOPROW),(SWOPCOL) *
*****

subroutine swop

integer rit,rjt
character*20 input
logical change,exist
real temp
integer key,getch
external getch

$INCLUDE:'MENU.BLK'
$include:'rowop.blk'
$include:'design.blk'
$include:'desdta.blk'

11 menunb=10
call getchc(menunb,escape)
if (escape) goto 111
if (chcdf1(menunb).eq.0) then
1 call gotorc(4,20)
write(*,'(a\)' )'Select rows to be swopped.'
call gotorc(6,20)
write(*,'(a\)' )' Rows '
call saverc
write(*,'(i2.2,a,i2.2\)' ) ri,',',ruse
call loadrc
call readln(input,5,escape)
if (input.eq.' ') goto 11
if (escape) goto 11
read(input,222,err=1) rit,rjt
if ((rit.gt.order).or.(rit.le.0)) goto 1
if ((rjt.gt.order).or.(rjt.le.0)) goto 1
change=.true.
ri=rit
ruse=rjt
cuse=0

```

APPENDIX D SOFTWARE REFERENCE

```

                goto 1
222          format(bn,2i2)
          elseif (chcdf1(menunb).eq.1) then
2            call gotorc(4,20)
              write(*,'(a\)' )'Select columns to be swopped.'
              call gotorc(6,20)
              write(*,'(a\)' )' Columns '
              call saverc
              write(*,'(i2.2,a,i2.2\)' ) rj,',',cuse
              call loadrc
              call readln(input,5,escape)
              if (input.eq.' ') goto 11
              if (escape) goto 11
              read(input,222,err=2) rit,rjt
              if ((rit.gt.order).or.(rit.le.0)) goto 2
              if ((rjt.gt.order).or.(rjt.le.0)) goto 2
              change=.true.
              rj=rit
              cuse=rjt
              ruse=0
              goto 2
          elseif (chcdf1(menunb).eq.2) then
              goto 113
          elseif (chcdf1(menunb).eq.3) then
              call clrtop
              write(*,'(20x,a\)' )' Printer READY (y/n) ?'
              key=getch()
              if (key.eq.27) goto 11
              if (lowercase(key).eq.121) then
                  call clrbot
                  write(*,'(a\)' )' Printing operation . . .'
                  open(2,file='lpt1:')
              else
                  call cls
                  open(2,file='con:')
              endif
              write(2,'(1h ,a)' )' '
              write(2,'(1h ,a)' )'***** '
              if (qinvrt) then
                  if (cuse.eq.0) then
                      write(2,'(1h ,a)' )' Row operation on 1/[Q(s)] -> [K(s)]'
                  else
                      write(2,'(1h ,a)' )' Column operation on 1/[Q(s)] -> [L(s)]'
                  endif
              else
                  if (cuse.eq.0) then
                      write(2,'(1h ,a)' )' Row operation on [Q(s)] -> [L(s)]'
                  else
                      write(2,'(1h ,a)' )' Column operation on [Q(s)] -> [K(s)]'
                  endif
              endif
              write(2,'(1h ,a)' )'***** '
              write(2,'(1h )' )'
              if (cuse.eq.0) then
                  write(2,'(1h ,a,i2.2,a,i2.2)' )
+                 'Row : ',ri,' swopped with row : ',ruse
              else
                  write(2,'(1h ,a,i2.2,a,i2.2)' )
+                 'Column: ',rj,' swopped with column: ',cuse
              endif
              write(2,'(1h0,a)' )' '

```

APPENDIX D SOFTWARE REFERENCE

```

write(2,'(1h ,a\))' '
call clrbot
write(*,'(20x,a\))' ' Press <key> to continue . . .'
key=getch()
close(2)
goto 11
endif
113 call gotorc(4,15)
write(*,'(25x,a\))' 'Perform Operation (y/n)?'
if (lowercase(getch()).ne.121) goto 100
write(*,'(a\))' ' YES'
if (qinvrt) then
+   if (((kfilen.eq.' ').and.(ruse.ne.0)).or.
      ((lfilen.eq.' ').and.(ruse.eq.0))) then
      call error(' No K(s) or L(s) file exists !      ')
      goto 100
    endif
    else
+   if (((kfilen.eq.' ').and.(ruse.eq.0)).or.
      ((lfilen.eq.' ').and.(ruse.ne.0))) then
      call error(' No K(s) or L(s) file exists !      ')
      goto 100
    endif
  endif
  exist=.true.
+  call savetf(tfdir,'backup ','.~ks',knum,kden,klag,
              order,mxsord,exist)
  if (exist) goto 100
  exist=.true.
+  call savetf(tfdir,'backup ','.~ls',lnum,lden,llag,
              order,mxsord,exist)
  if (exist) goto 100
  ksaved=.false.
  lsaved=.false.
  call clrtop
  if (qinvrt) then
    if (ruse.ne.0) then
      write(*,'(30x,a\))' ' Updating K(s). . .'
      call swopcol(knum,kden,klag,order,mxsord,ri,ruse)
      call calctf(w,noofw,knum,kden,klag,mxsord,order,
+             kfilen,tfdir,'.~kw',qexist)
      kexist=.true.
      ksaved=.true.
    else
      write(*,'(30x,a\))' ' Updating L(s). . .'
      call swoprow(lnum,lden,llag,order,mxsord,rj,cuse)
      call calctf(w,noofw,lnum,lden,llag,mxsord,order,
+             lfilen,tfdir,'.~lw',qexist)
      lexist=.true.
      lsaved=.true.
    endif
  else
    write(*,'(8x,a\))' 'WARNING: operating on DIRECT Nyquist!'
    if (ruse.ne.0) then
      write(*,'(a\))' ' Updating L(s). . .'
      call swoprow(lnum,lden,llag,order,mxsord,ri,ruse)
      call calctf(w,noofw,lnum,lden,llag,mxsord,order,
+             lfilen,tfdir,'.~lw',qexist)
      lexist=.true.
      lsaved=.true.
    else

```

APPENDIX D SOFTWARE REFERENCE

```

        write(*,'(a\)' )' Updating K(s). . .'
        call swopcol(knum,kden,klag,order,mxsord,rj,cuse)
        call calctf(w,noofw, knum,kden,klag,mxsord,order,
+           kfilen,tfdir,'.~kw',qexist)
        kexist=.true.
        ksaved=.true.
    endif
endif
100  goto 11
111  return
end

```

c Swop columns

```

subroutine swopcol(knum,kden,klag,order,mxsord,ri,ruse)
real          knum(*),kden(*),klag(*),temp
integer       order,mxsord,ri,ruse,i,j

do 1 i=1,order
    temp=klag(ruse+order*(i-1))
    klag(ruse+order*(i-1))=
+   klag(ri+order*(i-1))
    klag(ri+order*(i-1))=temp
    do 1 j=1,mxsord+1
        temp=knnum(j+(mxsord+1)*((ruse-1)+order*(i-1)))
        knum(j+(mxsord+1)*((ruse-1)+order*(i-1)))=
+       knum(j+(mxsord+1)*((ri-1)+order*(i-1)))
        knum(j+(mxsord+1)*((ri-1)+order*(i-1)))=temp
        temp=kden(j+(mxsord+1)*((ruse-1)+order*(i-1)))
        kden(j+(mxsord+1)*((ruse-1)+order*(i-1)))=
+       kden(j+(mxsord+1)*((ri-1)+order*(i-1)))
1       kden(j+(mxsord+1)*((ri-1)+order*(i-1)))=temp
    return
end

```

c Swop rows

```

subroutine swoprow(lnum,lden,llag,order,mxsord,rj,cuse)
real          lnum(*),lden(*),llag(*),temp
integer       order,mxsord,rj,cuse,i,j

do 1 i=1,order
    temp=llag(i+order*(cuse-1))
    llag(i+order*(cuse-1))=
+   llag(i+order*(rj-1))
    llag(i+order*(rj-1))=temp
    do 1 j=1,mxsord+1
        temp=lnum(j+(mxsord+1)*((i-1)+order*(cuse-1)))
        lnum(j+(mxsord+1)*((i-1)+order*(cuse-1)))=
+       lnum(j+(mxsord+1)*((i-1)+order*(rj-1)))
        lnum(j+(mxsord+1)*((i-1)+order*(rj-1)))=temp
        temp=lden(j+(mxsord+1)*((i-1)+order*(cuse-1)))
        lden(j+(mxsord+1)*((i-1)+order*(cuse-1)))=
+       lden(j+(mxsord+1)*((i-1)+order*(rj-1)))
1       lden(j+(mxsord+1)*((i-1)+order*(rj-1)))=temp
    return
end

```

\$include: 'add.blk'

APPENDIX D SOFTWARE REFERENCE

```

* SYSICAL * SYSTEM CALL
*****
* Descr:  Execute child process specified.
*
* Param:  COMMAND - String containing DOS command.
*
* Call.by:
* Calls:  SYSTEM - routine in CEXEC.LIB
*****

```

c Construct interface specification to C library routine

```

interface to integer*2 function system [c]
+ (string[reference])
character*1 string
end

subroutine syscal(command)

integer*2 i,system
character*30[c] command

i = system(command)
if (i.eq.-1) call error('No COMMAND.COM file found! ')
end

```

c Perform DOS command selection

```

subroutine dos

integer key,getch
external getch
character*30[c] command
logical success

call gotorc(4,1)
write(*,'(a)')'Enter DOS command or press <RTN> to exit.'
call gotorc(6,1)
1 write(*,'(a)')'C>'
read(*,'(a)') command
if (command.eq.' ') goto 100
call syscal(command)
write(*,'(3al)')' ',13,10
goto 1
100 return
end

```

c Delete all temporary files that were created.

```

subroutine deltmp
character*30[c] command

command='erase *.~??'
call syscal(command)
return
end

```

```

$include:'add.blk'
*****
* UNDOCH * UNDO ALTERATION OF K OR L MATRIX
*
```

APPENDIX D SOFTWARE REFERENCE

```
*****
* Descr:   Loads a saved copy of the K and L matrix from disk.           *
*          Subroutine is called to reverse the effect of a row         *
*          operation.                                                    *
*                                                                 *
* Call.by: ROWOP                                                         *
* Calls:   ansisup,CALCTF,LOADTF.                                       *
*****
```

```
subroutine undoch
      logical      exist
      character*8  name
      integer      getch,key
      external     getch
```

```
$include:'rowop.blk'
$include:'design.blk'
$include:'desdta.blk'
```

```
      if (kfilen.eq.' ') ksaved=.false.
      if (lfilen.eq.' ') lsaved=.false.
      if ((.not.ksaved).and(.not.lsaved)) then
        call error('No change pending !           ')
        goto 100
      endif
      call gotorc(4,20)
      if (lsaved.and.ksaved) then
        write(*,'(a\)' )'Undo Change to K(s) and L(s) matrix (y/n)?'
      elseif (lsaved) then
        write(*,'(a\)' )'Undo Change to L(s) matrix (y/n)?'
      else
        write(*,'(a\)' )'Undo Change to K(s) matrix (y/n)?'
      endif
      if (getch().eq.121) then
        write(*,'(a\)' )' YES'
        exist=.false.
        name='backup '
        if (ksaved) then
          call loadtf(tfdir,name,'.~ks',knum,kden,klag,
+             order,mxsord,exist)
          call calctf(w,noofw,knum,kden,klag,mxsord,order,
+             kfilen,tfdir,'.~kw',qexist)
        endif
        if (lsaved) then
          call loadtf(tfdir,name,'.~ls',lnum,lden,llag,
+             order,mxsord,exist)
          call calctf(w,noofw,lnum,lden,llag,mxsord,order,
+             lfilen,tfdir,'.~lw',qexist)
        endif
        ksaved=.false.
        lsaved=.false.
      endif
      return
100 end
```

1.5 MENU TREE STRUCTURE

The menu tree structure of the INACAD program is constructed as follows:

1.1 Dos Command

Run a DOS program or execute DOS command.

1.2 Help

Display help message.

1.3 Design Status

Displays current design program status and allows entry of design description.

1.4 Process Parameters

1.4.1 File Directories

Edit file directories.

1.4.2 Process Order

Edit process order.

1.4.3 Frequency Range

1.4.3.1 Load Frequency Data

Load frequency data from disk.

1.4.3.2 Edit Frequency Data

Edit the frequency type& range.

1.4.3.3 Save Frequency Data

Save frequency data to disk.

1.4.4 Plant matrix G(s)

1.4.4.1 Load Transfer Fn

Load data file from disk.

1.4.4.2 Edit Transfer Fn

Edit matrix data.

APPENDIX D SOFTWARE REFERENCE

1.4.4.3 Save Transfer Fn

Save data file to disk.

1.4.4.4 Print Transfer Fn

Print matrix on printer.

1.4.4.5 Remove Parameter

Remove parameter from design.

1.4.5 Controller mx K(s)

1.4.5.1 Load Transfer Fn

Load data file from disk.

1.4.5.2 Edit Transfer Fn

Edit matrix data.

1.4.5.3 Save Transfer Fn

Save data file to disk.

1.4.5.4 Print Transfer Fn

Print matrix on printer.

1.4.5.5 Remove Parameter

Remove parameter from design.

APPENDIX D SOFTWARE REFERENCE

1.4.6 Controller $m \times L(s)$

1.4.6.1 Load Transfer Fn

Load data file from disk.

1.4.6.2 Edit Transfer Fn

Edit matrix data.

1.4.6.3 Save Transfer Fn

Save data file to disk.

1.4.6.4 Print Transfer Fn

Print matrix on printer.

1.4.6.5 Remove Parameter

Remove parameter from design.

1.4.7 Feedback $m \times F(s)$

1.4.7.1 Load Transfer Fn

Load data file from disk.

1.4.7.2 Edit Transfer Fn

Edit matrix data.

1.4.7.3 Save Transfer Fn

Save data file to disk.

1.4.7.4 Print Transfer Fn

Print matrix on printer.

1.4.7.5 Remove Parameter

Remove parameter from design.

1.5 Diagonalisation

1.5.1 Nyquist Setup

*Enter options for Nyquist diagram.
i.e. scale, inverse/direct, Gershgorin/
Ostrowski circles, Row/Column dominance.*

APPENDIX D SOFTWARE REFERENCE

1.5.2 Plot Nyquist

Display diagram on the screen.

1.5.3 Row/Col. Operation

1.5.3.1 Operation Options

*Specify element to eliminate,
and element to use.*

1.5.3.2 Edit Multiplier

*Enter multiplier function for
the elimination.*

1.5.3.3 Optimize Multiplier

*Optimize multiplier function
for best elimination result.*

1.5.3.4 Plot Multiplier

*Display multiplier function and
quotient on the screen.*

1.5.3.5 Adjust Scale

Specify the scale of the plot.

1.5.3.6 Perform Operation

Calculate new K or L matrix.

1.5.3.7 Print Operation

Print operation on printer.

1.5.3.8 Print Plot

*Print multiplier and quotient
response on printer.*

APPENDIX D SOFTWARE REFERENCE

1.5.4 Swop Rows/Columns

1.5.4.1 Swop Rows

Select which rows to swop.

1.5.4.2 Swop Columns

Select which Columns to swop.

1.5.4.3 Perform Operation

Calculate new K or L matrix.

1.5.4.4 Print Operation

Print operation on printer.

1.5.5 Multiply Row/Col.

1.5.5.1 Operation Options

*Specify element to multiply
by the function.*

1.5.5.2 Edit Multiplier

*Enter function to use for the
multiplication.*

1.5.5.3 Optimize Multiplier

*Optimize function so that
result is close to unity.*

1.5.5.4 Plot Multiplier

*Display function and
quotient on the screen.*

1.5.5.5 Adjust Scale

Specify the scale of the plot.

1.5.5.6 Perform Operation

Calculate new K or L matrix.

1.5.5.7 Print Operation

Print operation on printer.

APPENDIX D SOFTWARE REFERENCE

1.5.5.8 Print Plot

Print multiplier and quotient response on printer.

1.5.6 Undo Operation

Restore K or L matrix.

1.5.7 Print Response

Print process response on printer.

1.6 Clear Design

Clear design specifications.

1.7 Quit Program

Terminate INACAD and return to DOS.

APPENDIX D SOFTWARE REFERENCE

2. POLE ASSIGNMENT ROUTINES

2.1 SUBROUTINE OVERVIEW

calcabk	Calculate matrix (A-BK)
calcf	Calculate feedback vector f
calck	Calculate feedback matrix K
calcm	Calculate solution matrix M
calcr	Calculate closed-loop coefficient vector r
control	Check controllability
faddev	Perform FADDEEV algorithm
getdata	Read input data from file
multpoly	Multiply polynomials
mxbyvec	Multiply matrix by vector
mximlt	Multiply matrices
mxinv	Invert matrix
mxmult	Multiply matrices
poleval	Find matrix eigenvalues
print	Print results
pacad	Main program
sume	Sum coefficients e for FADDEEV algorithm

2.1.1 Implementation of BORRIE method

Included in the listing are the following routines, which can be used to apply the controllable companion form algorithm instead of the FADDEEV method or as a check.

To implement note that $T=M^T$ and T^{-1} is calculated by *calct*.

calcac	Calculate open-loop characteristic coeff.
calct	Calculate matrix T^{-1} by BORRIE method
vecbymx	Multiply vector by matrix

2.2 SUBROUTINE INDEX

calcabk(n,a,b,k,t)	314
calcac(n,a,trinv,tr,tm,tm2,ac)	326
calcf(n,m,r,f)	315
calck(n,q,f,k)	315
calcm(n,g,bb,m)	315
calcr(n,pole,e,rv,r)	314
calct(n,p,a,tm,tm2,trinv)	325
control(n,a,u,q,t,tm,tm2,p,bb,det)	316

APPENDIX D SOFTWARE REFERENCE

faddev(n,a,b,e,p)	317
getdata(N,A,b,pole,q)	319
multpoly(mxsort,poly1,poly2)	323
mxbyvec(n,a,q,t)	320
mximlt(n,a,b,i,p)	318
mxinv(n,c,b)	320
mxmult(n,a,b,p)	319
pacad	312
poleval(n,pole,poly)	323
print(N,det,g,E,m,p,r,k,f,rv,id)	324
sume(n,e,p,b,i)	318
vecbymx(n,v,a,b)	326

2.4 SOURCE LISTING

```

*****
* PACAD * Pole Assignment Computer Aided Design *
*****
* Descr: This program applies the dyadic approach to the design of *
* a controller for a multivariable control system by pole *
* assignment. *
* *
* System description: *
* *
* dx A is nxn *
* ---- = A x(t) + B u(t) B is nxn max. *
* dt *
* *
* choose Q for pole assignment Q is a real n-vector *
* " POLE i.e. closed loop poles POLE is a complex n-vector *
* *
* Input File Format: *
* *
* Line Col:12345678901234567890 *
* 1 >Process Order max 25 *
* 2 >2 *
* 3 >System matrix A e.g. Identity matrix *
* 4 >1.0 0.0 *
* 5 >0.0 1.0 *
* 6 >System matrix B e.g. Identity matrix *
* 7 >1.0 0.0 *
* 8 >0.0 1.0 *
* 9 >Required Roots Real part Imaginary part *
* 10 >-1.0 0.0 -1.0 0.0 *
* 11 >Q vector *
* 12 >1.0 0.0 *
* *
* Format used I2, E10.4 *
* *
* Note - In this examples lines 1,3,6,9 & 11 will be skipped *
* and may contain any comment. *
* *
*****

```

APPENDIX D SOFTWARE REFERENCE

```

program pacad

c   input data

integer order,pass
character*64 ifnam,ofnam,comment
real*8 a(25,25),b(25,25),q(25)
complex*16 pole(25)

c   calculation data

real*8 det
real*8 g(25,25,25),e(25),p(25,25),m(25,25),k(25,25),f(25),r(25)
real*8 t(25),bb(25),id(25,25),rv(25),tm(25,25),tm2(25,25)

c   G used for for faddeev method
c   E coeff. of characteristic function for closed loop system
c   P temporary matrix used by faddeev and retains M before inversion
c   M matrix identified with G(s)
c   K controller matrix
c   F feedback control vector
c   DET determinant used to test controllability
c   R solution vector
c   T temporary vector used by CONTROL
c   TM, TM2 temporary matrices used by CONTROL
c   BB vector containing b=Uq
c   ORDER process order max. 25

write(*,911) '#Multivariable Pole Assignment Design Program'
write(*,911) '#(C) Copyright R.Venzke 1988'
write(*,911) '#'

write(*,900)
900 format('#Data filename : '\)
read(*,911) ifnam
write(*,901)
901 format('#Output filename : '\)
read(*,911) ofnam
910 format(a\)
911 format(a)

open(3,file=ifnam)
open(4,file=ofnam,status='new')

write(*,910) '#Reading, '
read(3,'(a)') comment
read(3,500) order
500 format(bn,i7)

c   read input data from file
call getdata(order,a,b,pole,q)

write(*,910) 'processing, control ,'
c   check controllability
call control(order,a,b,q,t,tm,tm2,p,bb,det)

write(*,910) 'faddeev, '
c   get matrix G from faddeev algorithm
call faddev(order,a,g,e,p)

```

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```

c      write(*,910) 'Matrix M, '
      calculate matrix identified with G(s)
      call calcm(order,g,bb,m)

c      write(*,910) 'Matrix M, '
      get a copy of M before inversion
      call calcm(order,g,bb,p)

c      calculate inverse of m to solve simultaneous eqs.
      call mxinv(n,det,m)
      if (det.eq.0) then
        write(*,*) ' ERROR:Inversion of M not possible!'
      endif

c      write(*,910) 'vector R, '
      calculate solution vector R
      call calcr(order,pole,e,rv,r)

c      write(*,910) 'Vector F, '
      calculate vector F
      call calcf(order,m,r,f)

c      write(*,910) 'check inversion , '
      check inversion of m
      call mxmult(order,m,p,id)

c      write(*,910) 'Matrix K, '
      calculate controller matrix K
      call calck(order,q,f,k)

c      write(*,910) 'Matrix A-BK, '
      calculate closed loop A matrix
      call calcabk(order,a,b,k,t)

      write(*,910) 'writing, '

c      print results to output file
      call print(order,det,g,e,m,p,r,k,f,rv,id)

      write(*,911) 'done.'
      close(3)
      close(4)
      end

```

```

*****
* CALCABK* Calculate A-BK matrix
*****
* Descr: Calculate the closed loop A matrix after state feedback.
*         The results are written to a file ABK.DAT sothat
*         this matrix can be used to check where the resulting system
*         poles are placed after pole assignment.
*
* Param: N - order of matrix
*         A - A matrix
*         B - B matrix
*         K - K matrix
*         T - temporary nxn matrix
*
*****

```

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```

subroutine calcabk(n,a,b,k,t)
integer n,i,j,l
real*8 a(n,n),b(n,n),k(n,n),t(n,n)

do 1 i=1,n
  do 1 j=1,n
    t(i,j)=a(i,j)
    do 1 l=1,n
1      t(i,j)=t(i,j)-b(i,l)*k(l,j)

open(8,file='abk.dat',status='new')
write(8,'(i2)') n
do 2 i=1,n
2  write(8,'(25e10.4)') (t(i,j),j=1,n)
close(8)
return
end

*****
* CALCR * Calculate resulting r-vector *
*****
* Descr: Subtract the open loop characteristic coefficient vector *
*         from the desired closed loop characteristic equation and store *
*         result in the solution vector-r. *
* * * * *
* Param: N - system order *
*         POLE - array containing desired pole positions *
*         E - open loop characteristic equation from Faddeev algorithm *
*         RV - desired characteristic eqn for closed loop system *
*         R - solution vector *
* * * * *
* Call.by: PACAD *
* Calls : POLEVAL *
*****

subroutine calcr(n,pole,e,rv,r)
integer n
real*8 e(n),r(n),t,rv(n)
complex*16 pole(n)

call poleval(n,pole,rv)
do 1 i=1,n
1  r(i)=rv(i)-e(i)
return
end

*****
* CALCM * CALCULATE M MATRIX *
*****
* Descr: Here the m(s)-matrix containing the product of the faddeev *
*         equivalent single input system g(s) and the b=Bq vector is *
*         calculated. *
* * * * *
* Param: N - system order *
*         G - Faddeev g(s) nxn matrix *
*         BB - b-vector *
*         M - resulting nxn matrix *
* * * * *
* Call.by: PACAD *
* Calls: none. *

```


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end

```

*****
* CONTROL* Check controllability
*****
* Descr: This routine checks whether the choice of vector Q
*        for the pole assignment technique gives the necessary
*        controllability of the feedback system, by inverting
*        matrix W and finding its determinant.
*
*
*          2          n
*        P = [ b, Ab, A b, .... A b ] , where b= Bq
*
* Param: DET - determinant of P
*        A - system matrix nxn
*        N - process order
*        U - input matrix B
*        Q - design n-vector q
*        P - controllabilty matrix nxn
*        T - temporary n-vector
*        TM - temporary nxn matrix
*        TM2 - temporary nxn matrix
*        BB - resulting n-vector b
*****

subroutine control(n,a,u,q,t,tm,tm2,p,bb,det)
integer n
real*8 a(n,n),u(n,n),q(n),p(n,n),t(n),det
real*8 bb(n),tm(n,n),tm2(n,n)

c      t=u*q
      call mxbyvec(n,u,q,t)

c
c      p(1)=t
      do 1 i=1,n
1         p(i,1)=t(i)

      if (n.eq.1) goto 100

c      put matrix A into temporary storage
      do 2 i=1,n
        do 2 j=1,n
2          tm(i,j)=a(i,j)

c      calculate A*t
      call mxmult(n,a,t,bb)

c      store in p(2) => p(2)=At
      do 3 i=1,n
3         p(i,2)=bb(i)

      do 4 k=3,n

c      calculate A * A * ....
      call mxmult(n,tm,a,tm2)
      do 5 i=1,n
        do 5 j=1,n
5          tm(i,j)=tm2(i,j)

      call mxbyvec(n,tm,t,bb)

```


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```

max=0
do 21 j=1,n
  do 21 k=1,n
    if (j.eq.k) then
      max=dmax1(max,p(j,k)+e(1))
    elseif (i.ne.1) then
      max=dmax1(max,p(j,k))
    endif
21  continue
write(*,'(a,e12.4,a\)' ) 'Check= ',max,'=zero '
return
end

c    Do summation for characteristic eqn

subroutine sume(n,e,p,b,i)
integer n,j,k,i
real*8  p(n,n),e,b(n,n,n)

c    Add new coefficient e to AB

do 21 j=1,n
  do 21 k=1,n
    if (j.eq.k) then
      b(i,j,k)=p(j,k)+e
    elseif (i.ne.1) then
      b(i,j,k)=p(j,k)
    endif
21  continue
return
end

c    Calculate the trace of a matrix

real*8 function trace(n,b)
integer n
real*8  b(n,n),t

t=0.
do 2 i=1,n
2   t=t+b(i,i)
trace=t
return
end

c    Multiply matrix A by matrix B[i]

subroutine mximlt(n,a,b,i,p)
integer n,i,j,l,k
real*8  a(n,n),b(n,n,n),p(n,n)

do 10 l=1,n
  do 10 j=1,n
    p(l,j)=0.
    do 10 k=1,n
10   p(l,j)=p(l,j)+a(l,k)*b(i,k,j)
return
end

c    Multiply matrix A by matrix B[i]

```

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c used to check inversion routine

```

subroutine mxmult(n,a,b,p)
integer n,j,l,k
real*8  a(n,n),b(n,n),p(n,n)

do 10 l=1,n
  do 10 j=1,n
    p(l,j)=0.
    do 11 k=1,n
11      p(l,j)=p(l,j)+a(l,k)*b(k,j)
c      write(*,*) ' ',p(l,j)
10    continue
      return
end

```

```

*****
*GETDATA* Get Program Data
*****
* Descr: Reads ORDER,matrix A, matrix B, POLE positions and vector Q
*        from file #4. The read data is then written to file #3 to
*        check the input data.
*
* Param: N process order
*        A,B nxn matrix
*        POLE n-vector containing pole positions
*        Q design n-vector
*        File #4 - INPUT
*        File #3 - OUTPUT
*
* Call.by: PACAD
* Calls: none
*****

```

```

SUBROUTINE getdata(N,A,b,pole,q)
INTEGER N
REAL*8 A(n,n),b(n,n),q(n)
COMPLEX*16 pole(n)
INTEGER I,J

501 format(bn,25e10.4)
502 format(lp,50e12.4)
503 format(bn,50e10.4)
write(4,400) N
400 format(' Process Order = ',i7)

write(4,'(a)') ' Matrix A : '
read(3,'(a)') comment
do 99 i = 1,N
  read(3,501) (A(i,j), j=1,N)
  write(4,'(lp,25e12.4)') (A(i,j), j = 1,N)
99 continue
write(4,'(a)') ' '

write(4,'(a)') ' Matrix B : '
read(3,'(a)') comment
do 199 i = 1,N
  read(3,501) (b(i,j), j=1,N)
  write(4,'(lp,25e12.4)') (b(i,j), j = 1,N)
199 continue
write(4,'(a)') ' '

```

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```

write(4,'(a)') ' Design Poles : '
read(3,'(a)') comment
read(3,503) (pole(i), i =1,n)
write(4,502) (pole(i), i = 1,N)
write(4,'(a)') ' '

write(4,'(a)') ' Design Q vector : '
read(3,'(a)') comment
read(3,501) (q(i), i =1,n)
write(4,'(lp,25e12.4)') (q(i), i = 1,N)
write(4,'(a)') ' *****'
write(4,'(a)') ' '
RETURN
end

*****
*MXBYVEC * Matrix by vector multiplication *
*****
* Descr: MXBYVEC mutliplies matrix A by a vector Q and stores the *
* result in vector T *
* *
* Param: A is nxn matrix *
* Q is n vector *
* T is resulting n vector *
* N is the order n *
* Call.by: *
* Calls: none *
*****

subroutine mxbyvec(n,a,q,t)
integer n
real*8 a(n,n),q(n),t(n)

do 1 i=1,n
t(i)=0.
do 1 j=1,n
1 t(i)=t(i)+a(i,j)*q(j)
return
end

*****
* MXINV * REAL MATRIX INVERSION *
*****
* Descr: Inverts a real matrix using the Gauss-Jordan *
* ellimination with complete pivoting. *
* *
* Note: It is an adaptation of a complex matrix inversion routine *
* *
* Param: B = matrix *
* N = Dimension of B where B is nxn *
* C = determinant of B *
* *
* Call.by: CONTROL,CALCM *
* Calls: none. *
*****

SUBROUTINE mxinv(n,c,b)

INTEGER IR(30),IC(30)
C IR,IC are the pivot point of the matrix

```

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```

real*8      a(900),D,TEMP,HOLD
real*8      b(n,n),c
INTEGER     I,N,J,K,L,II,JJ,III,M,IJ,IIJ,IT,KI,KJ,LP

do 101 i=1,n
do 101 j=1,n
101      a((i-1)*n+j)=b(i,j)
DO 10 I=1,N
      IR(I)=I
      IC(I)=I
10     CONTINUE
D=1.0d0
M=-N
DO 70 I=1,N
      M=M+N+1
      IF (I.EQ.N) GOTO 40
      BIG=dABS(A(M))
      II=I
      JJ=I
      DO 20 K=I,N
        LP=(I-2)*N+K
        DO 20 L=I,N
          LP=LP+N
          IF (dABS(A(LP)).LE.BIG) GOTO 20
          BIG=dABS(A(LP))
          II=K
          JJ=L
20     CONTINUE
22     IF (II.EQ.I) GOTO 30
        IJ=I-N
        IIJ=II-N
        DO 25 J=1,N
          IJ=IJ+N
          IIJ=IIJ+N
          TEMP=A(IJ)
          A(IJ)=A(IIJ)
          A(IIJ)=TEMP
25     CONTINUE
        IT=IR(I)
        IR(I)=IR(II)
        IR(II)=IT
        D=-D
30     IF (JJ.EQ.I) GOTO 40
        IJ=(I-1)*N
        IIJ=(JJ-1)*N
        DO 35 J=1,N
          IJ=IJ+1
          IIJ=IIJ+1
          TEMP=A(IJ)
          A(IJ)=A(IIJ)
          A(IIJ)=TEMP
35     CONTINUE
        IT=IC(JJ)
        IC(JJ)=IC(I)
        IC(I)=IT
        D=-D
40     if (dabs(d*a(m)).lt.1.d-150) then
          c=0.0d0
          return
        endif
      D=D*A(M)

```

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```

TEMP=A(M)
A(M)=1.0d0
IJ=I-N
DO 50 J=1,N
    IJ=IJ+N
    A(IJ)=A(IJ)/TEMP
50  CONTINUE
    KI=(I-1)*N
    DO 70 K=1,N
        KI=KI+1
        IF (K.EQ.I) GOTO 70
        TEMP=A(KI)
        A(KI)=0.0d0
        KJ=K-N
        IJ=I-N
        DO 60 J=1,N
            KJ=KJ+N
            IJ=IJ+N
            HOLD=-TEMP*A(IJ)
            A(KJ)=A(KJ)+HOLD
60  CONTINUE
70  CONTINUE
72  CONTINUE
    DO 80 I=1,N
        IF (IR(I).EQ.I) GOTO 80
        K=IR(I)
        JI=(I-1)*N
        JK=(K-1)*N
        DO 85 J=1,N
            JI=JI+1
            JK=JK+1
            TEMP=A(JI)
            A(JI)=A(JK)
            A(JK)=TEMP
85  CONTINUE
        IR(I)=IR(K)
        IR(K)=K
    GOTO 72
80  CONTINUE
82  CONTINUE
    DO 90 I=1,N
        IF(IC(I).EQ.I) GOTO 90
        K=IC(I)
        IJ=I-N
        KJ=K-N
        DO 75 J=1,N
            IJ=IJ+N
            KJ=KJ+N
            TEMP=A(IJ)
            A(IJ)=A(KJ)
            A(KJ)=TEMP
75  CONTINUE
        IC(I)=IC(K)
        IC(K)=K
    GOTO 82
90  CONTINUE
do 100 i=1,n
do 100 j=1,n
    b(i,j)=a((i-1)*n+j)
100 c=d
RETURN

```

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END

```
*****
*POLEVAL * Polynomial Evaluation *
*****
* Descr: POLEVAL evaluates a polynomial from given roots. *
* *
* Param: N no. of roots *
*       POLE array containing roots *
*       POLY array containing subscripts of polynomial *
*       eqn= s^(n-1)*poly(n)+...s*poly(2)+poly(1) *
* *
*****
```

```
subroutine poleval(n,pole,poly)
integer    n,i,j
real*8    poly(n)
complex*16 pole(n),polyt,polyc(25)

do 2 i=1,n
  polyc(i)=(0.0,0.0)
  polyc(1)=(1.0,0.0)
  do 1 i=1,n
    polyt=-pole(i)
    call multpoly(n,polyc,polyt)
  1 continue
  do 3 i=1,n
    poly(i)=dreal(polyc(i))
    if (cabs(polyc(i)).ne.abs(poly(i))) then
      write(*,'(a\)' ) ' Coeff= '
      write(*,'(1p,50e12.4)')polyc(i)
      write(*,*)' WARNING:Complex poles are not conjugates.'
    endif
  3 continue

return
end
```

```
*****
*MULTPOLY* Multiply Polynomials *
*****
* Descr: Multiply polynomial of form: *
*       s^(n-1)*poly(n)+...s*poly(2)+poly(1) * ( s + poly2 ) *
* *
* Param: MXSORD maximum order of s *
*       POLY1 array containing polynomials of s *
*       POLY2 -pole to add *
*       POLY1 resulting polynomial of order MXSORD *
* *
*****
```

```
subroutine multpoly(mxsort,poly1,poly2)
complex*16 poly1(*),poly2
integer    mxsort,i,j

do 2 i=mxsort,2,-1
  poly1(i)=POLY1(I-1)+poly1(i)*poly2
  poly1(1)=poly1(1)*poly2
return
end
```

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```

*****
* PRINT * Print data
*****
* Descr: Prints the intermediate results of the pole assignment
*        technique and the resulting controller.
*
* Call.by: PACAD
* Calls:  none
*****

```

```

subroutine print(N,det,g,E,m,p,r,k,f,rv,id)
INTEGER N,l
REAL*8 g(n,n,n),e(n),m(n,n),p(n,n),r(n),rv(n),k(n,n),det,f(n)
real*8 id(n,n)

write(4,'(a)') ' '
write(4,'(a\)') ' Controllability determinant : '
write(4,'(1p,25e12.4)') det
write(4,'(a)') ' '

write(4,'(a)') ' Open Loop Characteristic polynomial : '
write(4,'(1p,25e12.4)') (e(i), i=1,N)
write(4,'(a)') ' '

write(4,'(a)') ' Faddev Matrix'
do 1 i=1,n
  write(4,'(a,i2)') ' s^',n-i
  do 1 j=1,n
1    write(4,'(1p,25e12.4)') (g(i,j,l), l=1,N)
write(4,'(a)') ' '

write(4,'(a)') ' Closed Loop Characteristic polynomial : '
write(4,'(1p,25e12.4)') (rv(i), i=1,N)
write(4,'(a)') ' '

write(4,'(a)') ' Matrix M identified with G(s) : '
do 2 j=1,n
2  write(4,'(1p,25e12.4)') (p(j,l), l=1,N)
write(4,'(a)') ' '

write(4,'(a)') ' Inverse of M : '
do 3 j=1,n
3  write(4,'(1p,25e12.4)') (m(j,l), l=1,N)
write(4,'(a)') ' '

write(4,'(a)') ' Identity of M * 1/M : '
do 7 j=1,n
7  write(4,'(1p,25e12.4)') (id(j,l), l=1,N)
write(4,'(a)') ' '

write(4,'(a)') ' Resulting vector : '
write(4,'(1p,25e12.4)') (r(i), i=1,N)
write(4,'(a)') ' '

write(4,'(a)') ' Feedback vector : '
write(4,'(1p,25e12.4)') (f(l), l=1,N)
write(4,'(a)') ' '

write(4,'(a)') ' Resulting controller : '
do 4 j=1,n
4  write(4,'(1p,25e12.4)') (k(j,l), l=1,N)

```


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```

end

c Calculate vector by matrix multiplication

subroutine vecbymx(n,v,a,b)
integer n,i,j
real*8 v(n),a(n,n),b(n)

do 1 i=1,n
  b(i)=0.0
  do 1 j=1,n
1    b(i)=b(i)+v(j)*a(j,i)
  return
end

*****
* CALCAC * CALCULATE AC VECTOR *
*****
* Descr: This routine calculates the closed-loop character- *
*        istic equation from T and T-1 from the controllable *
*        companion method. *
* * * * *
* Param: N - system order *
*        TRINV - controllabilty matrix inverse *
*        TR - controllabiliy matrix *
*        A - system A matrix *
*        TM, TM2 - temporary nxn matrices *
*        AC - Resulting vector *
* * * * *
* Call.by: BORRIE *
* * * * *
* Calls: MXMULT, VECBYMX, *
*****
subroutine calcac(n,a,trinv,tr,tm,tm2,ac)
integer n
real*8 a(n,n),trinv(n,n),tr(n,n),tm(n,n)
real*8 tm2(n,n),ac(n)

call mxmult(n,trinv,a,tm)
call mxmult(n,tm,tr,tm2)
do 2 i=1,n
2  ac(i)=-tm2(n,i)
write(4,'(a)') 'Ac vector:'
write(4,600) (ac(j), j=1,n)
600 format(1p,25e12.4)

return
end

```

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